

**AIR EMISSION TEST REPORT**  
**Wiggins, Mississippi Wood Pellet Production Facility**  
**Enviva Pellets Wiggins, LLC**

Submitted to

Enviva Pellets Wiggins, LLC

Submitted by

Air Control Techniques, P.C.  
301 East Durham Road  
Cary, NC 29513  
(919) 460-7811

Report Submittal Date: October 31, 2013  
(Revised November 14, 2013)  
Air Control Techniques, P.C. File 1911



## TABLE OF CONTENTS

<b>1.</b>	<b>Summary</b>	<b>1</b>
<b>2.</b>	<b>Emission Test Program Description</b>	<b>3</b>
	2.1 Wiggins, Mississippi Plant Description	3
	2.2 Purpose and Scope of the Emission Test Program	3
	2.3 Test Participants	4
<b>3.</b>	<b>Test Matrix and Test Results</b>	<b>6</b>
	3.1 Test Matrix	6
	3.2 Test Results	6
	3.3 Emission Data Evaluation	14
	3.4 VOC and HAP Emission Summary	16
<b>4.</b>	<b>Sampling Locations</b>	<b>18</b>
	4.1 Dryer 1 Stack Sampling Location	18
	4.2 Dryer 2 Stack Sampling Location	19
	4.3 Dry Hammermill 2 Cyclone Outlet Sampling Location	20
	4.4 Pellet Mill Aspiration System Sampling Location	21
	4.5 Pellet Cooler 2 Stack Sampling Location	22
	4.6 Pellet Cooler 1 Stack Sampling Location	23
	4.7 Green Hammermill Stack Sampling Location	24
<b>5.</b>	<b>Testing Procedures</b>	<b>25</b>
	5.1 Flue Gas Velocity and Volumetric Flow Rate – EPA Method 2	25
	5.2 Flue Gas Composition and Molecular Weight – EPA Method 3	25
	5.3 Flue Gas Moisture – EPA Method 4	25
	5.4 Total Hydrocarbon Concentrations – EPA Method 25A	25
	5.5 Organic HAPs – EPA Method 320	26
<b>6.</b>	<b>Quality Assurance</b>	<b>28</b>
	6.1 Method 1 Quality Assurance	28
	6.2 Method 4 Quality Assurance	28
	6.3 Method 25A Quality Assurance	28
	6.4 Method 320 Quality Assurance	33
<b>7.</b>	<b>Process Documentation</b>	<b>35</b>
<b>8.</b>	<b>References</b>	<b>36</b>
 <b>Appendices</b>		
	<b>A. Moisture and Gas Flow Rate Data</b>	
	<b>B. Method 25A Data</b>	
	<b>C. Method 320 Data</b>	
	<b>D. Method 320 Log Sheet</b>	
	<b>E. Example Calculations</b>	
	<b>F. Gas Cylinder Certification Sheets</b>	
	<b>G. Equipment Calibration Sheets</b>	

## TABLES

1-1.	Total Emissions at Plant Permit Limit of 185,550 ODT per Year	1
1-2	Total Emissions at Plant Permit Limit of 140,000 ODT per Year	2
3-1	Test Matrix, Air Emission Testing, Enviva Pellets Wiggins, MS	6
3-2	Green Hammermill Emission Test Results	7
3-3	Dryer 1 Emission Test Results	8
3-4	Pellet Cooler 1 Emission Test Results	9
3-5	Dryer 2 Emission Test Results	10
3-6	Dry Hammermill 2 Emission Test Results	11
3-7	Pellet Cooler 2 Emission Test Results	12
3-8	Aspiration System Emission Test Results	13
3-9	Alpha-Pinene Method 25A Response Factors	15
3-10	Calculated Method 25A Response Factors in Phase I Laboratory Tests	15
3-11.	Total Emissions at Plant Permit Limit of 185,550 ODT per Year	17
3-12	Total Emissions at Plant Permit Limit of 140,000 ODT per Year	17
6-1	Dryer 1 Quality Assurance Results, Total Hydrocarbons, Method 25A	29
6-2	Pellet Cooler 1 Quality Assurance Results, Total Hydrocarbons, Method 25A	29
6-3	Dryer 2 Quality Assurance Results, Total Hydrocarbons, High Range, Method 25A	30
6-4	Dryer 2 Quality Assurance Results, Total Hydrocarbons, Low Range, Method 25A	30
6-5	Dry Hammermill 2 Quality Assurance Results, Total Hydrocarbons, Method 25A	31
6-6	Pellet Cooler 2 Quality Assurance Results, Total Hydrocarbons, Method 25A	31
6-7	Aspiration System Quality Assurance Results, Total Hydrocarbons, Method 25A	32
6-8	Green Hammermill Quality Assurance Results, Total Hydrocarbons, Method 25A	32
6-9	CTS Results, Method 320	33
6-10	Spike Recovery Results, Method 320	34

## FIGURES

4-1	Dryer 1 Stack Sampling Location	18
4-2	Photograph of the Dryer 1 Stack	18
4-3	Dryer 2 Stack Sampling Location	19
4-4	Photograph of the Dryer 2 Stack	19
4-5	Dry Hammermill 2 Sampling Location	20
4-6	Photograph of the Dry Hammermill 2 Sampling Location	20
4-7	Pellet Mill Aspiration System Sampling Location	21
4-8	Photograph of the Pellet Mill Aspiration System Sampling Location	21
4-9	Pellet Mill 2 Cooler Stack Sampling Location	22
4-10	Photograph of the Pellet Mill 2 Cooler Stack Sampling Location	22
4-11	Pellet Mill 1 Cooler Stack Sampling Location	23
4-12	Photograph of the Pellet Mill 1 Cooler Stack Sampling Location	23
4-13	Green Hammermill Stack Sampling Location	24
4-14	Photograph of the Green Hammermill Stack Sampling Location	24
5-1	Method 320 Organic HAP Sampling System	26

## Definitions

Total Hydrocarbons All organic compounds containing hydrogen and carbon that are detected by a flame ionization detector operated in accordance with U.S. EPA Method 25A.

### Volatile Organic Compounds

All organic compounds that are emitted to the atmosphere in a gaseous or vapor form that can participate in photochemical reactions to produce ozone. All volatile organic compounds are considered VOCs unless specifically exempted in 40 CFR 51.100(s). Relevant excluded compounds include methane, ethane, and acetone.

VOC Emissions Mass emissions of VOC measured on a pounds of carbon basis.

## Acronyms

EPA	U.S. Environmental Protection Agency
FID	Flame Ionization Detector
FTIR	Fourier Transform Infrared Spectrometer
HAP	Hazardous Air Pollutant
MC	Moisture Content
MDEQ	Mississippi Department of Environmental Quality
ODT	Oven Dried Tons
THC	Total Hydrocarbons
VOC	Volatile Organic Compounds
C1	Carbon

## Units of Measure

ppm	Parts per million (wet basis)
ppmvd	Parts per million (dry basis)
ppm C <sub>3</sub>	Parts per million as propane
ppm C <sub>1</sub>	Parts per million as carbon
mg	Milligram
kg	Kilogram
µg	Micrograms

## Permit Designations/Titles

Dryer 1	AA-001, 30 MMBTU Wood-Fired Dryer (No. 1) with a Multiclone
Dryer 2	AA-002, 45 MMBTU Wood Fired Dryer (No. 2) with a Cyclone
Dry Hammermill 1	AA-006, No. 1 Secondary Hammermill w/High-Eff. Cyclone
Dry Hammermill 2	AA-007, No. 2 Secondary Hammermill w/High-Eff. Cyclone
Pellet Cooler 1	AA-004, Includes Line 1 Press Aspiration (AA-012)
Pellet Cooler 2	AA-014, Pellet Cooler 2 w/Hi-Efficiency Cyclone
Aspiration System	AA-013, Line 2 Pellet Mill Aspiration System
Green Hammermill	AA-016 (Hammermill Bin)

## Air Emission Test Report Wiggins, Mississippi Wood Pellet Production Facility

### 1. SUMMARY

Enviva Pellets, Wiggins, LLC (Enviva) has sponsored air emission testing to satisfy the requirements of Agreed Order 6366-13 dated June 16, 2013 (the “Order”). These test results are being submitted to the Mississippi Department of Environmental Quality (MDEQ) by October 31, 2013 in accordance with the Order.

The scope of the testing program included volatile organic compounds (VOCs) and six organic hazardous air pollutants (HAPs). Annual emissions of each analyte have been calculated and compared to applicable permit limits. The results of the testing program are summarized in Table 1-1 based on the present maximum permitted production limit of 185,550 ODT per year in the permit.

Analyte	Dryer 1	Dryer 2	Dry Hammermill 2	Green Hammermill	Pellet Cooler 1	Pellet Cooler 2	Aspirator	Dry Hammermill 1	Total
Total VOC	66.3	57.6	11.1	21.1	15.7	7.8	46.4	7.4	233.5
Organic HAPs									
Methanol	1.85	7.26	0.08	0.27	0.16	0.24	0.34	0.05	10.3
Acetaldehyde	0.00	1.40	0.25	0.61	0.39	0.35	0.23	0.17	2.0
Acrolein	1.03	2.32	0.43	1.24	0.77	0.68	0.20	0.29	7.0
Formaldehyde	2.01	3.48	0.39	0.37	0.49	0.34	0.03	0.26	7.4
Phenol	0.00	0.00	0.00	0.00	0.39	0.00	0.00	0.00	0.4
Propionaldehyde	1.06	1.82	0.17	0.09	0.16	0.11	0.00	0.11	3.5
Total HAPS	5.96	14.87	1.32	2.59	2.35	1.72	0.80	0.88	31.89

At the current maximum permitted production limit, VOC emissions remain below the PSD threshold of 250 tons per year. However, HAP emissions exceed the 25 ton per year threshold for major source classification, and methanol exceeds the 10 ton per year single compound threshold for major source classification. Importantly, the plant has never operated at the maximum permitted production limit of 185,550 ODT per year.

Enviva plans to propose to MDEQ a new maximum permitted production limit of 140,000 ODT/year. VOC and HAP emissions based on this proposed maximum permitted production limit are summarized in Table 1-2. Like the current limit of 185,000 ODT/year, to date, the Wiggins plant has also never achieved 140,000 ODT/year.

VOC emissions at the newly proposed production rate limit would be well below the PSD threshold of 250 tons per year. Furthermore, combined HAPs emissions are less than 25 tons per year, and none of the HAPs are emitted at more than 10 tons per year. Because the plant has never achieved a production rate of 140,000 ODT/year, the plant has never exceeded the major source threshold for VOCs or HAPs.

Analyte	Dryer 1	Dryer 2	Dry Hammermill 2	Green Hammermill	Pellet Cooler 1	Pellet Cooler 2	Aspirator	Dry Hammermill 1	Total
Total VOC	50.1	43.4	8.4	15.9	11.7	5.9	35.0	5.6	175.9
Organic HAPs									
Methanol	1.40	5.48	0.06	0.21	0.12	0.18	0.26	0.04	7.7
Acetaldehyde	0.00	1.06	0.19	0.46	0.29	0.26	0.17	0.12	2.6
Acrolein	0.78	1.75	0.33	0.93	0.58	0.51	0.15	0.22	5.3
Formaldehyde	1.52	2.62	0.30	0.28	0.37	0.26	0.03	0.20	5.6
Phenol	0.00	0.00	0.00	0.00	0.29	0.00	0.00	0.00	0.3
Propionaldehyde	0.80	1.37	0.13	0.07	0.12	0.08	0.00	0.08	2.7
Total HAPS	4.50	12.28	0.99	1.95	1.78	1.30	0.61	0.66	24.06

These tests were conducted in accordance with the emission test protocol<sup>[1]</sup> submitted to MDEQ on July 31, 2013. The scope of the emission test program was increased since submittal of the test program protocol in order to ensure that Enviva evaluated emissions from all possible sources of VOCs and HAPs.

The air emission tests were conducted by Air Control Techniques, P.C. using EPA Reference Methods 1, 2, 3, 4, 25A, and 320. The emission tests were conducted from Thursday, October 10 through Sunday, October 13, 2013. This report summarizes the emissions test data, quality assurance data, test method procedures, sampling equipment calibrations, process operating conditions, and test program participants.

## **2. EMISSION TEST PROGRAM DESCRIPTION**

### **2.1 Wiggins, Mississippi Plant Description**

Enviva operates a plant producing wood pellets. The plant consists of a wood receiving yard, log debarkers and chippers, two rotary dryers, two hammermills, two pellet presses and coolers, and an aspiration system. The plant processes wood composed of a range of hardwoods and softwoods.

### **2.2 Purpose and Scope of the Emission Test Program**

Based on a voluntary self-evaluation, Enviva reported to the Mississippi Department of Environmental Quality (MDEQ) that it may have underreported emissions of volatile organic compounds (VOCs) in its permit application. Enviva's concern was based on a set of engineering-oriented tests<sup>[2]</sup> conducted in November 2012 that indicated that VOC emissions from a hammermill source and a press cooler aspiration vent may be higher than previously known. While emissions from specific wood pellet plants are highly dependent on the specific equipment employed and to a lesser degree the hardwood/softwood mix of raw material, Enviva's preliminary findings in the November 2012 engineering test are generally consistent with other recent findings in the Wood Pellet Industry, specifically the engineering-oriented tests<sup>[3]</sup> at a Georgia Biomass, Inc. plant in Waycross, Georgia and Green Circle Bio Energy in Cottondale, Florida.

This air emission testing program is intended to address Enviva's concern and fulfills the requirements of the Order. Specifically, Enviva agreed to generate VOC emissions data for the following sources.

- Dryer 1 multiclone stack
- Dryer 2 cyclone stack
- Secondary Hammermill 2 cyclone outlet
- Pellet Mill 2 Aspiration System

Since signing the Order, Enviva has determined that it would be beneficial to expand the scope of the emission testing program to include these three additional sources.

- Green Hammermill
- Pellet Cooler 1
- Pellet Cooler 2

The tests at Secondary Hammermill 2 cyclone outlet also represent emissions from Secondary Hammermill 1. Secondary Hammermill 2 is identical to Secondary Hammermill 1 except for the larger capacity of Secondary Hammermill 2.

## 2.3 Test Participants

The Enviva project manager for this project was Mr. Michael Doniger, Director of Plant Operations. He was assisted by Mr. Joe Harrell, Environmental Manager, Mr. Mike Jones, and Mr. Gary Williams, Wiggins Plant Manager.

Mr. Mike J. Doniger, Director, Plant Operations  
Enviva, LP  
7200 Wisconsin Avenue, Suite 1000  
Bethesda, Maryland 20814  
Phone: (301) 657 5560 Extension 163  
Email: Michael.Doniger@envivabiomass.com

Mr. Joe Harrell, Environmental Manager  
Enviva, LP  
142 NC Route 561 East  
Ahoskie, NC 27910 USA  
Phone (252) 209-6032, Extension 202  
Email: Joe.Harrell@envivabiomass.com

Mr. Gary Williams, Plant Manager  
Enviva Pellets Wiggins, LLC  
Wiggins, MS  
Email: Gary.Williams@envivabiomass.com

Legal counsel for Enviva is Mr. Alan McConnell. Mr. McConnell participated in this study to ensure that it addressed the requirements of the Order.

Alan McConnell  
Kilpatrick Townsend & Stockton, LLP  
Suite 1400, 4208 Six Forks Road  
Raleigh, North Carolina 27609  
Phone (919) 420-1798  
Email: amcconnell@kilpatricktownsend.com

Enviva retained Air Control Techniques, P.C. to conduct the air emission testing program at the Wiggins plant. The Air Control Techniques, P.C. project manager was John Richards, Ph.D., P.E, QSTI. He was assisted by David Goshaw, P.E., QSTI, Todd Brozell, P.E., QSTI, and Jonas Gilbert. Tom Holder, QSTI provided quality assurance services for the test program. Contact information for Air Control Techniques, P.C. includes the following.

Air Control Techniques, P.C.  
301 East Durham Road  
Durham, N.C. 27513  
Phone: (919) 460-7811  
John Richards (john.richards@aircontroltechniques.com)  
David Goshaw (dave.goshaw@aircontroltechniques.com)  
Todd Brozell (todd.brozell@aircontroltechniques.com)  
Jonas Gilbert (jonas.gilbert@aircontroltechniques.com)  
Tom Holder (tom.holder@aircontroltechniques.com)

Enthalpy, Inc. provided the laboratory analyses of the samples. The Enthalpy project manager for this project was Mr. Bryan Tyler. He was assisted by Dr. Grant Plummer, Mr. Clint Thrasher, and Mr. Steve Eckert, President.

Enthalpy Analytical, Inc.  
800 Capitola Drive  
Durham, North Carolina 27713  
Phone: (919) 850-4392, Extension 250  
Email: Bryan.tyler@enthalpyanalytical.com

### 3. TEST MATRIX AND TEST RESULTS

#### 3.1 Test Matrix

Table 3-1 summarizes the test program analytes, sampling methods, and analytical methods used for the seven sources listed in Section 1.1

Analyte	Test Method	Number of Runs	Run Length	Analytical Method
Acetaldehyde, Acrolein, Formaldehyde, Methanol, Phenol, Propionaldehyde	EPA Method 320	3	60 min	FTIR
Gas Flow	EPA Method 2	3	60 min	Manometer
Gas Molecular Weight, Oxygen, Carbon Dioxide	EPA Method 3	3	60 min	Fyrite® Analyzer
Gas Moisture	EPA Method 4	3	60 min	Gravimetric
Total Hydrocarbons (THC)	EPA Method 25A	3	60 min	FID

The tests were conducted on Thursday, October 10 through Sunday October 13, 2013. During all of the tests, the plant operated with a 60% softwood/40% hardwood feed.

#### 3.2 Test Results

The VOC and organic HAP test results and calculated annual emission rates are summarized in Tables 3-2 through 3-8. VOC and HAP emissions were measured simultaneously at each of the seven emission units tested.

The VOC emissions have been calculated based on the total hydrocarbon data provided by Method 25A. The Method 25A data have been converted from a wet to a dry basis to account for the moisture in the stack gas stream. Total hydrocarbon concentrations (THC) has been used as a surrogate for VOCs.

The VOC emission calculations do not include any corrections for methane, ethane, or acetone despite the fact that these compounds are detected by Method 25A but are not classified as VOCs. Accordingly, the reported VOC emissions are biased to higher-than-true levels to the extent that these three compounds affected the Method 25A results.

The Method 25A data reflect the combined THC concentrations consisting of (1) alpha and beta pinene, (2) numerous other terpenes such as limonene and 3-carene, and (3) the organic HAPs. The organic HAP emissions discussed later in this report are also classified as VOCs and represent a small fraction of the total VOC emissions reported.

Method 320 was used to measure six organic compounds. Several of the organic compounds were below the detection limits of Method 320 in this matrix of gaseous constituents. These non-detection concentrations are designated by shading in Tables 3-2 through 3-8.

Parameter	Run 1	Run 2	Run 3	Average
Date	10/10/2013	10/10/2013	10/10/2013	N/A
Start	9:17	10:36	11:50	N/A
Stop	10:17	11:36	12:50	N/A
Throughput, tons/hour	36	36	36	36.0
Moisture Content Outlet, %wt.	47.15	47.15	47.15	47.2
Throughput, ODT/hour	19.026	19.026	19.026	19.0
ACFM	27,642	27,273	27,189	27,368.0
DSCFM	25,184	24,803	25,031	25,006
Stack Temperature, °F	70.8	70.6	70.9	70.8
O <sub>2</sub> , %	20.9	20.9	20.9	20.9
% Moisture	3.41	3.62	2.37	3.1
VOC, ppmvd as Propane	31.9	33.4	27	30.8
VOC, ppmvd as C1	95.7	100.3	81.1	92.4
VOC, lbs/hour as C1	4.5	4.7	3.8	4.3
VOC, lbs/ODT	0.24	0.25	0.20	0.2
Methanol, ppmvd	0.53	0.48	0.39	0.46
Acetaldehyde, ppmvd	0.79	0.75	0.74	0.76
Acrolein, ppmvd	1.17	1.25	1.18	1.20
Formaldehyde, ppmvd	0.77	0.65	0.57	0.66
Phenol, ppmvd	0.91	0.91	0.90	0.91
Propionaldehyde, ppmvd	0.24	0.24	0.26	0.247
Methanol, lbs/hour	0.066	0.060	0.049	0.058
Acetaldehyde, lbs/hour	0.136	0.129	0.127	0.131
Acrolein, lbs/hour	0.257	0.274	0.259	0.263
Formaldehyde, lbs/hour	0.090	0.077	0.068	0.078
Phenol, lbs/hour	0.000	0.000	0.000	0.000
Propionaldehyde, lbs/hour	0.000	0.000	0.058	0.019
Methanol, lbs/ODT	0.003	0.003	0.002	0.003
Acetaldehyde, lbs/ODT	0.007	0.007	0.006	0.007
Acrolein, lbs/ODT	0.013	0.014	0.013	0.013
Formaldehyde, lbs/ODT	0.005	0.004	0.003	0.004
Phenol, lbs/ODT	0.000	0.000	0.000	0.000
Propionaldehyde, lbs/ODT	0.000	0.000	0.003	0.001

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Table 3-3. Dryer 1 Emissions <sup>1</sup> Emission Test Results				
Parameter	Run 1	Run 2	Run 3	Average
Date	10/10/2013	10/11/2013	10/11/2013	N/A
Start	17:38	10:00	11:37	N/A
Stop	18:38	11:00	12:37	N/A
Throughput, tons/hour	8.5	8.45	9	8.7
Moisture Content Outlet, %wt.	15.5	14.36	18.9	16.3
Throughput, ODT/hour	7.18	7.24	7.30	7.2
ACFM	44,448	42,243	42,593	43,095
DSCFM	32,404	31,700	31,215	31,773
Stack Temperature, °F	146.3	150.1	147.3	147.9
O <sub>2</sub> , %	19.0	17.0	17.0	17.7
% Moisture	16.07	12.79	15.23	14.7
VOC, ppmvd as Propane	79.5	71	67.4	72.6
VOC, ppmvd as C1	238.8	213.3	202.6	218.2
VOC, lbs/hour as C1	14.4	12.6	11.8	12.93
VOC, lbs/ODT	2.00	1.74	1.62	1.79
Methanol, ppmvd	3.00	1.95	1.88	2.28
Acetaldehyde, ppmvd	1.51	1.46	1.50	1.49
Acrolein, ppmvd	2.13	1.97	2.03	2.04
Formaldehyde, ppmvd	3.96	1.83	2.10	2.63
Phenol, ppmvd	2.43	2.34	2.41	2.39
Propionaldehyde, ppmvd	0.76	0.81	0.59	0.72
Methanol, lbs/hour	0.483	0.308	0.292	0.36
Acetaldehyde, lbs/hour	0.0	0.0	0.0	0.000
Acrolein, lbs/hour	0.598	0.0	0.0	0.199
Formaldehyde, lbs/hour	0.597	0.272	0.307	0.392
Phenol, lbs/hour	0.0	0.0	0.0	0.000
Propionaldehyde, lbs/hour	0.222	0.233	0.167	0.207
Methanol, lbs/ODT	0.067	0.043	0.040	0.050
Acetaldehyde, lbs/ODT	0.0	0.0	0.0	0.000
Acrolein, lbs/ODT	0.083	0.0	0.0	0.028
Formaldehyde, lbs/ODT	0.083	0.038	0.042	0.054
Phenol, lbs/ODT	0.0	0.0	0.0	0.000
Propionaldehyde, lbs/ODT	0.031	0.032	0.023	0.029

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Parameter	Run 1	Run 2	Run 3	Average
Date	10/12/2013	10/12/2013	10/12/2013	N/A
Start	8:58	10:22	11:41	N/A
Stop	9:58	11:22	12:41	N/A
Throughput, tons/hour	4	4	4	4.0
Moisture Content Outlet, %wt.	7.9	7.9	7.9	7.9
Throughput, ODT/hour	3.68	3.68	3.68	3.68
ACFM	16,168	16,246	16,134	16,182.7
DSCFM	15,189	14,870	14,825	14,961
Stack Temperature, °F	82.3	94.8	97.7	91.6
O <sub>2</sub> , %	20.9	20.9	20.9	20.9
% Moisture	3.35	3.68	2.79	3.27
VOC, ppmvd as Propane	40.4	34.6	36.7	37.2
VOC, ppmvd as C1	121.2	103.8	110.1	111.7
VOC, lbs/hour as C1	3.44	2.88	3.05	3.12
VOC, lbs/ODT	0.93	0.78	0.83	0.85
Methanol, ppmvd	0.56	0.34	0.36	0.42
Acetaldehyde, ppmvd	0.71	0.73	0.78	0.74
Acrolein, ppmvd	1.01	1.06	1.39	1.15
Formaldehyde, ppmvd	1.49	1.30	1.30	1.36
Phenol, ppmvd	1.03	1.02	1.01	1.02
Propionaldehyde, ppmvd	0.39	0.30	0.25	0.31
Methanol, lbs/hour	0.042	0.026	0.027	0.032
Acetaldehyde, lbs/hour	0.074	0.076	0.081	0.077
Acrolein, lbs/hour	0.135	0.141	0.184	0.153
Formaldehyde, lbs/hour	0.105	0.092	0.092	0.096
Phenol, lbs/hour	0.2	0.0	0.0	0.077
Propionaldehyde, lbs/hour	0.054	0.041	0.000	0.032
Methanol, lbs/ODT	0.011	0.007	0.007	0.009
Acetaldehyde, lbs/ODT	0.020	0.021	0.022	0.021
Acrolein, lbs/ODT	0.037	0.038	0.050	0.042
Formaldehyde, lbs/ODT	0.029	0.025	0.025	0.026
Phenol, lbs/ODT	0.063	0.000	0.0	0.021
Propionaldehyde, lbs/ODT	0.015	0.011	0.000	0.009

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Parameter	Run 1	Run 2	Run 3	N/A
Date	10/13/2013	10/13/2013	10/13/2013	N/A
Start	9:21	11:14	12:31	N/A
Stop	10:21	12:52	13:47	N/A
Throughput, tons/hour	14.5	11.2	11.3	12.3
Moisture Content Outlet, %wt.	18.5	13.45	13.75	15.2
Throughput, ODT/hour	11.82	9.69	9.75	10.4
ACFM	24,998	25,318	25,278	25,198.0
DSCFM	14,745	15,224	14,842	14,937
Stack Temperature, °F	174.3	154.9	171.8	167.0
O <sub>2</sub> , %	16.5	17	17	16.8
% Moisture	29.04	29.86	29.64	29.5
VOC, ppmvd as Propane	129.4	115.8	138.1	127.8
VOC, ppmvd as C1	388.2	347.4	414.3	383.3
VOC, lbs/hour as C1	10.70	9.88	11.49	10.69
VOC, lbs/ODT	0.91	1.02	1.18	1.03
Methanol, ppmvd	26.5	14.5	15.3	18.795
Acetaldehyde, ppmvd	1.4	4.7	1.4	2.498
Acrolein, ppmvd	2.7	3.7	3.5	3.303
Formaldehyde, ppmvd	9.0	9.4	9.6	9.336
Phenol, ppmvd	3.9	4.0	4.0	3.944
Propionaldehyde, ppmvd	3.3	2.0	2.4	2.575
Methanol, lbs/hour	1.949	1.070	1.129	1.383
Acetaldehyde, lbs/hour	0.138	0.473	0.147	0.253
Acrolein, lbs/hour	0.345	0.476	0.456	0.425
Formaldehyde, lbs/hour	0.622	0.647	0.662	0.644
Phenol, lbs/hour	0.0	0.0	0.0	0.000
Propionaldehyde, lbs/hour	0.445	0.262	0.322	0.343
Methanol, lbs/ODT	0.165	0.110	0.116	0.130
Acetaldehyde, lbs/ODT	0.012	0.049	0.015	0.025
Acrolein, lbs/ODT	0.029	0.049	0.047	0.042
Formaldehyde, lbs/ODT	0.053	0.067	0.068	0.062
Phenol, lbs/ODT	0.0	0.0	0.0	0.000
Propionaldehyde, lbs/ODT	0.038	0.027	0.033	0.033

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Parameter	Run 1	Run 2	Run 3	Average
Date	10/11/2013	10/11/2013	10/11/2013	N/A
Start	18:11	19:35	20:48	N/A
Stop	19:11	20:35	21:48	N/A
Throughput, tons/hour	11.18	11.22	11.12	11.2
Moisture Content Outlet, %wt.	10.2	10.3	10.2	10.2
Throughput, ODT/hour	10.04	10.06	9.99	10.0
ACFM	15,197	14,385	15,165	14,916
DSCFM	13,183	12,366	13,303	12,951
Stack Temperature, °F	122.4	128.4	116.4	122.4
O <sub>2</sub> , %	20.9	20.9	20.9	20.9
% Moisture	4.25	4.18	4.18	4.20
VOC, ppmvd as Propane	26.3	31.0	25.5	27.6
VOC, ppmvd as C1	78.9	93	76.5	82.8
VOC, lbs/hour as C1	1.94	2.15	1.90	2.00
VOC, lbs/ODT	0.19	0.21	0.19	0.20
Methanol, ppmvd	0.20	0.22	0.21	0.21
Acetaldehyde, ppmvd	0.75	0.74	0.74	0.74
Acrolein, ppmvd	1.02	1.02	1.01	1.02
Formaldehyde, ppmvd	1.09	1.19	1.16	1.14
Phenol, ppmvd	1.13	1.13	1.13	1.13
Propionaldehyde, ppmvd	0.24	0.25	0.27	0.254
Methanol, lbs/hour	0.013	0.014	0.014	0.014
Acetaldehyde, lbs/hour	0.067	0.067	0.000	0.045
Acrolein, lbs/hour	0.118	0.118	0.000	0.078
Formaldehyde, lbs/hour	0.067	0.073	0.071	0.071
Phenol, lbs/hour	0.000	0.000	0.000	0.000
Propionaldehyde, lbs/hour	0.029	0.030	0.032	0.030
Methanol, lbs/ODT	0.001	0.001	0.001	0.0014
Acetaldehyde, lbs/ODT	0.007	0.007	0.000	0.0045
Acrolein, lbs/ODT	0.012	0.012	0.000	0.0078
Formaldehyde, lbs/ODT	0.007	0.007	0.007	0.0070
Phenol, lbs/ODT	0.000	0.000	0.000	0.0000
Propionaldehyde, lbs/ODT	0.003	0.003	0.003	0.0030

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Parameter	Run 1	Run 2	Run 3	Average
Date	10/11/2013	10/11/2013	10/11/2013	N/A
Start	13:43	15:08	16:39	N/A
Stop	14:43	16:08	17:39	N/A
Throughput, tons/hour	15.0	15.0	15.0	15.0
Moisture Content Outlet, %wt.	7.12	7.36	7.17	7.2
Throughput, ODT/hour	13.93	13.90	13.92	13.9
ACFM	13,252	12,718	12,831	12,934
DSCFM	10,938	10,543	10,488	10,656
Stack Temperature, °F	148.9	143.2	152.3	148.1
O <sub>2</sub> , %	20.9	20.9	20.9	20.9
% Moisture	4.86	4.64	4.54	4.68
VOC, ppmvd as Propane	25.0	22.3	26.0	24.4
VOC, ppmvd as C1	75	66.9	78	73.3
VOC, lbs/hour as C1	1.53	1.32	1.53	1.46
VOC, lbs/ODT	0.11	0.09	0.11	0.10
Methanol, ppmvd	0.84	0.71	0.88	0.81
Acetaldehyde, ppmvd	0.90	0.87	0.83	0.87
Acrolein, ppmvd	1.36	1.27	1.39	1.34
Formaldehyde, ppmvd	1.12	0.69	1.93	1.25
Phenol, ppmvd	1.14	1.13	1.13	1.13
Propionaldehyde, ppmvd	0.26	0.26	0.38	0.30
Methanol, lbs/hour	0.046	0.039	0.048	0.044
Acetaldehyde, lbs/hour	0.068	0.065	0.062	0.065
Acrolein, lbs/hour	0.130	0.121	0.133	0.128
Formaldehyde, lbs/hour	0.058	0.035	0.099	0.064
Phenol, lbs/hour	0	0	0	0.000
Propionaldehyde, lbs/hour	0.026	0.000	0.037	0.021
Methanol, lbs/ODT	0.003	0.003	0.003	0.003
Acetaldehyde, lbs/ODT	0.005	0.005	0.004	0.005
Acrolein, lbs/ODT	0.009	0.009	0.010	0.009
Formaldehyde, lbs/ODT	0.004	0.003	0.007	0.005
Phenol, lbs/ODT	0.0	0.0	0.0	0.000
Propionaldehyde, lbs/ODT	0.002	0.000	0.003	0.002

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Parameter	Run 1	Run 2	Run 3	Average
Date	10/12/2013	10/12/2013	10/12/2013	N/A
Start	15:09	16:36	18:00	N/A
Stop	16:09	17:36	19:00	N/A
Throughput, tons/hour	15	15	15	15.0
Moisture Content Outlet, %wt.	7.12	8.83	7.85	7.93
Throughput, ODT/hour	13.93	13.68	13.82	13.8
ACFM	1,756	1,692	1,624	1,691
DSCFM	1,079	1,016	985	1,027
Stack Temperature, °F	148.6	148.3	152.1	149.7
O <sub>2</sub> , %	20.9	20.9	20.9	20.9
% Moisture	27.67	29.33	28.19	28.4
VOC, ppmvd as Propane	1485.8	1354.2	1671.1	1,503.7
VOC, ppmvd as C1	4457.4	4062.6	5013.3	4,511.1
VOC, lbs/hour as C1	8.99	7.71	9.23	8.64
VOC, lbs/ODT	0.65	0.56	0.67	0.63
Methanol, ppmvd	11.5	12.6	11.4	11.81
Acetaldehyde, ppmvd	6.4	5.5	5.2	5.73
Acrolein, ppmvd	4.4	4.4	3.1	3.97
Formaldehyde, ppmvd	1.5	2.2	1.5	1.72
Phenol, ppmvd	3.8	3.9	3.8	3.81
Propionaldehyde, ppmvd	4.1	4.2	4.2	4.19
Methanol, lbs/hour	0.062	0.068	0.061	0.064
Acetaldehyde, lbs/hour	0.048	0.041	0.039	0.042
Acrolein, lbs/hour	0.041	0.042	0.030	0.037
Formaldehyde, lbs/hour	0.000	0.011	0.007	0.006
Phenol, lbs/hour	0.000	0.000	0.000	0.000
Propionaldehyde, lbs/hour	0.000	0.000	0.000	0.000
Methanol, lbs/ODT	0.004	0.005	0.004	0.005
Acetaldehyde, lbs/ODT	0.003	0.003	0.003	0.003
Acrolein, lbs/ODT	0.003	0.003	0.002	0.003
Formaldehyde, lbs/ODT	0.000	0.001	0.001	0.000
Phenol, lbs/ODT	0.000	0.000	0.000	0.000
Propionaldehyde, lbs/ODT	0.000	0.000	0.000	0.000

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

### 3.3 Emissions Data Evaluation

#### Method 25A VOC Concentrations

The VOC emissions from the various process units ranged from 0.10 to 1.79 pounds per ODT. VOC emissions were highest from the two dryers.

Dryer 1 had an emission rate of 1.79 pounds per ODT, and Dryer 2 had an emission rate of 1.03 pounds per ODT. This is equivalent to a 79% difference despite the fact that the dryers were handling similar hardwood/softwood blends and were generating wood with similar outlet moisture levels. The dryer outlet temperatures were also similar. These data clearly demonstrate that VOC emissions from the dryers are due to two factors: (1) the performance of the wood waste burner supplying the heat to the dryer, and (2) volatilization of VOCs from the wood in the dryer. Of these two sources, contributions of the burner are most important.

Due to the dominance of the burner in establishing the VOC emission rates from the combined burner/dryer source, the importance of the hardwood/softwood ratio is less important than previously thought. Changes in the hardwood/softwood ratio do not necessarily affect the VOC emissions from the burner.

The emissions of organic HAP compounds are not sensitive to the hardwood/softwood ratio. The data summarized in the Phase I report indicate that emissions of organic HAPs decreased slightly as the softwood content increased from 10% to 100%.

The data summarized in Tables 3-2 through 3-8 indicate that the total VOC emissions from the Wiggins Plant exceed 100 tons per year calculated as carbon. These tests confirm that the plant is a major source for VOCs.

The accuracy of the VOC data is demonstrated by a Method 25A response factor of approximately 1 for the group of compounds present in the gas stream. The Method 25A response is expressed in terms of a response factor that is defined as the observed Method 25A concentration divided by the true concentration. The Method 25A FID has a response factor close to 1.0 for a large set of organic compounds. Some high molecular weight organics have a response factor larger than 1, and in some cases, approaching 1.5. For these compounds, Method 25A is biased to higher-than-true concentrations. Some low molecular weight highly oxygenated organic compounds such as methanol and formaldehyde have very low response factors in the range of 0.1 to 0.4. For these compounds, Method 25A is biased to lower-than-true concentrations.

As part of the laboratory tests reported to MDEQ in Enviva's Phase I emission study dated July 31, 2013<sup>[4]</sup> (the "Phase I Study"). Air Control Techniques, P.C. has taken the following two independent approaches in assessing the Method 25A response factors: (1) direct measurement of the Method 25A response factor using an alpha-pinene gas standard, the dominant organic compound measured during the laboratory tests and (2) a comparison of the Method 25A concentration data with the summed concentrations of all of the specific organics measured simultaneously using NCASI Method 98.01 and EPA Method 18. The results of these response factor analyses are presented in Tables 3-9 and 3-10.

Table 3-9. Alpha-Pinene Method 25A Response Factor <sup>1</sup>	
Alpha-Pinene Gas Standard, as C <sub>10</sub> H <sub>16</sub>	259 ppm
Alpha-Pinene Gas Standard, as C <sub>3</sub>	863 ppm
FID Response, as C <sub>3</sub>	888 ppm
Response Factor as C <sub>3</sub>	1.03

1. Note: This table was included in the Phase I Study report to MDEQ.

Table 3-10. Calculated Method 25A Response Factors in Phase I Laboratory Tests <sup>1</sup>					
Run	Process Type	Softwood Content, %	Method 25A versus Combined NCASI 98.01 and Method 18	Dominant Compounds	Other Important Compounds
4	Dryer	10	0.72	$\alpha$ -and $\beta$ -Pinene	Acetone, Methanol
5	Dryer	10	0.70	$\alpha$ -and $\beta$ -Pinene	Acetone, Methanol
6	Dryer	10	0.75	$\alpha$ -and $\beta$ -Pinene	Methanol, Formaldehyde
21	Dryer	10	1.23	$\alpha$ -and $\beta$ -Pinene	Acetone, Methanol
22	Press	10	1.05	$\alpha$ -and $\beta$ -Pinene	Acetone, Methanol
7	Dryer	70	0.85	$\alpha$ -and $\beta$ -Pinene	Acetone
8	Dryer	70	0.90	$\alpha$ -and $\beta$ -Pinene	Acetone
9	Dryer	70	1.02	$\alpha$ -and $\beta$ -Pinene	Acetone
10	Dryer	70	0.91	$\alpha$ -and $\beta$ -Pinene	Acetone
24	Press	70	1.51	$\alpha$ -and $\beta$ -Pinene	Acetone, Methanol
11	Dryer	100	0.99	$\alpha$ -and $\beta$ -Pinene	Acetone
12	Dryer	100	0.96	$\alpha$ -and $\beta$ -Pinene	Acetone
13	Dryer	100	0.85	$\alpha$ -and $\beta$ -Pinene	Acetone
14	Dryer	100	0.87	$\alpha$ -and $\beta$ -Pinene	Acetone
16	Dryer	100	1.09	$\alpha$ -and $\beta$ -Pinene	Methanol, Acetone
19	Dryer	100	1.21	$\alpha$ -and $\beta$ -Pinene	Methanol, Acetone
20	Press	100	1.13	$\alpha$ -and $\beta$ -Pinene	Methanol, Acetone
Test Program Average			0.98		

1. Note: This table was included in the Phase I Study report to MDEQ.

The excellent agreement between the Method 25A total concentration and the combined concentrations of all of the organics measured by NCASI 98.01 and EPA Method 18 demonstrate that Method 25A is an appropriate VOC measurement technique for wood pellet production facilities.

### Method 320 HAP Concentrations

At the maximum permitted production limit of 185,550 ODT per year, five of the six organic HAP compounds measured by Method 320 were each emitted at a rate less than 10 tons per year. The methanol emission rate at this production level was 11.0 tons per year. The combined emission rate of all six organic HAPs was slightly over 31.1 tons per year at the maximum permitted production rate.

The list of HAPs specifically included in the test protocol included methanol, acetaldehyde, acrolein, formaldehyde, phenol, and propionaldehyde. This list was compiled based on (1) the organic compounds identified in laboratory analyses of pellet production facilities emissions, (2) previous emission tests conducted in the Pellet Manufacturing Industry, and (3) organic HAPs identified in studies of other wood products industries—specifically, MDF production.

The results of this test program indicate that this list of HAPs compounds needs to be amended. Phenol was detected at low concentration in only one of the tests of the seven process units. Furthermore, propionaldehyde was not detected in most of the tests.

The low to non-detectable phenol emissions data are consistent with the results of the Phase I Study. Phenol was not identified at detectable concentrations in any of the laboratory studies summarized in the Phase I Study report. The emission rates of phenol reported in the November 2012 Wiggins report <sup>[2]</sup> ranged from 0.0002 to 0.0018 pounds per hour—all insignificant emission rates. Phenol was also not listed in previous emission tests reviewed in preparation for this test program. Phenol was included in the test protocol primarily because other researchers such as Beauchemin and Tampier, <sup>[5]</sup> Milot, <sup>[6]</sup> and Milot and Mosher <sup>[7]</sup> listed phenol due to its inclusion in tests conducted at MDF and particleboard facilities. However, phenol emissions in MDF and particleboard production are due to the use of phenolic resins and similar binders. There is no reason to expect any appreciable phenol formation in pellet production considering (1) the lack of binders of any type in pellet production, (2) the higher moisture levels in pellet production as compared to MDF and particleboard processes, and (3) the lower material temperatures in pellet process equipment. Air Control Techniques, P.C. has assigned zero values to non-detected concentrations.

Acetaldehyde, propionaldehyde, and acrolein had very low concentrations in most of the emission tests summarized in this report. The IR absorption spectra of both water and the terpene compounds overlap the absorption spectra of acetaldehyde, propionaldehyde, and acrolein. Accordingly, the reported concentrations of these three compounds are biased to higher-than-true levels to the extent that this interference could not be avoided by Method 320 spectral absorption modeling. Zero values have been assigned when these concentrations were below detection limits of Method 320 due, in part, to the interference bias.

The use of zero values for non-detected compounds is an appropriate approach for any source, such as pellet production, where there are a few dominant compounds (i.e. methanol and formaldehyde) and a large number of possible compounds at extremely low levels such as phenol, acetaldehyde, and propionaldehyde. The use of non-detect or one-half non-detect concentrations in emission calculations for a large number of compounds potentially present at trace levels inherently makes any source “major” regardless of the actual emissions, size, or operations characteristics of the emission unit.

### **3.4 VOC and Organic HAP Emission Summary**

Table 3-11 summaries annual emissions of VOC and organic HAP compounds. The annual emission rates are based on operation at the permit limited production rate of 185,550 ODT.

As discussed, the plant has never operated at the maximum permitted production limit of 185,550 ODT per year. The VOC and HAP emissions based on the newly proposed maximum production rate of 140,000 ODT/year are summarized in Table 3-12.

The VOC emissions at the lower production rate are well below the PSD threshold of 250 tons per year. The combined HAPs emissions are less than 25 tons per year, and none of the HAPs are emitted at more than 10 tons per year. Accordingly, at this production limit, the plant is not above the major source threshold for HAPs.

Analyte	Dryer 1	Dryer 2	Dry Hammermill 2	Green Hammermill	Pellet Cooler 1	Pellet Cooler 2	Aspirator	Dry Hammermill 1	Total
Total VOC	66.3	57.6	11.1	21.1	15.7	7.8	46.4	7.4	233.5
Organic HAPs									
Methanol	1.85	7.26	0.08	0.27	0.16	0.24	0.34	0.05	10.3
Acetaldehyde	0.00	1.40	0.25	0.61	0.39	0.35	0.23	0.17	2.0
Acrolein	1.03	2.32	0.43	1.24	0.77	0.68	0.20	0.29	7.0
Formaldehyde	2.01	3.48	0.39	0.37	0.49	0.34	0.03	0.26	7.4
Phenol	0.00	0.00	0.00	0.00	0.39	0.00	0.00	0.00	0.4
Propionaldehyde	1.06	1.82	0.17	0.09	0.16	0.11	0.00	0.11	3.5
Total HAPS	5.96	14.87	1.32	2.59	2.35	1.72	0.80	0.88	31.89

Analyte	Dryer 1	Dryer 2	Dry Hammermill 2	Green Hammermill	Pellet Cooler 1	Pellet Cooler 2	Aspirator	Dry Hammermill 1	Total
VOC Total	50.1	43.4	8.4	15.9	11.7	5.9	35.0	5.6	175.9
Organic HAPs									
Methanol	1.40	5.48	0.06	0.21	0.12	0.18	0.26	0.04	7.7
Acetaldehyde	0.00	1.06	0.19	0.46	0.29	0.26	0.17	0.12	2.6
Acrolein	0.78	1.75	0.33	0.93	0.58	0.51	0.15	0.22	5.3
Formaldehyde	1.52	2.62	0.30	0.28	0.37	0.26	0.03	0.20	5.6
Phenol	0.00	0.00	0.00	0.00	0.29	0.00	0.00	0.00	0.3
Propionaldehyde	0.80	1.37	0.13	0.07	0.12	0.08	0.00	0.08	2.7
Total HAPS	4.50	12.28	0.99	1.95	1.78	1.30	0.61	0.66	24.06

## 4. SAMPLING LOCATIONS

### 4.1 Dryer # 1 Stack Sampling Location

The Dryer 1 sampling location meets EPA Method 1 location requirements as indicated in Figure 4-1. Twelve sampling points were used to measure the gas flow rate.

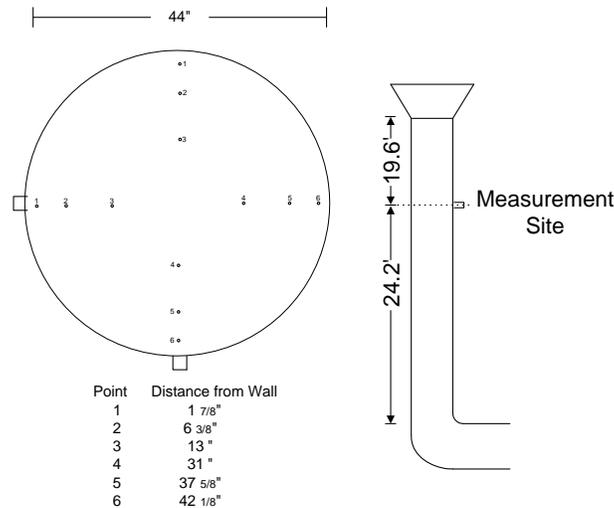


Figure 4-1 Dryer # 1 Stack Sampling Location

The downstream<sup>1</sup> flow disturbance is the stack discharge. The upstream flow disturbance is the duct from the fan entering the base of the stack.

During the sampling program, only the port facing south was used. The port facing east was blocked by the stack support equipment and the Dry Hammermill 1 ductwork. Test personnel reached all of the sampling ports by angling the probe inserted through the south port.

No cyclonic flow conditions were observed in the Dryer 1 stack. The point-by-point cyclonic flow checks indicated an average flow angle 3.1 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Dryer 1 stack is shown in Figure 4-2.



Figure 4-2. Photograph of the Dryer 1 Stack

<sup>1</sup> “Upstream” and “downstream” are defined based on the sampling location as the reference point.

## 4.2 Dryer 2 Stack Sampling Location

The Dryer 2 sampling location meets EPA Method 1 location requirements as indicated in Figure 4-2. Twelve sampling points were used to measure the gas flow rate.

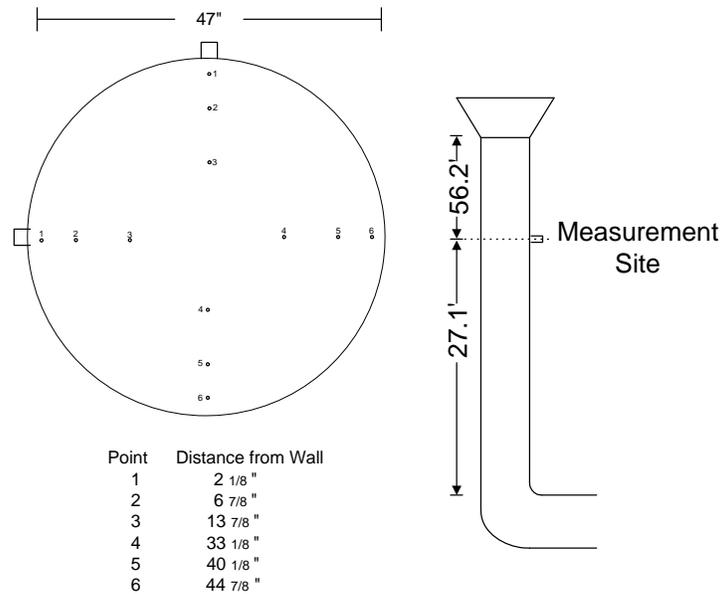


Figure 4-3. Dryer # 2 Stack Sampling Location

The downstream flow disturbance is the stack discharge. The upstream flow disturbance is the duct from the fan entering the base of the stack.

During the sampling program, only the port facing west was used in the test program. The port facing north could not be reached without potentially interrupting operation of the CEM sampling equipment. Test personnel reached all of the sampling ports by angling the probe inserted through the west port.

No cyclonic flow conditions were observed in the Dryer 2 stack. The point-by-point cyclonic flow checks indicated an average flow angle 2.4 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Dryer 2 stack is shown in Figure 4-4.



Figure 4-4. Photograph of the Dryer 2 Stack

### 4.3 Dry Hammermill 2 Cyclone Outlet Sampling Location

The Dry Hammermill 2 sampling location meets EPA Method 1 location requirements as indicated in Figure 4-5. Twelve sampling points were used to measure the gas flow rate.

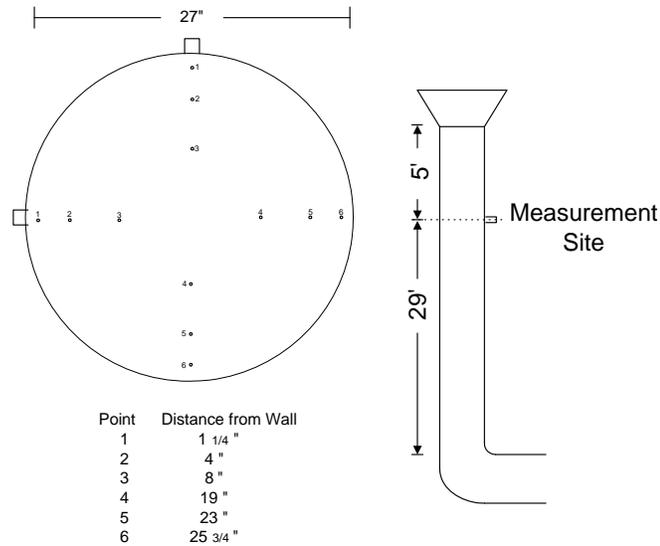


Figure 4-5. Dry Hammermill 2 Sampling Location

The downstream flow disturbance is an elbow in the fan outlet duct. The upstream flow disturbance is the fan discharge. During the sampling program both ports were accessible.

No cyclonic flow conditions were observed in the Dry Hammermill 2 stack. The point-by-point cyclonic flow checks indicated an average flow angle of 0.6 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Dry Hammermill 2 stack is shown in Figure 4-6.



Figure 4-6. Photograph of the Dry Hammermill 2 Sampling Location

#### 4.4 Pellet Mill Aspiration System Sampling Location

The Pellet Mill Aspiration System has a six-inch diameter. Gas flow rate sampling was performed in general accordance with EPA Method 1A. The sampling port location met EPA Method 1 location requirements as indicated in Figure 4-7. A total of eight sampling points were used—four in a horizontal direction and four reached by an angled probe in the vertical direction. Due to the position of the duct and surrounding equipment, it was not possible to sample from any orientation except horizontal.

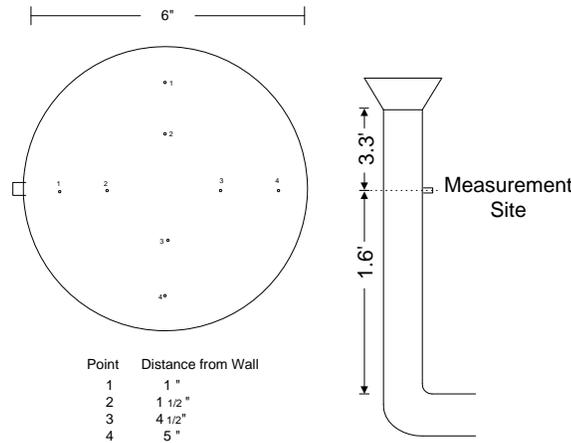


Figure 4-7. Pellet Mill Aspiration System Sampling Location

The upstream flow disturbance was an entry duct from Pellet Mill 6. The downstream flow disturbance was the fan inlet.

No cyclonic flow conditions were observed in the Pellet Mill Aspiration System outlet duct. The point-by-point cyclonic flow checks indicated an average flow angle of 0.75 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Pellet Mill Aspiration System sampling location is shown in Figure 4-8.



Figure 4-8. Photograph of the Pellet Mill Aspiration System Sampling Location

### 4.5 Pellet Mill 2 Cooler Stack Sampling Location

The Pellet Mill 2 Cooler stack sampling location meets the minimum requirements specified in Method 1, Section 11.1. As indicated in Figure 4-9, the downstream<sup>2</sup> disturbance (stack exit) is 0.6 stack diameters from the sampling location. The minimum allowed by Method 1 is 0.5 stack diameters. The upstream flow disturbance was the fan outlet duct. The distance to the upstream flow disturbance meets Method 1 requirements. Both sampling ports were used in the test program.

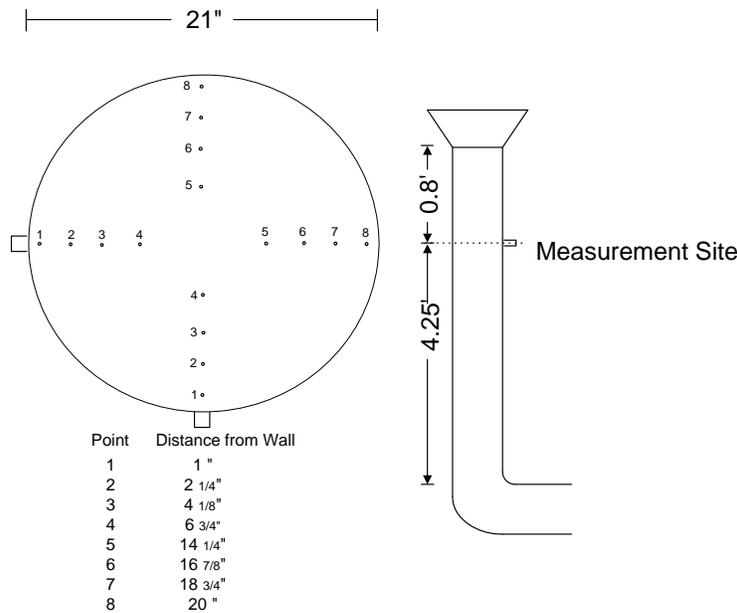


Figure 4-9. Pellet Mill 2 Cooler Stack Sampling Location

No cyclonic flow conditions were observed in the Pellet Mill 2 Cooler stack. The point-by-point cyclonic flow checks indicated an average flow angle of 1.5 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Pellet Cooler 2 stack is shown in Figure 4-10



Figure 4-10. Photograph of the Pellet Cooler 2 Stack

<sup>2</sup> The terms “upstream” and “downstream” are defined based on the test location as the reference point. A recent change in a figure in EPA Method 1 has these terms incorrectly stated.

#### 4.6 Pellet Mill 1 Cooler Stack

The Pellet Mill 1 Cooler stack sampling location meets the minimum requirements specified in Method 1, Section 11.1. As indicated in Figure 4-11, the downstream disturbance (stack exit) is 0.6 stack diameters from the sampling location. The minimum allowed is 0.5 stack diameters. The upstream flow disturbance is the fan outlet duct. The distance to the upstream flow disturbance meets Method 1 requirements. Four of the six sampling ports were used in the test program. The plugs in two of the ports could not be removed.

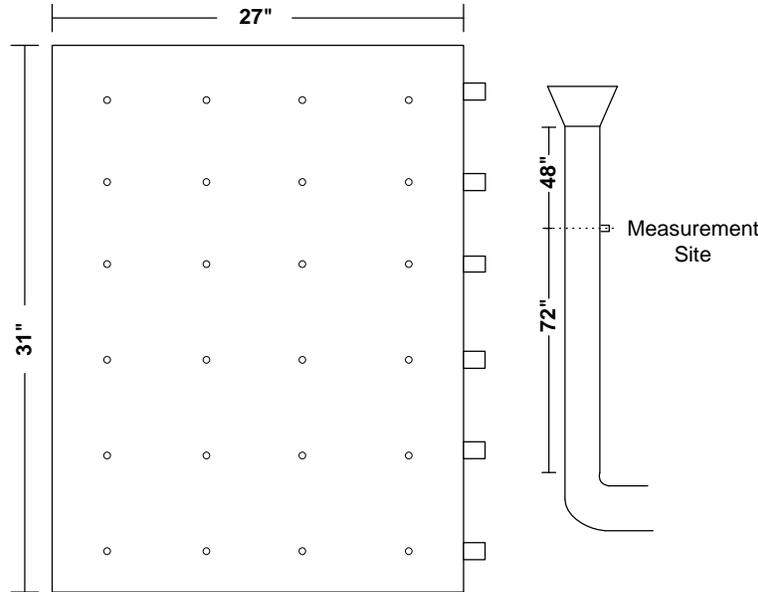


Figure 4-11. Pellet Mill 1 Cooler Stack Sampling Location

No cyclonic flow conditions were observed in the Pellet Mill 1 Cooler stack. The point-by-point cyclonic flow checks indicated an average flow angle of 2.0 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Pellet Mill 1 Cooler Stack is shown in Figure 4-12.



Figure 4-12. Photograph of the Pellet Mill 1 Cooler Stack

### 4.7 Green Hammermill Stack Sampling Location

The Green Hammermill stack sampling location shown in Figure 4-13 meets the minimum requirements for a downstream flow disturbance specified in Method 1, Section 11.1. The upstream flow disturbance is the fan outlet duct. The downstream flow disturbance is the stack discharge. The distance to the upstream flow disturbance meets Method 1 requirements. Only one sampling port could be reached safely. All of the sampling ports were reached by angling the Pitot tube inserted through the port facing south.

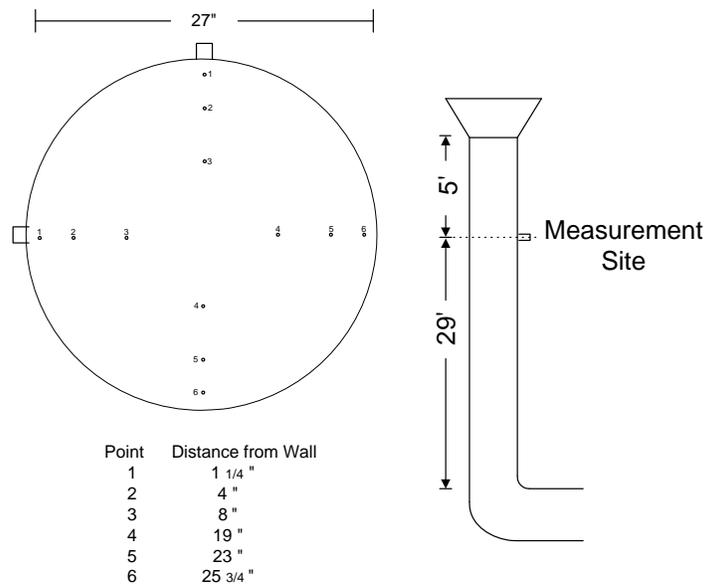


Figure 4-13. Green Hammermill Stack Sampling Location

No cyclonic flow conditions were observed in the Green Hammermill stack. The point-by-point cyclonic flow checks indicated an average flow angle of 1.7 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Green Hammermill stack is shown in Figure 4-14.



Figure 4-14. Photograph of the Green Hammermill Fan Inlet

## **5. TESTING PROCEDURES**

### **5.1 Flue Gas Velocity and Volumetric Flow Rate - EPA Method 2**

The flue gas velocities and volumetric flow rates during all of the emission tests were determined according to the procedures outlined in U.S. EPA Reference Method 2. Velocity measurements were made using S-Type Pitot tubes conforming to the geometric specifications outlined in Method 2. Accordingly, each Pitot was assigned a coefficient of 0.84. Velocity pressures were measured with fluid manometers. Effluent gas temperatures were measured with chromel-alumel thermocouples attached to digital readouts.

### **5.2 Flue Gas Composition and Molecular Weight - EPA Method 3**

Flue gas analyses and calculation of flue gas dry molecular weights were performed in accordance with EPA Method 3. A stainless steel probe was inserted into the gas stream to collect a representative sample of the flue gas during each test run. The samples were analyzed using a Fyrite gas analyzer. Moisture was removed from the sample gas by means of a knockout jar located prior to the sample pump.

### **5.3 Flue Gas Moisture Content - EPA Method 4**

The flue gas moisture content was determined in conjunction with each test run according to the sampling and analytical procedures outlined in EPA Method 4. Wet impinger sampling trains were used to withdraw and analyze the stack gas. The impingers were connected in series and contained water in the first two impingers followed by an empty impinger and then a silica gel impinger. The impingers were contained in an ice bath to assure condensation of the flue gas stream moisture. Any moisture that was not condensed in the impingers was captured in the silica gel; therefore, all moisture was weighed and entered into moisture content calculations.

### **5.4 Total Hydrocarbons – EPA Method 25A**

Continuous emissions monitoring was conducted for volatile organic compounds. The sampling and analytical procedures for VOCs were conducted in accordance with EPA 25A. The CEM system consisted of a sample acquisition system, the THC emission monitor, and a data acquisition system (DAS). A California Analytical Model 300 flame ionization detector was used for the Method 25A tests.

The sample acquisition system included an in-stack probe, a heated out-of-stack glass mat filter for particulate matter removal, a heat-traced Teflon® sample line, a Teflon® heated-head pump, and a gas manifold board. All components of the sample acquisition system that contacted the sampled gas were constructed of Type 316 stainless steel or Teflon®. The sample gas was continuously extracted from a central point within the duct at a constant rate ( $\pm 10\%$ ) for the duration of each test run. The wet, filtered gas was transported to a heated-head pump located at the CEM laboratory. The sample gas was sent directly to the VOC analyzer. Care was taken to ensure that the sample gas was greater than 250°F during transport from the stack to the VOC monitor. All pretest and posttest calibration procedures were performed as outlined in the EPA Reference Method 25A.

Total organic hydrocarbon concentrations were measured on a wet basis using a California Analytical 300 FID continuous emission monitor. The THC concentrations were monitored on a propane (C<sub>3</sub>) basis using a flame ionization detector (FID). The FID was fueled by a gas mixture consisting of 40% helium and 60% hydrogen to reduce the effect of oxygen synergism. The

THC analyzer was calibrated with a set of at least four gas standards. Calibration tests were performed prior to and following each test run.

Outputs from the individual emission monitors were connected to a computerized data acquisition system. Outputs from the analyzer were sent to a portable computer via a National Instruments™ FieldPoint controller. The signals were downloaded to a STRATA® software program every two seconds. The two-second readings were averaged for the duration of the test run.

Total mass emissions of VOCs were determined based on the Method 25A total hydrocarbon concentration data. The mass emissions were expressed on a pounds mass of carbon per hour.

### 5.5 Organic HAP Compounds – EPA Method 320

Testing for wet-basis organic HAP concentrations was conducted by extractive Fourier transform infrared (FTIR) spectroscopy using EPA Method 320 (40CFR, Part 63, Appendix A). Sample gas was continuously passed through the sampling system, which included an in-stack probe, a heated out-of-stack glass mat filter for particulate matter removal, a Teflon® heat-traced sample line, a MIDAC Fourier Transform Infrared (FTIR) spectrometer, a Teflon® heated-head pump, and a gas manifold board as shown in Figure 5-1. All components of the sample acquisition system that contacted the sampled gas were Type 316 stainless steel or Teflon®. All components of the sampling system and the FTIR cell were maintained at or above 120° C. Air Control Techniques, P.C. took great care to ensure that the sampling system contained no “cold spots” to prevent organic HAP loss. The sampling rate was maintained at approximately 10 liters per minute.

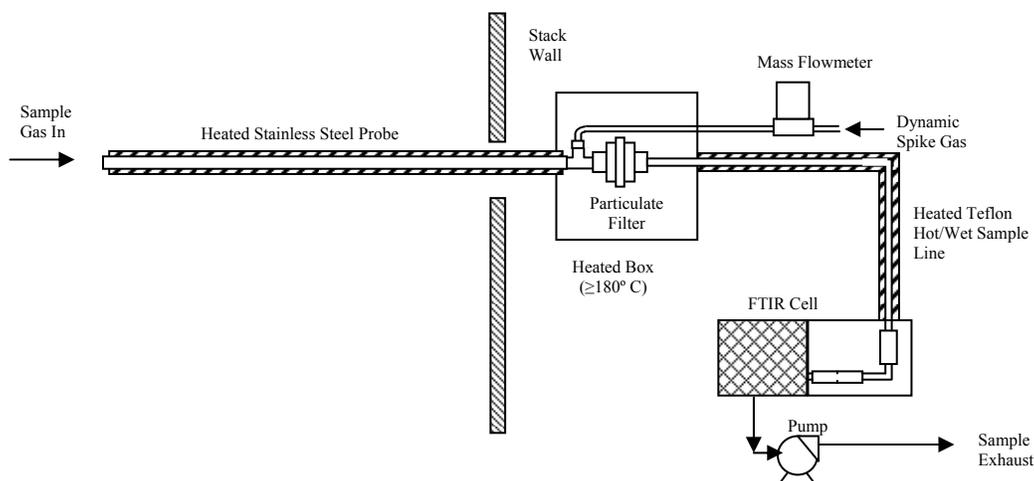


Figure 5-1. Method 320 Organic HAP Sampling System

The FTIR system included a MIDAC Corporation I-1301 spectrometer equipped with a heated, nominal 10-meter path absorption cell, a potassium bromide (KBr) beam splitter, zinc selenide (ZnSe) non-hygroscopic windows, and a liquid nitrogen-cooled Mercury Cadmium Telluride detector. Measurements were made using a MIDAC Model I-1301 high resolution Michelson interferometer with AutoQuant Pro software. Sample gas continuously passed through the sampling system, and sample spectra (based on 50 co-added interferograms) were recorded every

minute. The system's nominal spectral resolution was  $0.5 \text{ cm}^{-1}$ . Samples and standards were analyzed at temperatures greater than  $120^\circ\text{C}$  and near ambient pressures.

The inside walls of the cells were polished stainless steel to minimize interaction of the sample with the cell walls, and the cell mirrors were of bare gold. The gas pressure in the FTIR sample cell was monitored with a pressure transducer connected directly to the sample cell. The heated sample cell was wrapped in an insulating thermal jacket, and the temperature was controlled with type J thermocouples. The absorption cell volume was approximately 2 liters.

The FTIR system was operated via a portable computer, and a data archive storage system (USB Mass Storage Drive) was used for data backup. All interferograms, single beams, absorbance spectra, and background single beams were stored and have been archived. The filename, time, pressure and temperature of the sample cell, scan rate, background identification and other pertinent information was recorded by hand during the test program.

Air Control Techniques used the program AutoquantPro™ Version 4.5.0.195, (©Midac Corporation, 2012) to collect and analyze all the infrared field data. The program allows the development and storage of analytical “methods” for analysis of spectral data (absorbance) files. The reference spectra used for these analyses were developed by MIDAC Corporation, EPA, and Enthalpy Analytical, Inc. One “model” was developed for determining the absorption path length and one additional “method” for determining the concentrations of the target compounds for each source.

The concentration uncertainty reported by AutoquantPro is called the Standard Error of the Estimated Concentration, or SEC; it is also known as the Marginal Standard Deviation. The uncertainties in the concentration are proportional to the square root of the sums of the squares of the residual. After the residual spectrum is obtained, which we will call R, the error variance for the case of a single reference spectrum is calculated as follows.

$$\sigma^2 = \frac{\sum_i R_i^2}{(n-1)}$$

Where n is the number of observations. The SEC is given by the following.

$$SEC = \frac{\sigma C}{\sqrt{\sum_i A_i^2}}$$

Where **A** is the spectrum and **C** is the known concentration of the reference.

The 95% confidence interval is 1.96 times the SEC.

## **6. QUALITY ASSURANCE**

### **6.1 Method 1 Quality Assurance**

All S-type Pitot tubes used in this project conformed to EPA guidelines concerning construction and geometry. Pitot tubes were inspected prior to use. Information pertaining to S-type Pitot tubes is presented in detail in Section 3.1.1 of EPA Publication No. 600/4-77-027b. Only S-type Pitot tubes meeting the required EPA specifications were used in this project.

The thermocouples used in this project were calibrated using the procedures described in Section 3.4.2 of EPA Publication No. 600/4-77-027b. Each temperature sensor was calibrated at a minimum of three points over the anticipated range of use against NIST-traceable mercury in glass thermometer.

### **6.2 Method 4 Quality Assurance**

Pretest and posttest leak checks were conducted on each Method 4 sampling train used. The observed leak rates for the sampling trains were below 0.02 actual cubic feet per minute as required by Method 4.

All dry gas meters were fully calibrated to determine the volume correction factor prior to field use. Post-tests calibration checks were performed as soon as possible after the equipment was returned to the laboratory. Pre-and post-test calibrations agreed within  $\pm 5$  percent. The calibration procedure is documented in Section 3.3.2 of EPA Publication No. 600/4-77-237b.

The scales used at the test location to determine flue gas moisture content were calibrated using a standard set of weights.

### **6.3 Method 25A Quality Assurance**

At the beginning of the test day, a linearity calibration test was performed on each analyzer. The continuous emission monitoring instrument response did not differ by more  $\pm 5$  from the propane calibration standard. Linearity results for the test program are provided in Table 6-1 through 6-8.

Prior to and following each test run, a system calibration test was performed. The system test was performed to verify that the sampling system did not contain leaks (system bias) and to measure a change in analyzer response during the test program (system drift). The system bias was less than  $\pm 5\%$  of full-scale, and system drift was less than  $\pm 3\%$  of full scale. System calibration results for the test program are provided in Tables 6-1 through 6-8.

Table 6-1. Dryer 1 Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.0		
Low, %	±5	0.4		
Mid, %	±5	2.2		
High, %	±5	0.0		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.8	0.1
Zero Bias (Post), %	±5	0.9	0.1	0.0
Up-scale Bias (Pre), %	±5	0.0	-0.2	-0.6
Up-scale Bias (Post), %	±5	0.1	-0.6	-1.0
Zero Drift, %	±3	0.9	-0.7	-0.2
Up-scale Drift, %	±3	0.1	-0.4	-0.4
Response Time, sec	N/A			

Table 6-2. Pellet Cooler 1 Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.1		
Low, %	±5	0.4		
Mid, %	±5	0.8		
High, %	±5	0.0		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.3	0.2
Zero Bias (Post), %	±5	0.3		0.3
Up-scale Bias (Pre), %	±5	0.1	-0.1	-0.1
Up-scale Bias (Post), %	±5	-0.1		0.3
Zero Drift, %	±3	0.3	-0.1	0.1
Up-scale Drift, %	±3	-0.1	0.0	-0.1
Response Time, sec	N/A			

Table 6-3. Dryer 2 Quality Assurance Results, Total Hydrocarbons, Method 25A, High Range				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.1		
Low, %	±5	0.3		
Mid, %	±5	-0.1		
High, %	±5	0.0		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.1	-0.1
Zero Bias (Post), %	±5	0.1	-0.1	-0.1
Up-scale Bias (Pre), %	±5	0.0	-0.3	-0.4
Up-scale Bias (Post), %	±5	-0.3	-0.4	-0.3
Zero Drift, %	±3	0.1	-0.1	0.0
Up-scale Drift, %	±3	-0.3	-0.1	0.1
Response Time, sec	N/A	28		

Table 6-4. Dryer 2 Quality Assurance Results, Total Hydrocarbons, Method 25A, Low Range				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±8	1.0		
Low, %	±8	1.5		
Mid, %	±8	0.7		
High, %	±8	0.1		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.6	-0.6
Zero Bias (Post), %	±5	0.6	-0.6	-0.7
Up-scale Bias (Pre), %	±5	0.0	0.3	0.1
Up-scale Bias (Post), %	±5	0.3	0.1	-0.1
Zero Drift, %	±3	0.6	-1.2	-0.1
Up-scale Drift, %	±3	0.3	-0.2	-0.2
Response Time, sec	N/A	28		

Table 6-5. Dry Hammermill 2 Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.0		
Low, %	±5	0.4		
Mid, %	±5	2.2		
High, %	±5	0.0		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.2	0.0	0.2
Zero Bias (Post), %	±5	0.0	0.2	0.2
Up-scale Bias (Pre), %	±5	-1.3	-1.1	-1.3
Up-scale Bias (Post), %	±5	-1.1	-1.3	-1.2
Zero Drift, %	±3	-0.1	0.1	0.0
Up-scale Drift, %	±3	0.2	-0.1	0.0
Response Time, sec	N/A	28		

Table 6-6 Pellet Cooler 2 Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0		
Low, %	±5	0.4		
Mid, %	±5	2.2		
High, %	±5	0.0		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.3	0.1
Zero Bias (Post), %	±5	0.3	0.1	0.2
Up-scale Bias (Pre), %	±5	-1.0	-0.9	-1.0
Up-scale Bias (Post), %	±5	-0.9	-1.0	-1.3
Zero Drift, %	±3	0.3	-0.2	0.0
Up-scale Drift, %	±3	0.1	-0.1	-0.3
Response Time, sec	N/A	28		

Table 6-7. Aspiration Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.1		
Low, %	±5	0.7		
Mid, %	±5	0.0		
High, %	±5	0.1		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.1	0.0
Zero Bias (Post), %	±5	0.1	0.0	0.1
Up-scale Bias (Pre), %	±5	0.0	-0.1	-0.1
Up-scale Bias (Post), %	±5	-0.1	-0.1	-0.3
Zero Drift, %	±3	0.1	-0.1	0.1
Up-scale Drift, %	±3	-0.1	0.1	-0.3
Response Time, sec	N/A	28		

Table 6-8. Green Hammermill Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.0		
Low, %	±5	1.1		
Mid, %	±5	1.6		
High, %	±5	0.4		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.1	0.1
Zero Bias (Post), %	±5	0.1	0.1	0.1
Up-scale Bias (Pre), %	±5	0.0	-0.1	-0.7
Up-scale Bias (Post), %	±5	-0.1	-0.7	-1.0
Zero Drift, %	±3	0.1	-0.1	0.1
Up-scale Drift, %	±3	-0.1	-0.5	-0.3
Response Time, sec	N/A	28		

#### 6.4 Method 320 Quality Assurance

Air Control Techniques, P.C. performed daily quality assurance checks. Background scans and calibration transfer standard (CTS) spectra tests were performed prior to and following each test series. An analyte spike was performed using methanol.

The flow rate at the outlet of the pump was measured while the probe was plugged to verify that the sampling system was leaks. The flow rate was less than 200 ml/min.

The FTIR cell was tested for leaks by closing the value while the cell was at minimum absolute pressure.

Background Spectra

Sample spectra were divided point-by-point by a 128-scan background recorded using N<sub>2</sub>. The single beam spectrum was constantly monitored, and a new background was generated approximately following each test series or when residual and absorbance spectra indicated component build-up on the optical surfaces or alignment-related baseline shifts.

Calibration Transfer Standards and Absorption Path Lengths

A cylinder of 100 ppm ethylene in nitrogen served as the CTS. A CTS gas was introduced to the FTIR and allowed to reach steady state. The CTS was used to determine effective cell path length based on comparisons of the “field” CTS spectra to a laboratory CTS spectrum recorded by MIDAC. As shown in Table 6-9, the maximum path length deviation was less than 5% of the average.

Date	Time	CTS Scan (pathlength)	SEC (ppm)	Cell Press. (psi)	Cell Temp (deg C)	Deviation from Previous	Deviation from Average
10-Oct	806	8.78	0.137	14.7	121	NA	-0.6%
	1927	8.68	0.120	14.89	121	1.1%	0.5%
11-Oct	1121	8.73	0.134	14.8	121	-0.6%	-0.1%
	1301	8.73	0.133	14.7	121	0.0%	-0.1%
	1755	8.75	0.133	14.6	121	-0.3%	-0.3%
	2204	8.72	0.133	14.8	121	0.4%	0.1%
12-Oct	0809	8.59	0.133	14.9	121	1.4%	1.5%
	1300	8.77	0.137	14.6	121	-2.1%	-0.5%
	1940	8.78	0.134	14.72	121	-0.1%	-0.6%
13-Oct	0810	8.71	0.134	14.82	121	0.7%	0.1%
	1435	8.73	0.135	14.85	121	-0.1%	0.0%
Average		8.725	0.133				

Background Spectra

On-site test personnel performed matrix spiking using a certified calibration standard of methanol and SF<sub>6</sub>. The methanol gas standard was introduced into the sampling system upstream of the particulate matter filter at an average dilution ratio of less than 10% of the total sample volume. Analyte spiking was performed to demonstrate the suitability of the sampling system. The dilution factor was calculated based on the ratio of the SF<sub>6</sub> tracer gas analyzed directly by the FTIR and the in-stack measured concentration.

$$\frac{SF_6 \text{ during spike}}{SF_6 \text{ direct}} = DF$$

The recovery was calculated using the mean concentration of the spiked analyte ( $S_m$ ), the native concentration of the analyte in the stack ( $S_u$ ), the dilution factor (DF), and the cylinder concentration ( $C_s$ ).

$$\text{Recovery}(\%) = \frac{S_m - S_u (1 - DF)}{DF \times C_s}$$

As shown in Table 6-10, the percent recovery was 100±30% as required by Method 320.

Table 6-10. Spike Recovery Results Summary						
Direct Cylinder Spike, ppm		System Spiked Gas, ppm		Native Concentration, ppm		Recovery, %
methanol	SF <sub>6</sub>	methanol	SF <sub>6</sub>	methanol	SF <sub>6</sub>	
101.26	2.84	9.867	0.272	0.496	-0.00789	94.6

Minimum Detectable Concentration

EPA Method 320 and the equivalent ASTM Standard D6348-03 specify a number of analytical uncertainty parameters that the analyst may calculate to characterize the FTIR system performance.

QA Review

Before the test program began, an analysis of possible analytical interferences (e.g., H<sub>2</sub>O, CO<sub>2</sub>, CO, pinenes) based on previous stack test data. Analytical wavelengths were determined to minimize analytical uncertainty and detection limits using reference spectra and the FTIR instrument that was used for the field testing.

At the conclusion of the testing a quality assurance review of the test data was performed. This review included examination of the sample spectra and the quantitative analytical results. It also included spot-checking the analysis results by hand. These examinations included visual comparisons of the sample and reference spectra.

## **7. PROCESS DOCUMENTATION**

Enviva Pellets Wiggins, LLC personnel logged the following process data during each test run of each process unit.

- Throughput in tons per hour (all process units)
- Inlet temperature (dryer)
- Outlet temperature (dryer)
- Cyclone static pressure drop (dryer, hammermill, presses)
- Wood feed % softwood content

## 8. REFERENCES

1. Enviva, LP. "Emission Testing Protocol." Submitted to Mississippi Department of Environmental Quality, July 31, 2013.
2. Environmental Monitoring Laboratories, Inc. "Investigative Air Emissions Tests, Enviva Pellets Wiggins, LLC.", November 15-16, 2012" Report to Enviva, LP, January 13, 2013.
3. Air Compliance Testing, Inc. "Self-Evaluation Engineering Study Test Report, Determination of Hydrogen Chloride Removal Efficiency and Total Gaseous Organic Emissions." Report to Georgia Biomass, LLC, August 27, 2012.
4. Richards, J., D. Goshaw, and T. Holder. "Laboratory Evaluation of VOC Emissions from Wood Pellet Processes." Report to Enviva, LP. July 31, 2013.
5. Beauchemin, P. and M. Tampier. "Emissions and Air Pollution Control for the Biomass Pellet Manufacturing Industry." Report submitted to the British Columbia Ministry of the Environment. May 12, 2010.
6. Milota, M.R. "Emissions from Wood Drying" Forest Projects Journal, Volume 50, Number 6, Pages 10-19, June 2000.
7. Milota, M. and P. Mosher. "Emissions of Hazardous Air Pollutants from Lumber Drying." Forest Products Journal, Volume 58, No. 7/8, Pages 50-55, July/August 2008.

## **APPENDIX A**

### **Moisture and Gas Flow Rate Data**

Air Control Techniques, PC: Emissions Calculations

Job # 1911

Enviva	Wiggins	Green Hammermill	Green Hammermill	Green Hammermill	Dryer 1	Dryer 1	Dryer 1
PARAMETER	NOMENCLATURE	1	2	3	4	5	6
Sampling Location		Green Hammermill	Green Hammermill	Green Hammermill	Dryer 1	Dryer 1	Dryer 1
Date		10/10/2013	10/10/2013	10/10/2013	10/10/2013	10/11/2013	10/11/2013
Run Time	θ	60	60	60	60	60	60
Nozzle Diameter	inches	N/A	N/A	N/A	N/A	N/A	N/A
Stack Area	As - sq. ft.	3.98	3.98	3.98	10.56	10.56	10.56
Pitot Tube Coefficient	Cp	0.84	0.84	0.84	0.84	0.84	0.84
Meter Calibration Factor	Y	0.9828	0.9828	0.9828	0.9828	0.9828	0.9828
Barometric Pressure, inches Hg	Bp - in Hg	29.90	29.90	29.90	29.90	29.80	29.80
Static Pressure	Pg - in. H <sub>2</sub> O	-20.8	-20.8	-20.8	-0.75	-0.71	-0.71
Stack Pressure	Ps	28.37	28.37	28.37	29.84	29.75	29.75
Meter Box Pressure Differential	Δ H - in. H <sub>2</sub> O	1.00	1.00	1.00	1.00	1.00	1.00
Average Velocity Head	Δ p - in. H <sub>2</sub> O	3.961	3.854	3.847	1.283	1.172	1.185
Volume of Gas Sampled	Vm - cu. ft.	33.868	33.981	33.156	33.201	33.221	32.565
Dry Gas Meter Temperature	Tm - °F	66.0	70.8	75.5	81.250	76.5	87.0
Stack Temperature	Ts - °F	70.8	70.6	70.9	146.3	150.1	147.3
Liquid Collected	grams	25.1	26.5	16.6	129.5	99.8	117.5
Carbon Dioxide	% CO <sub>2</sub>	0	0	0	2	4	4
Oxygen	% O <sub>2</sub>	20.9	20.9	20.9	19	17	17
Carbon Monoxide	% CO	0	0	0	0	0	0
Nitrogen	% N <sub>2</sub>	79.1	79.1	79.1	79	79	79
Volume of Gas Sampled, Dry	Vmstd - cu. ft.	33.472	33.283	32.187	31.888	32.082	30.845
Volume of Water Vapor	Vwstd - cu. ft.	1.183	1.249	0.783	6.106	4.706	5.540
Moisture Content	% H <sub>2</sub> O	3.41	3.62	2.37	16.07	12.79	15.23
Saturation Moisture	% H <sub>2</sub> O	2.7	2.7	2.7	23.1	25.4	23.7
Dry Mole Fraction	Mfd	0.966	0.964	0.976	0.839	0.872	0.848
Fuel Factor	Fo	#DIV/0!	#DIV/0!	#DIV/0!	0.950	0.975	0.975
Gas Molecular Weight, Dry	Md	28.84	28.84	28.84	29.08	29.32	29.32
Gas Molecular Weight, Wet	Ms	28.47	28.44	28.58	27.30	27.87	27.60
Gas Velocity	vs - ft./sec.	115.87	114.32	113.97	70.16	66.68	67.23
Volumetric Air Flow, Actual	Qaw - ACFM	27,642	27,273	27,189	44,448	42,243	42,593
Volumetric Air Flow, Standard	Qsd - DSCFM	25,184	24,803	25,031	32,404	31,700	31,215

Air Control Techniques, PC: Emissions Calculations

Job #

1911

	Enviva	Wiggins	Dry Hammermill 2	Dry Hammermill 2	Dry Hammermill 2	Pellet Mill 2 Aspiration	Pellet Mill 2 Aspiration	Pellet Mill 2 Aspiration
PARAMETER	NOMENCLATURE		10	11	12	16	17	18
Sampling Location			Dry Hammermill 2	Dry Hammermill 2	Dry Hammermill 2	Pellet Mill 2 Aspiration	Pellet Mill 2 Aspiration	Pellet Mill 2 Aspiration
Date			10/11/2013	10/11/2001	10/11/2013	10/12/2013	10/12/2013	10/12/2013
Run Time	θ		60	60	60	60	60	60
Nozzle Diameter	inches		N/A	N/A	N/A	N/A	N/A	N/A
Stack Area	As - sq. ft.		2.64	2.64	2.64	0.20	0.20	0.20
Pitot Tube Coefficient	Cp		0.84	0.84	0.84	0.84	0.84	0.84
Meter Calibration Factor	Y		0.9828	0.9828	0.9828	0.9828	0.9828	0.9828
Barometric Pressure, inches Hg	Bp - in Hg		29.80	29.80	29.80	29.85	29.85	29.85
Static Pressure	Pg - in. H <sub>2</sub> O		1.4	1.4	1.4	-7.5	-7.5	-7.5
Stack Pressure	Ps		29.90	29.90	29.90	29.30	29.30	29.30
Meter Box Pressure Differential	Δ H - in. H <sub>2</sub> O		1.00	1.00	1.00	1.00	1.00	1.00
Average Velocity Head	Δ p - in. H <sub>2</sub> O		2.601	2.308	2.618	5.359	4.944	4.547
Volume of Gas Sampled	Vm - cu. ft.		33.419	33.679	33.876	33.241	32.149	34.408
Dry Gas Meter Temperature	Tm - °F		80.3	78.8	78.3	85.0	84.8	81.8
Stack Temperature	Ts - °F		122.4	128.2	116.4	148.6	148.3	152.1
Liquid Collected	grams		30.2	30	30.2	256.8	269.6	274.4
Carbon Dioxide	% CO <sub>2</sub>		0	0	0	0	0	0
Oxygen	% O <sub>2</sub>		20.9	20.9	20.9	20.9	20.9	20.9
Carbon Monoxide	% CO		0	0	0	0	0	0
Nitrogen	% N <sub>2</sub>		79.1	79.1	79.1	79.1	79.1	79.1
Volume of Gas Sampled, Dry	Vmstd - cu. ft.		32.050	32.389	32.609	31.654	30.628	32.962
Volume of Water Vapor	Vwstd - cu. ft.		1.424	1.415	1.424	12.108	12.712	12.938
Moisture Content	% H <sub>2</sub> O		4.25	4.18	4.18	27.67	29.33	28.19
Saturation Moisture	% H <sub>2</sub> O		12.3	14.4	10.4	24.9	24.7	27.2
Dry Mole Fraction	Mfd		0.957	0.958	0.958	0.723	0.707	0.718
Fuel Factor	Fo		#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
Gas Molecular Weight, Dry	Md		28.84	28.84	28.84	28.84	28.84	28.84
Gas Molecular Weight, Wet	Ms		28.38	28.38	28.38	25.84	25.66	25.78
Gas Velocity	vs - ft./sec.		95.95	90.82	95.74	149.06	143.63	137.85
Volumetric Air Flow, Actual	Qaw - ACFM		15,197	14,385	15,165	1,756	1,692	1,624
Volumetric Air Flow, Standard	Qsd - DSCFM		13,183	12,366	13,303	1,079	1,016	985

## Air Control Techniques, PC: Emissions Calculations

Job #

1911

Enviva	Wiggins	Dryer 2	Dryer 2	Dryer 2
PARAMETER	NOMENCLATURE	19	20	21
Sampling Location		Dryer 2	Dryer 2	Dryer 2
Date		10/13/2013	10/13/2013	10/13/2013
Run Time	$\theta$	60	60	60
Nozzle Diameter	inches	N/A	N/A	N/A
Stack Area	As - sq. ft.	12.05	12.05	12.05
Pitot Tube Coefficient	Cp	0.84	0.84	0.84
Meter Calibration Factor	Y	0.9828	0.9828	0.9828
Barometric Pressure, inches Hg	Bp - in Hg	29.90	29.90	29.90
Static Pressure	Pg - in. H <sub>2</sub> O	-0.33	-0.33	-0.33
Stack Pressure	Ps	29.88	29.88	29.88
Meter Box Pressure Differential	$\Delta H$ - in. H <sub>2</sub> O	1.00	1.00	1.00
Average Velocity Head	$\Delta p$ - in. H <sub>2</sub> O	0.285	0.300	0.291
Volume of Gas Sampled	Vm - cu. ft.	31.888	33.650	30.796
Dry Gas Meter Temperature	Tm - °F	77.5	89.5	90.3
Stack Temperature	Ts - °F	174.3	154.9	171.8
Liquid Collected	grams	267.7	287.5	260
Carbon Dioxide	% CO <sub>2</sub>	4.5	4	4
Oxygen	% O <sub>2</sub>	16.5	17	17
Carbon Monoxide	% CO	0	0	0
Nitrogen	% N <sub>2</sub>	79	79	79
Volume of Gas Sampled, Dry	Vmstd - cu. ft.	30.841	31.834	29.094
Volume of Water Vapor	Vwstd - cu. ft.	12.622	13.556	12.259
Moisture Content	% H <sub>2</sub> O	29.04	29.86	29.64
Saturation Moisture	% H <sub>2</sub> O	44.9	28.5	42.4
Dry Mole Fraction	Mfd	0.710	0.701	0.704
Fuel Factor	Fo	0.978	0.975	0.975
Gas Molecular Weight, Dry	Md	29.38	29.32	29.32
Gas Molecular Weight, Wet	Ms	26.08	25.94	25.96
Gas Velocity	vs - ft./sec.	34.58	35.02	34.97
Volumetric Air Flow, Actual	Qaw - ACFM	24,998	25,318	25,278
Volumetric Air Flow, Standard	Qsd - DSCFM	14,745	15,224	14,842

**Method 1 - Air Control Techniques, P.C.**

Date

10/10/2013

Client	Enviva
Job #	1911
Plant Name	Wiggins
State	Mississippi
City	Wiggins
Sampling Location	Dryer 1
No. of Ports Available	2
No. of Ports Used	1
Port Inside Diameter, Inches	4
Distance From Far Wall To Outside Of Port, Inches	46
Nipple Length And/Or Wall Thickness, Inches	2
Depth Of Stack Or Duct, Inches	44
Stack Or Duct Width (if rectangular), Inches	
Equiv. Diameter = 2DW/(D+W), Inches	44
Stack/Duct Area, Square Feet	10.6
( <input type="checkbox"/> x R <sup>2</sup> or L x W)	
	Upstream Downstream
Distance to Flow Disturbances, Inches	290.4 235.2
Diameters	6.60 5.35

Note: If more than 8 and 2 diameters and if duct dia. is less than 24" use 8 or 9 points.

Velocity	Diameters		Particulate
	UP	Down	
12	8	2	12
12	7	1.75	12
12	6	1.5	16
16	5	1.25	20
16	2	0.5	24 or 25

Location of Points in Circular Stacks or Ducts											
	4	6	8	10	12	14	16	18	20	22	24
1	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	25.0	14.6	10.6	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2
3	75.0	29.6	19.4	14.6	11.8	9.9	8.5	7.5	6.7	6.0	5.5
4	93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7	7.9
5		85.4	67.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6	10.5
6		95.6	80.6	65.8	35.6	26.9	22.0	18.8	16.5	14.6	13.2
7			89.5	77.4	64.4	36.6	28.3	23.6	20.4	18.0	16.1
8			96.8	85.4	75.0	63.4	37.5	29.6	25.0	21.8	19.4
9				91.8	82.3	73.1	62.5	38.2	30.6	26.2	23.0
10				97.4	88.2	79.9	71.7	61.8	38.8	31.5	27.2
11					93.3	85.4	78.0	70.4	61.2	39.3	32.3
12					97.9	90.1	83.1	76.4	69.4	60.7	39.8
13						94.3	87.6	81.2	75.0	68.5	60.2
14						98.2	91.5	85.4	79.6	73.8	67.7
15							95.1	89.1	83.5	78.2	72.8
16							98.4	92.5	87.1	82.0	77.0
17								95.6	90.3	85.4	80.6
18								98.6	93.3	88.4	83.9
19									96.1	91.3	86.8
20									98.7	94.0	89.5
21										96.5	92.1
22										98.9	94.5
23											96.8
24											98.9

2 diff nipples probe marked to inside of port

Point Location Data			
Point	% of Duct Depth	Distance From Inside Wall	Distance From Outside of Port
1	4.4	1 7/8	3 7/8
2	14.6	6 3/8	8 3/8
3	29.6	13	15
4	70.4	31	33
5	85.4	37 5/8	39 5/8
6	95.6	42 1/8	44 1/8
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

Location of Points in Rectangular Stacks or Ducts											
	2	3	4	5	6	7	8	9	10	11	12
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.5
3		83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8
4			87.5	70.0	58.3	50	43.8	28.9	35.0	31.8	29.2
5				90.0	75	64.3	56.3	50	45.0	40.9	37.5
6					91.7	78.6	68.8	61.1	55.0	50	45.8
7						92.9	81.3	72.2	65.0	59.1	54.2
8							93.8	83.3	75.0	68.2	62.5
9								94.4	85.0	77.3	70.8
10									95.0	86.4	79.2
11										95.5	87.5
12											95.8

- 0.0000 - 0.0625 - 0
- 0.0625 - 0.1875 - 1/8
- 0.1875 - 0.3125 - 1/4
- 0.3125 - 0.4375 - 3/8
- 0.4375 - 0.5625 - 1/2
- 0.5625 - 0.6875 - 5/8
- 0.6875 - 0.8125 - 3/4
- 0.8125 - 0.9375 - 7/8
- 0.9375 - 1.0000 - 1

Dryer 1 Run 1

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		4	
Plant	Wiggins			Date		10/10/2013	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Dryer 1			Pitot ID		6Pext	
<b>Averages</b>	<b>1.283</b>	<b>146.3</b>		Thermocouple ID		TC25	
	<b>Delta P</b>	<b>Temp</b>					
<b>Point No.</b>	<b>In Water</b>	<b>Deg F</b>	<b>Angle</b>				
A-1	1.200	144	7	<b>Oxygen %</b>		<b>19</b>	
2	1.100	145	2				
3	1.050	145	4	<b>Carbon Dioxide %</b>		<b>2</b>	
4	1.400	146	-3				
B-1	1.400	147	0	<b>Moisture %</b>		<b>16.07</b>	
2	1.500	147	-4				
B-1	1.100	147	6	<b>Stack Area sq.in.</b>		<b>1520.530867</b>	
2	1.300	147	3				
3	1.200	147	2	<b>Pbar</b>		<b>29.90</b>	
4	1.300	147	0				
5	1.300	147	-4	<b>Static Pressure</b>		<b>-0.75</b>	
6	1.600	147	-3				
0				<b>Pitot Coef.</b>		<b>0.84</b>	
0							
0				<b>Start Time</b>		<b>1732</b>	
0							
0				<b>Stop Time</b>		<b>1738</b>	
0							
0				<b>Absolute Gas Pressure inches water</b>	<b>Ps =</b>	<b>29.84</b>	
0							
0				<b>Dry Mole Fraction of Gas</b>	<b>Mfd =</b>	<b>0.83929</b>	
0							
0				<b>Dry Molecular Weight of Gas lb/lb Mole</b>	<b>Md =</b>	<b>29.08</b>	
0							
0				<b>Wet Molecular Weight of Gas lb/lb Mole</b>	<b>Ms =</b>	<b>27.30</b>	
0							
0				<b>Average Gas Velocity ft/sec</b>	<b>vs =</b>	<b>70.16</b>	
0							
0				<b>Dry Volumetric Gas Flow Rate</b>			
0				<b>at Standard Conditions SCFM</b>	<b>Qsd =</b>	<b>32404</b>	
0							
0				<b>Wet Volumetric Flue Gas Flow Rate</b>			
0				<b>at Stack Conditions ACFM</b>	<b>Qaw =</b>	<b>44448</b>	
0							
0				<b>Wet Volumetric Gas Flow Rate</b>			
0				<b>at Standard Conditions WSCFH</b>	<b>WSCFH =</b>	<b>2316527</b>	
0							
0				LKCH			
0				Pre	3-6		good
8				Post	5-4		good
0							
0							

Dryer 1 Run 2

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		5	
Plant	Wiggins			Date		10/11/2013	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Dryer 1			Pitot ID		6Pext	
<b>Averages</b>	<b>1.172</b>	<b>150.1</b>		Thermocouple ID		TC25	
	<b>Delta P</b>	<b>Temp</b>					
<b>Point No.</b>	<b>In Water</b>	<b>Deg F</b>					
A-1	0.900	145		<b>Oxygen %</b>		<b>17</b>	
2	0.990	147					
3	1.000	148		<b>Carbon Dioxide %</b>		<b>4</b>	
4	1.400	150					
B-1	1.400	151		<b>Moisture %</b>		<b>12.79</b>	
2	0.820	150					
B-1	1.200	151		<b>Stack Area sq.in.</b>		<b>1520.530867</b>	
2	1.300	151					
3	1.300	152		<b>Pbar</b>		<b>29.80</b>	
4	1.300	152					
5	1.350	152		<b>Static Pressure</b>		<b>-0.71</b>	
6	1.200	152					
0				<b>Pitot Coef.</b>		<b>0.84</b>	
0							
0				<b>Start Time</b>		<b>840</b>	
0							
0				<b>Stop Time</b>		<b>850</b>	
0							
0				<b>Absolute Gas Pressure inches water</b>	<b>Ps =</b>	<b>29.75</b>	
0							
0				<b>Dry Mole Fraction of Gas</b>	<b>Mfd =</b>	<b>0.87209</b>	
0							
0				<b>Dry Molecular Weight of Gas lb/lb Mole</b>	<b>Md =</b>	<b>29.32</b>	
0							
0				<b>Wet Molecular Weight of Gas lb/lb Mole</b>	<b>Ms =</b>	<b>27.87</b>	
0							
0				<b>Average Gas Velocity ft/sec</b>	<b>vs =</b>	<b>66.68</b>	
0							
0				<b>Dry Volumetric Gas Flow Rate</b>			
0				<b>at Standard Conditions SCFM</b>	<b>Qsd =</b>	<b>31700</b>	
0							
0				<b>Wet Volumetric Flue Gas Flow Rate</b>			
0				<b>at Stack Conditions ACFM</b>	<b>Qaw =</b>	<b>42243</b>	
0							
0				<b>Wet Volumetric Gas Flow Rate</b>			
0				<b>at Standard Conditions WSCFH</b>	<b>WSCFH =</b>	<b>2180938</b>	
0							
0				LKCH			
0				Pre	3-4		good
8				Post	5-3		good
0							
0							

Dryer 1 Run 3

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		6	
Plant	Wiggins			Date		10/11/2013	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Dryer 1			Pitot ID		6Pext	
<b>Averages</b>	<b>1.185</b>	<b>147.3</b>		Thermocouple ID		TC25	
	<b>Delta P</b>	<b>Temp</b>					
<b>Point No.</b>	<b>In Water</b>	<b>Deg F</b>					
A-1	1.050	148		<b>Oxygen %</b>		<b>17</b>	
2	1.050	147					
3	1.050	146		<b>Carbon Dioxide %</b>		<b>4</b>	
4	1.500	147					
B-1	1.500	147		<b>Moisture %</b>		<b>15.23</b>	
2	0.940	147					
B-1	1.100	147		<b>Stack Area sq.in.</b>		<b>1520.530867</b>	
2	1.200	147					
3	1.200	147		<b>Pbar</b>		<b>29.80</b>	
4	1.300	148					
5	1.300	148		<b>Static Pressure</b>		<b>-0.71</b>	
6	1.100	148					
0				<b>Pitot Coef.</b>		<b>0.84</b>	
0							
0				<b>Start Time</b>		<b>1112</b>	
0							
0				<b>Stop Time</b>		<b>1115</b>	
0							
0				<b>Absolute Gas Pressure inches water</b>	<b>Ps =</b>	<b>29.75</b>	
0							
0				<b>Dry Mole Fraction of Gas</b>	<b>Mfd =</b>	<b>0.84774</b>	
0							
0				<b>Dry Molecular Weight of Gas lb/lb Mole</b>	<b>Md =</b>	<b>29.32</b>	
0							
0				<b>Wet Molecular Weight of Gas lb/lb Mole</b>	<b>Ms =</b>	<b>27.60</b>	
0							
0				<b>Average Gas Velocity ft/sec</b>	<b>vs =</b>	<b>67.23</b>	
0							
0				<b>Dry Volumetric Gas Flow Rate</b>			
0				<b>at Standard Conditions SCFM</b>	<b>Qsd =</b>	<b>31215</b>	
0							
0				<b>Wet Volumetric Flue Gas Flow Rate</b>			
0				<b>at Stack Conditions ACFM</b>	<b>Qaw =</b>	<b>42593</b>	
0							
0				<b>Wet Volumetric Gas Flow Rate</b>			
0				<b>at Standard Conditions WSCFH</b>	<b>WSCFH =</b>	<b>2209261</b>	
0							
0				LKCH			
0				Pre	3-4		good
8				Post	5-3		good
0							
0							

**Method 1 - Air Control Techniques, P.C.**

Date

10/13/2013

Client	Enviva
Job #	1911
Plant Name	Wiggins
State	Mississippi
City	Wiggins
Sampling Location	Dryer 2
No. of Ports Available	2
No. of Ports Used	1
Port Inside Diameter, Inches	4
Distance From Far Wall To Outside Of Port, Inches	55.5
Nipple Length And/Or Wall Thickness, Inches	8.5
Depth Of Stack Or Duct, Inches	47
Stack Or Duct Width (if rectangular), Inches	
Equiv. Diameter = 2DW/(D+W), Inches	47
Stack/Duct Area, Square Feet	12.05
(□ x R <sup>2</sup> or L x W)	
	Upstream    Downstream
Distance to Flow Disturbances, Inches	325.2    674.4
Diameters	6.92    14.35

Note: If more than 8 and 2 diameters and if duct dia. is less than 24" use 8 or 9 points.

Diameters				
Velocity	UP	Down	Particulate	
12	8	2		12
12	7	1.75		12
12	6	1.5		16
16	5	1.25		20
16	2	0.5		24 or 25

Location of Points in Circular Stacks or Ducts

	4	6	8	10	12	14	16	18	20	22	24
1	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	25.0	14.6	10.6	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2
3	75.0	29.6	19.4	14.6	11.8	9.9	8.5	7.5	6.7	6.0	5.5
4	93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7	7.9
5		85.4	67.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6	10.5
6		95.6	80.6	65.8	35.6	26.9	22.0	18.8	16.5	14.6	13.2
7			89.5	77.4	64.4	36.6	28.3	23.6	20.4	18.0	16.1
8			96.8	85.4	75.0	63.4	37.5	29.6	25.0	21.8	19.4
9				91.8	82.3	73.1	62.5	38.2	30.6	26.2	23.0
10				97.4	88.2	79.9	71.7	61.8	38.8	31.5	27.2
11					93.3	85.4	78.0	70.4	61.2	39.3	32.3
12					97.9	90.1	83.1	76.4	69.4	60.7	39.8
13						94.3	87.6	81.2	75.0	68.5	60.2
14						98.2	91.5	85.4	79.6	73.8	67.7
15							95.1	89.1	83.5	78.2	72.8
16							98.4	92.5	87.1	82.0	77.0
17								95.6	90.3	85.4	80.6
18								98.6	93.3	88.4	83.9
19									96.1	91.3	86.8
20									98.7	94.0	89.5
21										96.5	92.1
22										98.9	94.5
23											96.8
24											98.9

2 diff nipples probe marked to inside of port

**Point Location Data**

Point	% of Duct	Distance From	Distance From
	Depth	Inside Wall	Outside of Port
1	4.4	2 1/8	10 5/8
2	14.6	6 7/8	15 3/8
3	29.6	13 7/8	22 3/8
4	70.4	33 1/8	41 5/8
5	85.4	40 1/8	48 5/8
6	95.6	44 7/8	53 3/8
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

Location of Points in Rectangular Stacks or Ducts

	2	3	4	5	6	7	8	9	10	11	12
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.5
3		83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8
4			87.5	70.0	58.3	50	43.8	28.9	35.0	31.8	29.2
5				90.0	75	64.3	56.3	50	45.0	40.9	37.5
6					91.7	78.6	68.8	61.1	55.0	50	45.8
7						92.9	81.3	72.2	65.0	59.1	54.2
8							93.8	83.3	75.0	68.2	62.5
9								94.4	85.0	77.3	70.8
10									95.0	86.4	79.2
11										95.5	87.5
12											96.8

- 0.0000 - 0.0625 - 0    0.5625 - 0.6875 - 5/8
- 0.0625 - 0.1875 - 1/8    0.6875 - 0.8125 - 3/4
- 0.1875 - 0.3125 - 1/4    0.8125 - 0.9375 - 7/8
- 0.3125 - 0.4375 - 3/8    0.9375 - 1.0000 - 1
- 0.4375 - 0.5625 - 1/2

Dryer 2 Run 1

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number	1911
Client	Enviva			ACT Run Number	19
Plant	Wiggins			Date	10/13/2013
City/State	Wiggins, MS			Gauge ID	909033
Location	Dryer 2			Pitot ID	6Pext
<b>Averages</b>	<b>0.285</b>	<b>174.3</b>		Thermocouple ID	TC25
	<b>Delta P</b>	<b>Temp</b>			
<b>Point No.</b>	<b>In Water</b>	<b>Deg F</b>	<b>Angle</b>		
A-1	0.200	168	5	<b>Oxygen %</b>	<b>16.5</b>
2	0.280	173	2		
3	0.330	175	0	<b>Carbon Dioxide %</b>	<b>4.5</b>
4	0.330	175	5		
5	0.300	174	0	<b>Moisture %</b>	<b>29.04</b>
6	0.230	170	0		
B-1	0.210	174	6	<b>Stack Area sq.in.</b>	<b>1734.94</b>
2	0.360	176	3		
3	0.350	177	0	<b>Pbar</b>	<b>29.90</b>
4	0.330	177	0		
5	0.300	177	-4	<b>Static Pressure</b>	<b>-0.33</b>
6	0.230	175	4		
0				<b>Pitot Coef.</b>	<b>0.84</b>
0					
0				<b>Start Time</b>	<b>843</b>
0					
0				<b>Stop Time</b>	<b>859</b>
2					
3				<b>Absolute Gas Pressure inches water</b>	<b>Ps = 29.88</b>
4					
5				<b>Dry Mole Fraction of Gas</b>	<b>Mfd = 0.70959</b>
6					
7				<b>Dry Molecular Weight of Gas lb/lb Mole</b>	<b>Md = 29.38</b>
8					
D-1				<b>Wet Molecular Weight of Gas lb/lb Mole</b>	<b>Ms = 26.08</b>
2					
3				<b>Average Gas Velocity ft/sec</b>	<b>vs = 34.58</b>
4					
5				<b>Dry Volumetric Gas Flow Rate</b>	
6				<b>at Standard Conditions SCFM</b>	<b>Qsd = 14745</b>
7					
8				<b>Wet Volumetric Flue Gas Flow Rate</b>	
E-1				<b>at Stack Conditions ACFM</b>	<b>Qaw = 24998</b>
2					
3				<b>Wet Volumetric Gas Flow Rate</b>	
4				<b>at Standard Conditions WSCFH</b>	<b>WSCFH = 1246788</b>
5					
6				LKCH	
7				Pre	6-5 good
8				Post	5-3 good

Dryer 2 Run 2

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		20	
Plant	Wiggins			Date		10/13/13	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Dryer 2			Pitot ID		6Pext	
<b>Averages</b>	<b>0.300</b>	<b>154.9</b>		Thermocouple ID		TC25	
	<b>Delta P</b>	<b>Temp</b>					
<b>Point No.</b>	<b>In Water</b>	<b>Deg F</b>					
A-1	0.200	167		<b>Oxygen %</b>		<b>17</b>	
2	0.800	167					
3	0.310	167		<b>Carbon Dioxide %</b>		<b>4</b>	
4	0.330	168					
5	0.340	169		<b>Moisture %</b>		<b>29.86</b>	
6	0.200	167					
B-1	0.220	170		<b>Stack Area sq.in.</b>		<b>1734.94</b>	
2	0.310	170					
3	0.310	2		<b>Pbar</b>		<b>29.90</b>	
4	0.290	170					
5	0.260	171		<b>Static Pressure</b>		<b>-0.33</b>	
6	0.190	171					
0				<b>Pitot Coef.</b>		<b>0.84</b>	
0							
0				<b>Start Time</b>		<b>1047</b>	
0							
0				<b>Stop Time</b>		<b>1051</b>	
2							
3				<b>Absolute Gas Pressure inches water</b>	<b>Ps =</b>	<b>29.88</b>	
4							
5				<b>Dry Mole Fraction of Gas</b>	<b>Mfd =</b>	<b>0.70135</b>	
6							
7				<b>Dry Molecular Weight of Gas lb/lb Mole</b>	<b>Md =</b>	<b>29.32</b>	
8							
D-1				<b>Wet Molecular Weight of Gas lb/lb Mole</b>	<b>Ms =</b>	<b>25.94</b>	
2							
2				<b>Average Gas Velocity ft/sec</b>	<b>vs =</b>	<b>35.02</b>	
4							
5				<b>Dry Volumetric Gas Flow Rate</b>			
6				<b>at Standard Conditions SCFM</b>	<b>Qsd =</b>	<b>15224</b>	
7							
8				<b>Wet Volumetric Flue Gas Flow Rate</b>			
E-1				<b>at Stack Conditions ACFM</b>	<b>Qaw =</b>	<b>25318</b>	
2							
3				<b>Wet Volumetric Gas Flow Rate</b>			
4				<b>at Standard Conditions WSCFH</b>	<b>WSCFH =</b>	<b>1302430</b>	
5							
6				LKCH			
7				Pre	6-5	good	
8				Post	5-3	good	

Dryer 2 Run 3

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		21	
Plant	Wiggins			Date		10/13/13	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Dryer 2			Pitot ID		6Pext	
<b>Averages</b>	<b>0.291</b>	<b>171.8</b>		Thermocouple ID		TC25	
	<b>Delta P</b>	<b>Temp</b>					
<b>Point No.</b>	<b>In Water</b>	<b>Deg F</b>					
A-1	0.220	169		<b>Oxygen %</b>		<b>17</b>	
2	0.250	172					
3	0.320	173		<b>Carbon Dioxide %</b>		<b>4</b>	
4	0.320	174					
5	0.330	174		<b>Moisture %</b>		<b>29.64</b>	
6	0.260	168					
B-1	0.240	168		<b>Stack Area sq.in.</b>		<b>1734.94</b>	
2	0.310	171		<b>Pbar</b>		<b>29.90</b>	
3	0.340	172					
4	0.330	172		<b>Static Pressure</b>		<b>-0.33</b>	
5	0.310	173					
6	0.280	175		<b>Pitot Coef.</b>		<b>0.84</b>	
0							
0				<b>Start Time</b>		<b>1208</b>	
0							
0				<b>Stop Time</b>		<b>1215</b>	
2							
3				<b>Absolute Gas Pressure inches water</b>	<b>Ps =</b>	<b>29.88</b>	
4							
5				<b>Dry Mole Fraction of Gas</b>	<b>Mfd =</b>	<b>0.70356</b>	
6							
7				<b>Dry Molecular Weight of Gas lb/lb Mole</b>	<b>Md =</b>	<b>29.32</b>	
8							
D-1				<b>Wet Molecular Weight of Gas lb/lb Mole</b>	<b>Ms =</b>	<b>25.96</b>	
2							
2				<b>Average Gas Velocity ft/sec</b>	<b>vs =</b>	<b>34.97</b>	
4							
5				<b>Dry Volumetric Gas Flow Rate</b>			
6				<b>at Standard Conditions SCFM</b>	<b>Qsd =</b>	<b>14842</b>	
7							
8				<b>Wet Volumetric Flue Gas Flow Rate</b>			
E-1				<b>at Stack Conditions ACFM</b>	<b>Qaw =</b>	<b>25278</b>	
2							
3				<b>Wet Volumetric Gas Flow Rate</b>			
4				<b>at Standard Conditions WSCFH</b>	<b>WSCFH =</b>	<b>1265741</b>	
5							
6				LKCH			
7				Pre	3-4	good	
8				Post	5-3	good	

**Method 1 - Air Control Techniques, P.C.**

Date

10/10/2013

Client	Enviva
Job #	1911
Plant Name	Wiggins
State	Mississippi
City	Wiggins
Sampling Location	Green Hammermill
No. of Ports Available	2
No. of Ports Used	1
Port Inside Diameter, Inches	3
Distance From Far Wall To Outside Of Port, Inches	30
Nipple Length And/Or Wall Thickness, Inches	3
Depth Of Stack Or Duct, Inches	27
Stack Or Duct Width (if rectangular), Inches	
Equiv. Diameter = 2DW/(D+W), Inches	27
Stack/Duct Area, Square Feet	3.9761
(□ x R <sup>2</sup> or L x W)	
	Upstream Downstream
Distance to Flow Disturbances, Inches	348 60
Diameters	12.89 2.22

Note: If more than 8 and 2 diameters and if duct dia. is less than 24" use 8 or 9 points.

Velocity	UP	Down	Particulate
12	8	2	12
12	7	1.75	12
12	6	1.5	16
16	5	1.25	20
16	2	0.5	24 or 25

Location of Points in Circular Stacks or Ducts											
	4	6	8	10	12	14	16	18	20	22	24
1	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	25.0	14.6	10.6	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2
3	75.0	29.6	19.4	14.6	11.8	9.9	8.5	7.5	6.7	6.0	5.5
4	93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7	7.9
5		85.4	67.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6	10.5
6		95.6	80.6	65.8	35.6	26.9	22.0	18.8	16.5	14.6	13.2
7			89.5	77.4	64.4	36.6	28.3	23.6	20.4	18.0	16.1
8			96.8	85.4	75.0	63.4	37.5	29.6	25.0	21.8	19.4
9				91.8	82.3	73.1	62.5	38.2	30.6	26.2	23.0
10				97.4	88.2	79.9	71.7	61.8	38.8	31.5	27.2
11					93.3	85.4	78.0	70.4	61.2	39.3	32.3
12					97.9	90.1	83.1	76.4	69.4	60.7	39.8
13						94.3	87.6	81.2	75.0	68.5	60.2
14						98.2	91.5	85.4	79.6	73.8	67.7
15							95.1	89.1	83.5	78.2	72.8
16							98.4	92.5	87.1	82.0	77.0
17								95.6	90.3	85.4	80.6
18								98.6	93.3	88.4	83.9
19									96.1	91.3	86.8
20									98.7	94.0	89.5
21										96.5	92.1
22										98.9	94.5
23											96.8
24											98.9

2 diff nipples probe marked to inside of port

Point Location Data			
Point	% of Duct Depth	Distance From Inside Wall	Distance From Outside of Port
1	4.4	1 2/8	4 2/8
2	14.6	4	7
3	29.6	8	11
4	70.4	19	22
5	85.4	23	26
6	95.6	25 6/8	28 6/8
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

Location of Points in Rectangular Stacks or Ducts											
	2	3	4	5	6	7	8	9	10	11	12
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
2	75		50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6
3		83.3		62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7
4			87.5		70.0	58.3	50	43.8	28.9	35.0	31.8
5				90.0		75	64.3	56.3	50	45.0	40.9
6					91.7		78.6	68.8	61.1	55.0	50
7						92.9		81.3	72.2	65.0	59.1
8							93.8		83.3	75.0	68.2
9								94.4		85.0	77.3
10									95.0		86.4
11										95.5	
12											95.8

- 0.0000 - 0.0625 - 0
- 0.0625 - 0.1875 - 1/8
- 0.1875 - 0.3125 - 1/4
- 0.3125 - 0.4375 - 3/8
- 0.4375 - 0.5625 - 1/2
- 0.5625 - 0.6875 - 5/8
- 0.6875 - 0.8125 - 3/4
- 0.8125 - 0.9375 - 7/8
- 0.9375 - 1.0000 - 1

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client		Enviva		ACT Run Number		1	
Plant		Wiggins		Date		10/10/2013	
City/State		Wiggins, MS		Gauge ID		909033	
Location		Green Hammermill		Pitot ID		4Pext	
Averages		3.961 70.8		Thermocouple ID		TC25	
		Delta P		Temp			
Point No.		In Water		Deg F		Angle	
A-1		2.800		71		0	
2		3.900		71		1	
3		4.400		71		1	
4		3.800		71		2	
5		3.800		70		4	
6		3.000		70		3	
B-1		4.200		72		0	
2		4.500		71		0	
3		4.600		71		0	
4		4.600		70		2	
5		4.400		71		4	
6		3.800		70		3	
0						Oxygen %	
0						20.9	
0						Carbon Dioxide %	
0						0	
0						Moisture %	
0						3.41	
0						Stack Area sq.in.	
0						572.5552696	
0						Pbar	
0						29.90	
0						Static Pressure	
0						-20.8	
0						Pitot Coef.	
0						0.84	
0						Start Time	
0						855	
0						Stop Time	
0						908	
2						Absolute Gas Pressure inches water	
3						Ps =	
4						28.37	
5						Dry Mole Fraction of Gas	
6						Mfd =	
7						0.96585	
8						Dry Molecular Weight of Gas lb/lb Mole	
D-1						Md =	
2						28.84	
3						Wet Molecular Weight of Gas lb/lb Mole	
4						Ms =	
5						28.47	
6						Average Gas Velocity ft/sec	
7						vs =	
8						115.87	
E-1						Dry Volumetric Gas Flow Rate	
2						at Standard Conditions SCFM	
3						Qsd =	
4						25184	
5						Wet Volumetric Flue Gas Flow Rate	
6						at Stack Conditions ACFM	
7						Qaw =	
8						27642	
0						Wet Volumetric Gas Flow Rate	
0						at Standard Conditions WSCFH	
0						WSCFH =	
0						1564487	
6						LKCH	
7						Pre	
8						3-4	
0						good	
0						Post	
0						5-3	
0						good	

GHM Run 2

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911		
Client		Enviva		ACT Run Number		2		
Plant		Wiggins		Date		10/10/2013		
City/State		Wiggins, MS		Gauge ID		909033		
Location		Green Hammermill		Pitot ID		4Pext		
Averages		3.854 70.6		Thermocouple ID		TC25		
		Delta P						
		Temp						
Point No.		In Water		Deg F				
A-1		2.700		71		Oxygen %		20.9
2		3.800		71		Carbon Dioxide %		0
3		4.400		71		Moisture %		3.62
4		3.800		70		Stack Area sq.in.		572.5552696
5		3.300		70		Pbar		29.90
6		3.100		68		Static Pressure		-20.8
B-1		3.900		72		Pitot Coef.		0.84
2		4.200		70		Start Time		1026
3		4.400		70		Stop Time		1030
4		4.400		70		Absolute Gas Pressure inches water		Ps = 28.37
5		4.300		71		Dry Mole Fraction of Gas		Mfd = 0.96382
6		4.200		73		Dry Molecular Weight of Gas lb/lb Mole		Md = 28.84
0						Wet Molecular Weight of Gas lb/lb Mole		Ms = 28.44
0						Average Gas Velocity ft/sec		vs = 114.32
0						Dry Volumetric Gas Flow Rate at Standard Conditions SCFM		Qsd = 24803
0						Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM		Qaw = 27273
2						Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH		WSCFH = 1544072
3						LKCH		
4						Pre		3-4 good
5						Post		5-3 good
6								
7								
8								
0								
0								

Air Control Techniques EPA Method 2 Data Sheet			ACT Job Number	1911
Client	Enviva		ACT Run Number	3
Plant	Wiggins		Date	10/10/2013
City/State	Wiggins, MS		Gauge ID	909033
Location	Green Hammermill		Pitot ID	4Pext
<b>Averages</b>	<b>3.847</b>	<b>70.9</b>	Thermocouple ID	TC25
	<b>Delta P</b>	<b>Temp</b>		
<b>Point No.</b>	<b>In Water</b>	<b>Deg F</b>		
A-1	2.700	71	<b>Oxygen %</b>	<b>20.9</b>
2	3.600	71	<b>Carbon Dioxide %</b>	<b>0</b>
3	4.400	71	<b>Moisture %</b>	<b>2.37</b>
4	3.700	71	<b>Stack Area sq.in.</b>	<b>572.5552696</b>
5	3.200	71	<b>Pbar</b>	<b>29.90</b>
6	3.300	69	<b>Static Pressure</b>	<b>-20.8</b>
B-1	4.000	72	<b>Pitot Coef.</b>	<b>0.84</b>
2	4.300	71	<b>Start Time</b>	<b>1141</b>
3	4.300	71	<b>Stop Time</b>	<b>1144</b>
4	4.300	71		
5	4.300	71		
6	4.300	71		
0				
0				
0				
0				
2				
3			<b>Absolute Gas Pressure inches water</b>	<b>Ps = 28.37</b>
4			<b>Dry Mole Fraction of Gas</b>	<b>Mfd = 0.97626</b>
5			<b>Dry Molecular Weight of Gas lb/lb Mole</b>	<b>Md = 28.84</b>
6			<b>Wet Molecular Weight of Gas lb/lb Mole</b>	<b>Ms = 28.58</b>
7			<b>Average Gas Velocity ft/sec</b>	<b>vs = 113.97</b>
8			<b>Dry Volumetric Gas Flow Rate at Standard Conditions SCFM</b>	<b>Qsd = 25031</b>
D-1			<b>Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM</b>	<b>Qaw = 27189</b>
2			<b>Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH</b>	<b>WSCFH = 1538379</b>
3				
4				
5				
6			LKCH	
7			Pre	3-4 good
8			Post	6-4 good
0				
0				

**Method 1 - Air Control Techniques, P.C.**

Date

10/12/2013

Client	Enviva
Job #	1911
Plant Name	Wiggins
State	Mississippi
City	Wiggins
Sampling Location	Pellet Mill 2 Aspiration
No. of Ports Available	1
No. of Ports Used	1
Port Inside Diameter, Inches	1
Distance From Far Wall To Outside Of Port, Inches	6
Nipple Length And/Or Wall Thickness, Inches	0
Depth Of Stack Or Duct, Inches	6
Stack Or Duct Width (if rectangular), Inches	
Equiv. Diameter = 2DW/(D+W), Inches	6
Stack/Duct Area, Square Feet	0.20
(□ x R <sup>2</sup> or L x W)	
	Upstream    Downstream
Distance to Flow Disturbances, Inches	19            39
Diameters	3.17           6.50

Note: If more than 8 and 2 diameters and if duct dia. is less than 24" use 8 or 9 points.

Velocity	Diameters			
	UP	Down	Particulate	
12	8	2		12
12	7	1.75		12
12	6	1.5		16
16	5	1.25		20
16	2	0.5		24 or 25

Location of Points in Circular Stacks or Ducts

	4	6	8	10	12	14	16	18	20	22	24
1	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	25.0	14.6	10.6	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2
3	75.0	29.6	19.4	14.6	11.8	9.9	8.5	7.5	6.7	6.0	5.5
4	93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7	7.9
5		85.4	67.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6	10.5
6		95.6	80.6	65.8	35.6	26.9	22.0	18.8	16.5	14.6	13.2
7			89.5	77.4	64.4	36.6	28.3	23.6	20.4	18.0	16.1
8			96.8	85.4	75.0	63.4	37.5	29.6	25.0	21.8	19.4
9				91.8	82.3	73.1	62.5	38.2	30.6	26.2	23.0
10				97.4	88.2	79.9	71.7	61.8	38.8	31.5	27.2
11					93.3	85.4	78.0	70.4	61.2	39.3	32.3
12					97.9	90.1	83.1	76.4	69.4	60.7	39.8
13						94.3	87.6	81.2	75.0	68.5	60.2
14						98.2	91.5	85.4	79.6	73.8	67.7
15							95.1	89.1	83.5	78.2	72.8
16							98.4	92.5	87.1	82.0	77.0
17								95.6	90.3	85.4	80.6
18								98.6	93.3	88.4	83.9
19									96.1	91.3	86.8
20									98.7	94.0	89.5
21										96.5	92.1
22										98.9	94.5
23											96.8
24											98.9

Point Location Data

Point	% of Duct Depth	Distance From Inside Wall	Distance From Outside of Port
1	6.7	3/8	1
2	25.0	1 4/8	1 4/8
3	75.0	4 4/8	4 4/8
4	93.3	5 5/8	5
5			
6			
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

Used 8 points because of diameter otherwise first 3 points are at 1" from wall

Location of Points in Rectangular Stacks or Ducts

	2	3	4	5	6	7	8	9	10	11	12
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.5
3		83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8
4			87.5	70.0	58.3	50	43.8	28.9	35.0	31.8	29.2
5				90.0	75	64.3	56.3	50	45.0	40.9	37.5
6					91.7	78.6	68.8	61.1	55.0	50	45.8
7						92.9	81.3	72.2	65.0	59.1	54.2
8							93.8	83.3	75.0	68.2	62.5
9								94.4	85.0	77.3	70.8
10									95.0	86.4	79.2
11										95.5	87.5
12											96.8

- 0.0000 - 0.0625 - 0    0.5625 - 0.6875 - 5/8
- 0.0625 - 0.1875 - 1/8    0.6875 - 0.8125 - 3/4
- 0.1875 - 0.3125 - 1/4    0.8125 - 0.9375 - 7/8
- 0.3125 - 0.4375 - 3/8    0.9375 - 1.0000 - 1
- 0.4375 - 0.5625 - 1/2

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number	1911
Client	Enviva			ACT Run Number	16
Plant	Wiggins			Date	10/12/2013
City/State	Wiggins, MS			Gauge ID	909033
Location	Pellet Mill 2 Aspiration			Pitot ID	4Pext
<b>Averages</b>	<b>5.359</b>	<b>148.6</b>		Thermocouple ID	TC25
	<b>Delta P</b>	<b>Temp</b>			
<b>Point No.</b>	<b>In Water</b>	<b>Deg F</b>	<b>Angle</b>		
A-1	5.400	149	0	<b>Oxygen %</b>	<b>20.9</b>
2	5.700	148	0		
3	5.100	149	2	<b>Carbon Dioxide %</b>	<b>0</b>
4	5.000	149	1		
B-1	5.700	149	0	<b>Moisture %</b>	<b>27.67</b>
2	5.600	148	1		
3	5.400	149	2	<b>Stack Area sq.in.</b>	<b>28.2743343</b>
4	5.000	148	0		
0				<b>Pbar</b>	<b>29.85</b>
0					
0				<b>Static Pressure</b>	<b>-7.5</b>
0					
0				<b>Pitot Coef.</b>	<b>0.84</b>
0					
0				<b>Start Time</b>	<b>1445</b>
0					
0				<b>Stop Time</b>	<b>1448</b>
0					
0				<b>Absolute Gas Pressure inches water</b>	<b>Ps = 29.30</b>
0					
0				<b>Dry Mole Fraction of Gas</b>	<b>Mfd = 0.72332</b>
0					
0				<b>Dry Molecular Weight of Gas lb/lb Mole</b>	<b>Md = 28.84</b>
0					
0				<b>Wet Molecular Weight of Gas lb/lb Mole</b>	<b>Ms = 25.84</b>
0					
0				<b>Average Gas Velocity ft/sec</b>	<b>vs = 149.06</b>
0					
0				<b>Dry Volumetric Gas Flow Rate at Standard Conditions SCFM</b>	<b>Qsd = 1079</b>
0					
0				<b>Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM</b>	<b>Qaw = 1756</b>
0					
0				<b>Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH</b>	<b>WSCFH = 89506.7</b>
0					
0				LKCH	
0				Pre	4-3 good
8				Post	5-5 good

Air Control Techniques EPA Method 2 Data Sheet			ACT Job Number	1911
Client	Enviva		ACT Run Number	17
Plant	Wiggins		Date	10/12/13
City/State	Wiggins, MS		Gauge ID	909033
Location	Pellet Mill 2 Aspiration		Pitot ID	4Pext
<b>Averages</b>	<b>4.944</b>	<b>148.3</b>	Thermocouple ID	TC25
	<b>Delta P</b>	<b>Temp</b>		
<b>Point No.</b>	<b>In Water</b>	<b>Deg F</b>		
A-1	3.700	147	<b>Oxygen %</b>	<b>20.9</b>
2	5.500	149	<b>Carbon Dioxide %</b>	<b>0</b>
3	5.400	148	<b>Moisture %</b>	<b>29.33</b>
4	5.200	148	<b>Stack Area sq.in.</b>	<b>28.2743</b>
B-1	5.600	148	<b>Pbar</b>	<b>29.85</b>
2	4.800	148	<b>Static Pressure</b>	<b>-7.5</b>
3	4.900	149	<b>Pitot Coef.</b>	<b>0.84</b>
4	4.600	149	<b>Start Time</b>	<b>1611</b>
0			<b>Stop Time</b>	<b>1615</b>
0				
0			<b>Absolute Gas Pressure inches water</b>	<b>Ps = 29.30</b>
0			<b>Dry Mole Fraction of Gas</b>	<b>Mfd = 0.7067</b>
0			<b>Dry Molecular Weight of Gas lb/lb Mole</b>	<b>Md = 28.84</b>
0			<b>Wet Molecular Weight of Gas lb/lb Mole</b>	<b>Ms = 25.66</b>
0			<b>Average Gas Velocity ft/sec</b>	<b>vs = 143.63</b>
0			<b>Dry Volumetric Gas Flow Rate at Standard Conditions SCFM</b>	<b>Qsd = 1016</b>
0			<b>Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM</b>	<b>Qaw = 1692</b>
0			<b>Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH</b>	<b>WSCFH = 86302.3</b>
0				
0			LKCH	
0			Pre	4-3 good
8			Post	5-5 good

Air Control Techniques EPA Method 2 Data Sheet			ACT Job Number		1911
Client	Enviva		ACT Run Number		18
Plant	Wiggins		Date		10/12/13
City/State	Wiggins, MS		Gauge ID		909033
Location	Pellet Mill 2 Aspiration		Pitot ID		4Pext
<b>Averages</b>	<b>4.547</b>	<b>152.1</b>	Thermocouple ID		TC25
	<b>Delta P</b>	<b>Temp</b>			
<b>Point No.</b>	<b>In Water</b>	<b>Deg F</b>			
A-1	4.400	152	<b>Oxygen %</b>		<b>20.9</b>
2	4.600	153	<b>Carbon Dioxide %</b>		<b>0</b>
3	4.600	152	<b>Moisture %</b>		<b>28.19</b>
4	4.300	152	<b>Stack Area sq.in.</b>		<b>28.2743</b>
B-1	4.800	152	<b>Pbar</b>		<b>29.85</b>
2	5.000	152	<b>Static Pressure</b>		<b>-7.5</b>
3	4.400	153	<b>Pitot Coef.</b>		<b>0.84</b>
4	4.300	151	<b>Start Time</b>		<b>1739</b>
0			<b>Stop Time</b>		<b>1742</b>
0			<b>Absolute Gas Pressure inches water</b>		<b>Ps = 29.30</b>
0			<b>Dry Mole Fraction of Gas</b>		<b>Mfd = 0.71813</b>
0			<b>Dry Molecular Weight of Gas lb/lb Mole</b>		<b>Md = 28.84</b>
0			<b>Wet Molecular Weight of Gas lb/lb Mole</b>		<b>Ms = 25.78</b>
0			<b>Average Gas Velocity ft/sec</b>		<b>vs = 137.85</b>
0			<b>Dry Volumetric Gas Flow Rate at Standard Conditions SCFM</b>		<b>Qsd = 985</b>
0			<b>Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM</b>		<b>Qaw = 1624</b>
0			<b>Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH</b>		<b>WSCFH = 82302.1</b>
0					
0			LKCH		
0			Pre	4-3	good
8			Post	5-5	good

**Method 1 - Air Control Techniques, P.C.**

Date

10/11/2013

Client	Enviva
Job #	1911
Plant Name	Wiggins
State	Mississippi
City	Wiggins
Sampling Location	Dry Hammermill 2
No. of Ports Available	2
No. of Ports Used	2
Port Inside Diameter, Inches	0
Distance From Far Wall To Outside Of Port, Inches	22
Nipple Length And/Or Wall Thickness, Inches	0
Depth Of Stack Or Duct, Inches	22
Stack Or Duct Width (if rectangular), Inches	
Equiv. Diameter = 2DW/(D+W), Inches	22
Stack/Duct Area, Square Feet	2.6
(□ x R <sup>2</sup> or L x W)	
	Upstream Downstream
Distance to Flow Disturbances, inches	52 8
Diameters	2.36 0.36

Note: If more than 8 and 2 diameters and if duct dia. is less than 24" use 8 or 9 points.

Diameters			
Velocity	UP	Down	Particulate
12	8	2	12
12	7	1.75	12
12	6	1.5	16
16	5	1.25	20
16	2	0.5	24 or 25

Location of Points in Circular Stacks or Ducts											
	4	6	8	10	12	14	16	18	20	22	24
1	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	25.0	14.6	10.6	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2
3	75.0	29.6	19.4	14.6	11.8	9.9	8.5	7.5	6.7	6.0	5.5
4	93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7	7.9
5		85.4	67.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6	10.5
6		95.6	80.6	65.8	35.6	26.9	22.0	18.8	16.5	14.6	13.2
7			89.5	77.4	64.4	36.6	28.3	23.6	20.4	18.0	16.1
8			96.8	85.4	75.0	63.4	37.5	29.6	25.0	21.8	19.4
9				91.8	82.3	73.1	62.5	38.2	30.6	26.2	23.0
10				97.4	88.2	79.9	71.7	61.8	38.8	31.5	27.2
11					93.3	85.4	78.0	70.4	61.2	39.3	32.3
12					97.9	90.1	83.1	76.4	69.4	60.7	39.8
13						94.3	87.6	81.2	75.0	68.5	60.2
14						98.2	91.5	85.4	79.6	73.8	67.7
15							95.1	89.1	83.5	78.2	72.8
16							98.4	92.5	87.1	82.0	77.0
17								95.6	90.3	85.4	80.6
18								98.6	93.3	88.4	83.9
19									96.1	91.3	86.8
20									98.7	94.0	89.5
21										96.5	92.1
22										98.9	94.5
23											96.8
24											98.9

2 diff nipples probe marked to inside of port

Point Location Data			
Point	% of Duct Depth	Distance From Inside Wall	Distance From Outside of Port
1	3.2	6/8	6/8
2	10.6	2 3/8	2 3/8
3	19.4	4 2/8	4 2/8
4	32.3	7 1/8	7 1/8
5	67.7	14 7/8	14 7/8
6	80.6	17 6/8	17 6/8
7	89.5	19 6/8	19 6/8
8	96.8	21 2/8	21 2/8
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

Location of Points in Rectangular Stacks or Ducts											
	2	3	4	5	6	7	8	9	10	11	12
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.5
3		83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8
4			87.5	70.0	58.3	50	43.8	28.9	35.0	31.8	29.2
5				90.0	75	64.3	56.3	50	45.0	40.9	37.5
6					91.7	78.6	68.8	61.1	55.0	50	45.8
7						92.9	81.3	72.2	65.0	59.1	54.2
8							93.8	83.3	75.0	68.2	62.5
9								94.4	85.0	77.3	70.8
10									95.0	86.4	78.2
11										95.5	87.5
12											95.8

- 0.0000 - 0.0625 - 0
- 0.0625 - 0.1875 - 1/8
- 0.1875 - 0.3125 - 1/4
- 0.3125 - 0.4375 - 3/8
- 0.4375 - 0.5625 - 1/2
- 0.5625 - 0.6875 - 5/8
- 0.6875 - 0.8125 - 3/4
- 0.8125 - 0.9375 - 7/8
- 0.9375 - 1.0000 - 1

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client		Enviva		ACT Run Number		10	
Plant		Wiggins		Date		10/11/2013	
City/State		Wiggins, MS		Gauge ID		909033	
Location		Dry Hammermill 2		Pitot ID		4Pext	
Averages		2.601 122.4		Thermocouple ID		TC25	
		Delta P		Temp			
Point No.		In Water		Deg F		Angle	
A-1		2.400		121		0	
2		2.600		122		1	
3		2.550		122		0	
4		2.400		123		0	
5		2.600		123		2	
6		3.000		122		0	
7		3.000		121		0	
8		3.300		120		0	
B-1		2.200		122		2	
2		2.200		122		0	
3		2.300		123		1	
4		2.300		123		0	
5		2.800		123		2	
6		2.700		123		0	
7		2.800		125		1	
8		2.600		124		1	
0							
2							
3							
4							
5							
6							
7							
8							
D-1							
2							
3							
4							
5							
6							
7							
8							
E-1							
2							
3							
4							
5							
6							
7							
8							
0							
0							
				Absolute Gas Pressure inches water		Ps = 29.90	
				Dry Mole Fraction of Gas		Mfd = 0.95746	
				Dry Molecular Weight of Gas lb/lb Mole		Md = 28.84	
				Wet Molecular Weight of Gas lb/lb Mole		Ms = 28.38	
				Average Gas Velocity ft/sec		vs = 95.95	
				Dry Volumetric Gas Flow Rate at Standard Conditions SCFM		Qsd = 13183	
				Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM		Qaw = 15197	
				Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH		WSCFH = 826137	
				LKCH			
				Pre		4-3 good	
				Post		5-5 good	

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number	1911
Client	Enviva			ACT Run Number	11
Plant	Wiggins			Date	10/11/2001
City/State	Wiggins, MS			Gauge ID	909033
Location	Dry Hammermill 2			Pitot ID	4Pext
<b>Averages</b>	<b>2.308</b>	<b>128.2</b>		Thermocouple ID	TC25
	<b>Delta P</b>	<b>Temp</b>			
<b>Point No.</b>	<b>In Water</b>	<b>Deg F</b>			
A-1	2.200	124		<b>Oxygen %</b>	<b>20.9</b>
2	2.150	127			
3	2.000	129		<b>Carbon Dioxide %</b>	<b>0</b>
4	2.100	129			
5	2.000	129		<b>Moisture %</b>	<b>4.18</b>
6	2.600	130			
7	2.600	130		<b>Stack Area sq.in.</b>	<b>380.132717</b>
8	2.600	129			
B-1	1.800	129		<b>Pbar</b>	<b>29.80</b>
2	2.200	127			
3	2.200	128		<b>Static Pressure</b>	<b>1.4</b>
4	2.300	128			
5	2.600	128		<b>Pitot Coef.</b>	<b>0.84</b>
6	2.500	128			
7	2.600	128		<b>Start Time</b>	<b>1917</b>
8	2.600	128			
0				<b>Stop Time</b>	<b>1923</b>
2					
3				<b>Absolute Gas Pressure inches water</b>	<b>Ps = 29.90</b>
4					
5				<b>Dry Mole Fraction of Gas</b>	<b>Mfd = 0.95816</b>
6					
7				<b>Dry Molecular Weight of Gas lb/lb Mole</b>	<b>Md = 28.84</b>
8					
D-1				<b>Wet Molecular Weight of Gas lb/lb Mole</b>	<b>Ms = 28.38</b>
2					
3				<b>Average Gas Velocity ft/sec</b>	<b>vs = 90.82</b>
4					
5				<b>Dry Volumetric Gas Flow Rate</b>	
6				<b>at Standard Conditions SCFM</b>	<b>Qsd = 12366</b>
7					
8				<b>Wet Volumetric Flue Gas Flow Rate</b>	
E-1				<b>at Stack Conditions ACFM</b>	<b>Qaw = 14385</b>
2					
3				<b>Wet Volumetric Gas Flow Rate</b>	
4				<b>at Standard Conditions WSCFH</b>	<b>WSCFH = 774351</b>
5					
6				LKCH	
7				Pre	4-3 good
8				Post	5-5 good
0					
0					

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client		Enviva		ACT Run Number		12	
Plant		Wiggins		Date		10/11/2013	
City/State		Wiggins, MS		Gauge ID		909033	
Location		Dry Hammermill 2		Pitot ID		4Pext	
Averages		2.618 116.4		Thermocouple ID		TC25	
		Delta P		Temp			
Point No.		In Water		Deg F			
A-1	2.700	114		Oxygen %		20.9	
2	2.700	116		Carbon Dioxide %		0	
3	2.700	116		Moisture %		4.18	
4	2.500	117		Stack Area sq.in.		380.1327167	
5	2.800	117		Pbar		29.80	
6	2.800	118		Static Pressure		1.4	
7	3.000	117		Pitot Coef.		0.84	
8	2.900	116		Start Time		2038	
B-1	3.000	117		Stop Time		2043	
2	2.900	116					
3	2.600	117		Absolute Gas Pressure inches water	Ps =	29.90	
4	2.500	116		Dry Mole Fraction of Gas	Mfd =	0.95816	
5	2.300	116		Dry Molecular Weight of Gas lb/lb Mole	Md =	28.84	
6	2.300	116		Wet Molecular Weight of Gas lb/lb Mole	Ms =	28.38	
7	2.100	116		Average Gas Velocity ft/sec	vs =	95.74	
8	2.200	117		Dry Volumetric Gas Flow Rate at Standard Conditions SCFM	Qsd =	13303	
0				Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM	Qaw =	15165	
2				Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH	WSCFH =	833051	
3							
4							
5							
6				LKCH			
7				Pre	4-3		good
8				Post	5-5		good
0							
0							

Air Control Techniques, PC: Emissions Calculations

Enviva, Wiggins, MS	Job 1911	Pellet Mill 2 Cooler 7	Pellet Mill 2 Cooler 8	Pellet Mill 2 Cooler 9	Pellet Mill 1 Cooler 13	Pellet Mill 1 Cooler 14	Pellet Mill 1 Cooler 15
<b>PARAMETER</b>	<b>NOMENCLATURE</b>						
Sampling Location		Pellet Mill 2 Cooler	Pellet Mill 2 Cooler	Pellet Mill 2 Cooler	Pellet Mill 1 Cooler	Pellet Mill 1 Cooler	Pellet Mill 1 Cooler
Date		10/11/2013	10/11/2013	10/11/2013	10/12/2013	10/12/2013	10/12/2013
Run Time	$\theta$	60	60	60	60	60	60
Nozzle Diameter	inches	N/A	N/A	N/A	N/A	N/A	N/A
Stack Area	As - sq. ft.	2.4	2.4	2.4	5.81	5.8	5.8
Pitot Tube Coefficient	Cp	0.84	0.84	0.84	0.84	0.84	0.84
Meter Calibration Factor	Y	0.9828	0.9828	0.9828	0.9828	0.9828	0.9828
Barometric Pressure, inches Hg	Bp - in Hg	29.80	29.80	29.80	29.90	29.90	29.90
Static Pressure	Pg - in. H <sub>2</sub> O	-1.2	-1.2	-1.2	-0.4	-0.4	-0.4
Stack Pressure	Ps	29.71	29.71	29.71	29.87	29.87	29.87
Meter Box Pressure Differential	$\Delta H$ - in. H <sub>2</sub> O	1.00	1.00	1	1.00	1.00	1.00
Average Velocity Head	$\Delta p$ - in. H <sub>2</sub> O	2.293	2.102	2.108	0.654	0.644	0.634
Volume of Gas Sampled	Vm - cu. ft.	34.310	34.423	33.681	33.818	35.845	34.567
Dry Gas Meter Temperature	Tm - °F	87.3	89.3	83.8	71.8	82.5	89.0
Stack Temperature	Ts - °F	148.9	143.2	152.3	82.3	94.8	97.7
Liquid Collected	Grams	35.2	33.5	32.4	24.3	27.8	19.9
Carbon Dioxide	% CO <sub>2</sub>	0	0	0	0	0	0
Oxygen	% O <sub>2</sub>	20.9	20.9	20.9	20.9	20.9	20.9
Carbon Monoxide	% CO	0	0	0	0	0	0
Nitrogen	% N <sub>2</sub>	79.1	79.1	79.1	79.1	79.1	79.1
Volume of Gas Sampled, Dry	Vmstd - cu. ft.	32.483	32.472	32.093	33.061	34.348	32.731
Volume of Water Vapor	Vwstd - cu. ft.	1.660	1.580	1.528	1.146	1.311	0.938
Moisture Content	% H <sub>2</sub> O	4.86	4.64	4.54	3.35	3.68	2.79
Saturation Moisture	% H <sub>2</sub> O	24.8	21.4	26.9	3.7	5.5	6.0
Dry Mole Fraction	Mfd	0.951	0.954	0.955	0.967	0.963	0.972
Gas Molecular Weight, Dry	Md	28.84	28.84	28.84	28.84	28.84	28.84
Gas Molecular Weight, Wet	Ms	28.31	28.33	28.34	28.47	28.44	28.53
Gas Velocity	vs - ft./sec.	92.52	88.13	88.91	46.36	46.58	46.26
Volumetric Air Flow, Actual	Qaw - ACFM	13,352	12,718	12,831	16,168	16,246	16,134
Volumetric Air Flow, Standard	Qsd - DSCFM	10,938	10,543	10,488	15,189	14,870	14,825

**Method 1 - Air Control Techniques, P.C.**

Date

10/12/2013

Client	Enviva
Job #	1911
Plant Name	Wiggins
State	Mississippi
City	Wiggins
Sampling Location	Pellet Mill 1 Cooler
No. of Ports Available	6
No. of Ports Used	4
Port Inside Diameter, Inches	3
Distance From Far Wall To Outside Of Port, Inches	30.5
Nipple Length And/Or Wall Thickness, Inches	3.5
Depth Of Stack Or Duct, Inches	27
Stack Or Duct Width (if rectangular), Inches	31
Equiv. Diameter = 2DW/(D+W), Inches	28.86207
Stack/Duct Area, Square Feet	5.8
(□ x R <sup>2</sup> or L x W)	
	Upstream      Downstream
Distance to Flow Disturbances, Inches	72      48
Diameters	2.49      1.66

Note: If more than 8 and 2 diameters and if duct dia. is less than 24" use 8 or 9 points.

Velocity	UP	Down	Particulate
12	8	2	12
12	7	1.75	12
12	6	1.5	16
16	5	1.25	20
16	2	0.5	24 or 25

Location of Points in Circular Stacks or Ducts											
	4	6	8	10	12	14	16	18	20	22	24
1	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	25.0	14.6	10.6	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2
3	75.0	29.6	19.4	14.6	11.8	9.9	8.5	7.5	6.7	6.0	5.5
4	93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7	7.9
5		85.4	67.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6	10.5
6		95.6	80.6	65.8	35.6	26.9	22.0	18.8	16.5	14.6	13.2
7			89.5	77.4	64.4	36.6	28.3	23.6	20.4	18.0	16.1
8			96.8	85.4	75.0	63.4	37.5	29.6	25.0	21.8	19.4
9				91.8	82.3	73.1	62.5	38.2	30.6	26.2	23.0
10				97.4	88.2	79.9	71.7	61.8	38.8	31.5	27.2
11					93.3	85.4	78.0	70.4	61.2	39.3	32.3
12					97.9	90.1	83.1	76.4	69.4	60.7	39.8
13						94.3	87.6	81.2	75.0	68.5	60.2
14						98.2	91.5	85.4	79.6	73.8	67.7
15							95.1	89.1	83.5	78.2	72.8
16							98.4	92.5	87.1	82.0	77.0
17								95.6	90.3	85.4	80.6
18								98.6	93.3	88.4	83.9
19									96.1	91.3	86.8
20									98.7	94.0	89.5
21										96.5	92.1
22										98.9	94.5
23											96.8
24											98.9

2 diff nipples probe marked to inside of port

Point Location Data			
Point	% of Duct Depth	Distance From Inside Wall	Distance From Outside of Port
1	12.5	3 3/8	6 7/8
2	37.5	10 1/8	13 5/8
3	62.5	16 7/8	20 3/8
4	87.5	23 5/8	27 1/8
5			
6			
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

Location of Points in Rectangular Stacks or Ducts											
	2	3	4	5	6	7	8	9	10	11	12
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
2	75		50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6
3		83.3		62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7
4			87.5		70.0	58.3	50	43.8	28.9	35.0	31.8
5				90.0		75	64.3	56.3	50	45.0	40.9
6					91.7		78.6	68.8	61.1	55.0	50
7						92.9		81.3	72.2	65.0	59.1
8							93.8		83.3	75.0	68.2
9								94.4		85.0	77.3
10									95.0		86.4
11										95.5	87.5
12											95.8

- 0.0000 - 0.0625 - 0    0.5625 - 0.6875 - 5/8
- 0.0625 - 0.1875 - 1/8    0.6875 - 0.8125 - 3/4
- 0.1875 - 0.3125 - 1/4    0.8125 - 0.9375 - 7/8
- 0.3125 - 0.4375 - 3/8    0.9375 - 1.0000 - 1
- 0.4375 - 0.5625 - 1/2

Pellet Mill 1 Run 1

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number	1911
Client	Enviva			ACT Run Number	13
Plant	Wiggins			Date	10/12/2013
City/State	Mississippi			Gauge ID	909033
Location	Pellet Mill 1 Cooler			Pitot ID	4Pext
<b>Averages</b>	<b>0.654</b>	<b>82.3</b>		Thermocouple ID	4Pext
	<b>Delta P</b>	<b>Temp</b>			
<b>Point No.</b>	<b>In Water</b>	<b>Deg F</b>	<b>Angle</b>		
A-1	0.380	78	0	Oxygen %	20.9
2	0.340	79	0		
3	0.330	79	0	Carbon Dioxide %	0
4	0.340	77	2		
B-1	0.680	82	8	Moisture %	3.35
2	0.650	81	2		
3	0.540	82	-5	Stack Area sq.in.	837
4	0.570	82	3		
C-1	0.680	84	-2	Pbar	29.90
2	0.700	84	-3		
3	0.690	84	0	Static Pressure	-0.4
4	0.710	84	3		
D-1	1.050	85	0	Pitot Coef.	0.84
2	1.050	85	-2		
3	1.050	85	-1	Start Time	830
4	1.100	86	2	Stop Time	847
0					
0					
0				Absolute Gas Pressure inches water	Ps = 29.87
0					
0				Dry Mole Fraction of Gas	Mfd = 0.96651
0					
0				Dry Molecular Weight of Gas lb/lb Mole	Md = 28.84
0					
0				Wet Molecular Weight of Gas lb/lb Mole	Ms = 28.47
0					
0				Average Gas Velocity ft/sec	vs = 46.36
0					
0				Dry Volumetric Gas Flow Rate	
0				at Standard Conditions SCFM	Qsd = 15189
0					
0				Wet Volumetric Flue Gas Flow Rate	
0				at Stack Conditions ACFM	Qaw = 16168
0					
0				Wet Volumetric Gas Flow Rate	
0				at Standard Conditions WSCFH	WSCFH = 942901
0					
0				LKCH	
0				Pre	3-4 good
0				Post	5-3 good
#REF!					
#REF!					

Pellet Mill 1 Run 2

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number	1911
Client	Enviva			ACT Run Number	14
Plant	Wiggins			Date	10/12/2013
City/State	Mississippi			Gauge ID	909033
Location	Pellet Mill 1 Cooler			Pitot ID	4PEXT
<b>Averages</b>	<b>0.644</b>	<b>94.8</b>		Thermocouple ID	4PEXT
	<b>Delta P</b>	<b>Temp</b>			
<b>Point No.</b>	<b>In Water</b>	<b>Deg F</b>			
A-1	0.380	92		<b>Oxygen %</b>	<b>20.9</b>
2	0.400	93			
3	0.380	93		<b>Carbon Dioxide %</b>	<b>0</b>
4	0.370	93			
B-1	0.530	94		<b>Moisture %</b>	<b>3.68</b>
2	0.550	95			
3	0.480	95		<b>Stack Area sq.in.</b>	<b>837</b>
4	0.500	95			
C-1	0.670	95		<b>Pbar</b>	<b>29.90</b>
2	0.690	95			
3	0.660	96		<b>Static Pressure</b>	<b>-0.4</b>
4	0.680	96			
D-1	1.300	96		<b>Pitot Coef.</b>	<b>0.84</b>
2	1.050	96			
3	1.050	96		<b>Start Time</b>	<b>1009</b>
4	1.050	96			
0				<b>Stop Time</b>	<b>1015</b>
0					
0				<b>Absolute Gas Pressure inches water</b>	<b>Ps = 29.87</b>
0					
0				<b>Dry Mole Fraction of Gas</b>	<b>Mfd = 0.96324</b>
0					
0				<b>Dry Molecular Weight of Gas lb/lb Mole</b>	<b>Md = 28.84</b>
0					
0				<b>Wet Molecular Weight of Gas lb/lb Mole</b>	<b>Ms = 28.44</b>
0					
0				<b>Average Gas Velocity ft/sec</b>	<b>vs = 46.58</b>
0					
0				<b>Dry Volumetric Gas Flow Rate at Standard Conditions SCFM</b>	<b>Qsd = 14870</b>
0					
0				<b>Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM</b>	<b>Qaw = 16246</b>
0					
0				<b>Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH</b>	<b>WSCFH = 926248</b>
0					
0				LKCH	
0				Pre	3-4 good
0				Post	5-3 good
#REF!					
#REF!					

Pellet Mill 1 Run 3

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number	1911
Client	Enviva			ACT Run Number	15
Plant	Wiggins			Date	10/12/2013
City/State	Mississippi			Gauge ID	909033
Location	Pellet Mill 1 Cooler			Pitot ID	4Pext
<b>Averages</b>	<b>0.634</b>	<b>97.7</b>		Thermocouple ID	4Pext
	<b>Delta P</b>	<b>Temp</b>			
<b>Point No.</b>	<b>In Water</b>	<b>Deg F</b>			
A-1	0.340	94		<b>Oxygen %</b>	<b>20.9</b>
2	0.290	96			
3	0.280	97		<b>Carbon Dioxide %</b>	<b>0</b>
4	0.330	97			
B-1	0.530	98		<b>Moisture %</b>	<b>2.79</b>
2	0.540	98			
3	0.500	98		<b>Stack Area sq.in.</b>	<b>837</b>
4	0.480	98			
C-1	0.730	98		<b>Pbar</b>	<b>29.90</b>
2	0.740	98			
3	0.670	98		<b>Static Pressure</b>	<b>-0.4</b>
4	0.670	99			
D-1	1.400	98		<b>Pitot Coef.</b>	<b>0.84</b>
2	1.050	99			
3	1.000	99		<b>Start Time</b>	<b>1125</b>
4	1.200	98			
0				<b>Stop Time</b>	<b>1134</b>
0					
0				<b>Absolute Gas Pressure inches water</b>	<b>Ps = 29.87</b>
0					
0				<b>Dry Mole Fraction of Gas</b>	<b>Mfd = 0.97213</b>
0					
0				<b>Dry Molecular Weight of Gas lb/lb Mole</b>	<b>Md = 28.84</b>
0					
0				<b>Wet Molecular Weight of Gas lb/lb Mole</b>	<b>Ms = 28.53</b>
0					
0				<b>Average Gas Velocity ft/sec</b>	<b>vs = 46.26</b>
0					
0				<b>Dry Volumetric Gas Flow Rate at Standard Conditions SCFM</b>	<b>Qsd = 14825</b>
0					
0				<b>Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM</b>	<b>Qaw = 16134</b>
0					
0				<b>Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH</b>	<b>WSCFH = 915021</b>
0					
0				LKCH	
0				Pre	3-4 good
0				Post	5-3 good
#REF!					
#REF!					

**Method 1 - Air Control Techniques, P.C.**

Date

10/11/2013

Client	Enviva
Job #	1911
Plant Name	Wiggins
State	Mississippi
City	Wiggins
Sampling Location	Pellet Mill 2 Cooler
No. of Ports Available	2
No. of Ports Used	2
Port Inside Diameter, Inches	3
Distance From Far Wall To Outside Of Port, Inches	21
Nipple Length And/Or Wall Thickness, Inches	0
Depth Of Stack Or Duct, Inches	21
Stack Or Duct Width (if rectangular), Inches	
Equiv. Diameter = 2DW/(D+W), Inches	21
Stack/Duct Area, Square Feet	2.4
(□ x R <sup>2</sup> or L x W)	
	Upstream    Downstream
Distance to Flow Disturbances, inches	51            9.5
Diameters	2.43            0.45

Note: If more than 8 and 2 diameters and if duct dia. is less than 24" use 8 or 9 points.

Velocity	Diameters		Particulate
	UP	Down	
12	8	2	12
12	7	1.75	12
12	6	1.5	16
16	5	1.25	20
16	2	0.5	24 or 25

Location of Points in Circular Stacks or Ducts

	4	6	8	10	12	14	16	18	20	22	24
1	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	25.0	14.6	10.6	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2
3	75.0	29.6	19.4	14.6	11.8	9.9	8.5	7.5	6.7	6.0	5.5
4	93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7	7.9
5		85.4	67.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6	10.5
6		95.6	80.6	65.8	35.6	26.9	22.0	18.8	16.5	14.6	13.2
7			89.5	77.4	64.4	36.6	28.3	23.6	20.4	18.0	16.1
8			96.8	85.4	75.0	63.4	37.5	29.6	25.0	21.8	19.4
9				91.8	82.3	73.1	62.5	38.2	30.6	26.2	23.0
10				97.4	88.2	79.9	71.7	61.8	38.8	31.5	27.2
11					93.3	85.4	78.0	70.4	61.2	39.3	32.3
12					97.9	90.1	83.1	76.4	69.4	60.7	39.8
13						94.3	87.6	81.2	75.0	68.5	60.2
14						98.2	91.5	85.4	79.6	73.8	67.7
15							95.1	89.1	83.5	78.2	72.8
16							98.4	92.5	87.1	82.0	77.0
17								95.6	90.3	85.4	80.6
18								98.6	93.3	88.4	83.9
19									96.1	91.3	86.8
20									98.7	94.0	89.5
21										96.5	92.1
22										98.9	94.5
23											96.8
24											98.9

2 diff nipples probe marked to inside of port

**Point Location Data**

Point	% of Duct	Distance From Inside Wall	Distance From Outside of Port
	Depth		
1	3.2	0.672	1
2	10.6	2.226	2 1/4
3	19.4	4.074	4 1/8
4	32.3	6.783	6 3/4
5	67.7	14.217	14 1/4
6	80.6	16.926	16 7/8
7	89.5	18.795	18 3/4
8	96.8	20.328	20
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

Location of Points in Rectangular Stacks or Ducts

	2	3	4	5	6	7	8	9	10	11	12
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.5
3		83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8
4			87.5	70.0	58.3	50	43.8	28.9	35.0	31.8	29.2
5				90.0	75	64.3	56.3	50	45.0	40.9	37.5
6					91.7	78.6	68.8	61.1	55.0	50	45.8
7						92.9	81.3	72.2	65.0	59.1	54.2
8							93.8	83.3	75.0	68.2	62.5
9								94.4	85.0	77.3	70.8
10									95.0	86.4	78.2
11										95.5	87.5
12											95.8

- 0.0000 - 0.0625 - 0    0.5625 - 0.6875 - 5/8
- 0.0625 - 0.1875 - 1/8    0.6875 - 0.8125 - 3/4
- 0.1875 - 0.3125 - 1/4    0.8125 - 0.9375 - 7/8
- 0.3125 - 0.4375 - 3/8    0.9375 - 1.0000 - 1
- 0.4375 - 0.5625 - 1/2

Pellet Mill 2 Cooler Run 1

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number	1911
Client	Enviva			ACT Run Number	7
Plant	Wiggins			Date	10/11/2013
City/State	Mississippi			Gauge ID	909033
Location	Pellet Mill 2 Cooler			Pitot ID	4PEXT
<b>Averages</b>	<b>2.293</b>	<b>148.9</b>		Thermocouple ID	4PEXT
	<b>Delta P</b>	<b>Temp</b>			
<b>Point No.</b>	<b>In Water</b>	<b>Deg F</b>	<b>Angle</b>		
A-1	1.800	150	-2	Oxygen %	20.9
2	2.400	153	-5		
3	2.800	150	-8	Carbon Dioxide %	0
4	2.900	150	-4		
5	2.800	150	6	Moisture %	4.86
6	2.500	150	5		
7	2.300	149	-2	Stack Area sq.in.	346.360595
8	1.900	144	-2		
B-1	2.300	142	8	Pbar	29.80
2	2.300	147	6		
3	2.500	149	7	Static Pressure	-1.2
4	2.500	149	6		
5	2.200	150	-5	Pitot Coef.	0.84
6	2.100	150	-4		
7	1.900	150	-2	Start Time	1315
8	1.700	150	-7	Stop Time	1335
#REF!					
#REF!					
#REF!				Absolute Gas Pressure inches water	Ps = 29.71
#REF!					
#REF!				Dry Mole Fraction of Gas	Mfd = 0.95139
#REF!					
#REF!				Dry Molecular Weight of Gas lb/lb Mole	Md = 28.84
#REF!					
#REF!				Wet Molecular Weight of Gas lb/lb Mole	Ms = 28.31
#REF!					
#REF!				Average Gas Velocity ft/sec	vs = 92.52
#REF!					
#REF!				Dry Volumetric Gas Flow Rate at Standard Conditions SCFM	Qsd = 10938
#REF!					
#REF!				Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM	Qaw = 13352
#REF!					
#REF!				Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH	WSCFH = 689797
#REF!					
#REF!				LKCH	
#REF!				Pre	3-4 good
#REF!				Post	5-3 good
#REF!					
#REF!					

Pellet Mill 2 Cooler Run 2

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number	1911
Client	Enviva			ACT Run Number	8
Plant	Wiggins			Date	10/11/2013
City/State	Mississippi			Gauge ID	909033
Location	Pellet Mill 2 Cooler			Pitot ID	4PEXT
<b>Averages</b>	<b>2.102</b>	<b>143.2</b>		Thermocouple ID	4PEXT
	<b>Delta P</b>	<b>Temp</b>			
<b>Point No.</b>	<b>In Water</b>	<b>Deg F</b>			
A-1	2.400	147		<b>Oxygen %</b>	<b>20.9</b>
2	2.300	143			
3	2.200	144		<b>Carbon Dioxide %</b>	<b>0</b>
4	2.000	144			
5	1.800	142		<b>Moisture %</b>	<b>4.64</b>
6	1.800	139			
7	1.800	140		<b>Stack Area sq.in.</b>	<b>346.360595</b>
8	1.700	140			
B-1	1.800	142		<b>Pbar</b>	<b>29.80</b>
2	2.050	144			
3	2.250	143		<b>Static Pressure</b>	<b>-1.2</b>
4	2.200	144			
5	2.300	144		<b>Pitot Coef.</b>	<b>0.84</b>
6	2.350	145			
7	2.400	145		<b>Start Time</b>	<b>1450</b>
8	2.400	145			
0				<b>Stop Time</b>	<b>1458</b>
0					
0				<b>Absolute Gas Pressure inches water</b>	<b>Ps = 29.71</b>
0					
0				<b>Dry Mole Fraction of Gas</b>	<b>Mfd = 0.95361</b>
0					
0				<b>Dry Molecular Weight of Gas lb/lb Mole</b>	<b>Md = 28.84</b>
0					
0				<b>Wet Molecular Weight of Gas lb/lb Mole</b>	<b>Ms = 28.33</b>
0					
0				<b>Average Gas Velocity ft/sec</b>	<b>vs = 88.13</b>
0					
0				<b>Dry Volumetric Gas Flow Rate at Standard Conditions SCFM</b>	<b>Qsd = 10543</b>
0					
0				<b>Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM</b>	<b>Qaw = 12718</b>
0					
0				<b>Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH</b>	<b>WSCFH = 663328</b>
0					
0				LKCH	
0				Pre	3-4 good
0				Post	5-3 good
#REF!					
#REF!					

Pellet Mill 2 Cooler Run 3

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number	1911
Client	Enviva			ACT Run Number	9
Plant	Wiggins			Date	10/11/2013
City/State	Mississippi			Gauge ID	909033
Location	Pellet Mill 2 Cooler			Pitot ID	4PEXT
<b>Averages</b>	<b>2.108</b>	<b>152.3</b>		Thermocouple ID	4PEXT
	<b>Delta P</b>	<b>Temp</b>			
<b>Point No.</b>	<b>In Water</b>	<b>Deg F</b>			
A-1	1.900	150		<b>Oxygen %</b>	<b>20.9</b>
2	2.300	151			
3	2.300	154		<b>Carbon Dioxide %</b>	<b>0</b>
4	2.200	152			
5	2.150	152		<b>Moisture %</b>	<b>4.54</b>
6	2.200	152			
7	2.000	152		<b>Stack Area sq.in.</b>	<b>346.360595</b>
8	2.100	146			
B-1	1.900	151		<b>Pbar</b>	<b>29.80</b>
2	2.000	154			
3	2.050	154		<b>Static Pressure</b>	<b>-1.2</b>
4	2.200	154			
5	2.100	154		<b>Pitot Coef.</b>	<b>0.84</b>
6	2.200	154			
7	2.050	154		<b>Start Time</b>	<b>1614</b>
8					
0				<b>Stop Time</b>	<b>1621</b>
0					
0				<b>Absolute Gas Pressure inches water</b>	<b>Ps = 29.71</b>
0					
0				<b>Dry Mole Fraction of Gas</b>	<b>Mfd = 0.95456</b>
0					
0				<b>Dry Molecular Weight of Gas lb/lb Mole</b>	<b>Md = 28.84</b>
0					
0				<b>Wet Molecular Weight of Gas lb/lb Mole</b>	<b>Ms = 28.34</b>
0					
0				<b>Average Gas Velocity ft/sec</b>	<b>vs = 88.91</b>
0					
0				<b>Dry Volumetric Gas Flow Rate at Standard Conditions SCFM</b>	<b>Qsd = 10488</b>
0					
0				<b>Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM</b>	<b>Qaw = 12831</b>
0					
0				<b>Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH</b>	<b>WSCFH = 659261</b>
0					
0				LKCH	
0				Pre	3-4 good
0				Post	5-3 good
#REF!					
#REF!					

**Air Control Techniques, P.C.**  
**Moisture Sampling Train Field Data Sheet**

Date 10/10/13  
~~8/14/13~~

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	ENVVA	Umbilical ID	200
City, State	Wiggins, MS	Meterbox ID	909033
Test Location	Green Hammer Mill	$\Delta H @$	1.917
Personnel	TJB JBG	Gamma ( $\gamma$ )	0.9828

Run Identification				Actual					Req'd	Vac
M41				Pre Leak Check	0.000	< 0.02 or 4%	10			
				Post Leak Check	0.000	< 0.02 or 4%	10			
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	$\Delta H$ (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)		
9:17	0	470.600	65	1.0	N/A	N/A	55	5		
9:32	15	477.71	66	1.0			55	5		
9:47	30	487.5	66	1.0			56	5		
10:02	45	496.2	67	1.0			60	6		
10:17	60	504.468								

Run Identification				Actual					Req'd	Vac
2				Pre Leak Check	0.000	< 0.02 or 4%	10			
				Post Leak Check	0.000	< 0.02 or 4%	9			
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	$\Delta H$ (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)		
10:36	0	504.700	68	1.0	N/A	N/A	60	5		
10:51	15	513.10	70				55	5		
11:06	30	521.9	72				55	5		
11:21	45	530.0	73				57	5		
11:36	60	538.681								

Run Identification				Actual					Req'd	Vac
3				Pre Leak Check	0.000	< 0.02 or 4%	11			
				Post Leak Check	0.000	< 0.02 or 4%	9			
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	$\Delta H$ (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)		
11:50	0	538.900	74	1.0	N/A	N/A	59	5		
12:05	15	549.0	75				50	5		
12:20	30	557.8	76				51	5		
12:35	45	563.4	77				53	5		
12:50	60	572.056								

# Method 4 - Air Control Techniques, P.C.

Date 10/10/13

Identification Information			
Client	<u>ENLIVA</u>	Job	<u>1911</u>
Plant Name	<u>Wiggins</u>	Process	<del>Green</del> <u>Green Hammer Mill</u>
City	<u>Wiggins</u>	State	<u>MS</u>

Sampling Information			
Run Number		Balance Number	<u>600</u>
Sampling Date		Balance Type	<u>ELECTRONIC</u>
Recovery Date		Balance Level	<u>EVI-1000</u>
Personnel	<u>TTS JBG</u>	Recovery Area	<input checked="" type="checkbox"/>

Location Moisture Data			
Run Number	<u>M4-1</u>	<u>M4-2</u>	<u>M4-3</u>
<u>Impinger 1</u>			
Final Weight, grams/mls	<u>809.3</u>	<u>743.0</u>	<u>822.7</u>
Initial Weight, grams/mls	<u>735.6</u>	<u>724.5</u>	<u>809.3</u>
Condensed Water, grams	<del>509.3</del> <u>73.7</u>	<u>18.5</u>	<u>13.4</u>
<u>Impinger 2</u>			
Final Weight, grams/mls	<u>661.1</u>	<u>729.5</u>	<u>661.5</u>
Initial Weight, grams/mls	<u>719.0</u>	<u>728.8</u>	<u>661.1</u>
Condensed Water, grams	<u>-57.9</u>	<u>0.7</u>	<u>0.4</u>
<u>Impinger 3</u>			
Final Weight, grams/mls	<u>595.9</u>	<u>597.0</u>	<u>596.1</u>
Initial Weight, grams/mls	<u>594.4</u>	<u>595.6</u>	<u>595.9</u>
Condensed Water, grams	<u>1.5</u>	<u>1.4</u>	<u>0.2</u>
Condensed Water, grams	<u>17.3</u>	<u>20.6</u>	
<u>Silica Gel</u>			
Final Weight, grams	<u>815.3</u>	<u>797.7</u>	<u>817.9</u>
Initial Weight, grams	<u>807.5</u>	<u>791.1</u>	<u>815.3</u>
Adsorbed Water, grams	<u>7.8</u>	<u>5.9</u>	<u>2.6</u>
Adsorbed Water, grams	<u>          </u>	<u>          </u>	<u>          </u>
Total Water, grams	<u>25.1</u>	<u>26.5</u>	<u>16.6</u>

$Vm(std) = \text{Volume of gas sampled at standard conditions (dscf)}$   
 $Vm(std) = ((\text{Gamma} * 17.64 * Vm * (Pbar + (\Delta H / 13.6))) / (Tm + 460))$   
 $Vwc(std) = \text{volume of water vapor at standard conditions (scf)}$   
 $Vwc(std) = (0.04707) * (\text{volume of water collected (mls)})$   
 $Bws = \text{Mole fraction of water vapor}$   
 $Bws = Vwc(std) / (Vm(std) + Vwc(std))$   
 $\text{Percent Moisture} = 100 * Bws$

**Air Control Techniques, P.C.**  
**Moisture Sampling Train Field Data Sheet**

Date ~~8/19/13~~  
 10/10/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	ENVIVA	Umbilical ID	200
City, State	Wiggins, MS	Meterbox ID	909033
Test Location	DRYER #1	$\Delta H @$	1.917
Personnel	TJB, JBS	Gamma ( $\gamma$ )	0.9828

Run Identification				Actual			Req'd		Vac
M44				Pre Leak Check	0.000	< 0.02 or 4%	10		
				Post Leak Check	0.000	< 0.02 or 4%	9		
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	$\Delta H$ (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
1734	0	572.300	80	1.0	N/A	N/A	58	3	
1753	15	580.90	81	↓	↓	↓	54	3	
1808	30	581.10	82	↓	↓	↓	56	3	
1823	45	577.2	82	↓	↓	↓	57	3	
1838	60	605.501							

10/11/13

Run Identification				Actual			Req'd		Vac
5				Pre Leak Check	0.000	< 0.02 or 4%	10		
				Post Leak Check	0.000	< 0.02 or 4%	10		
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	$\Delta H$ (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
1000	0	605.700	70	1.0	N/A	N/A	59	3	
1015	15	614.00	74	↓	↓	↓	63	3	
1030	30	622.24	79	↓	↓	↓	66	3	
1045	45	630.61	83	↓	↓	↓	67	3	
1100	60	638.921							

10/11/13

Run Identification				Actual			Req'd		Vac
6				Pre Leak Check	0.000	< 0.02 or 4%	10		
				Post Leak Check	0.000	< 0.02 or 4%	10		
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	$\Delta H$ (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
1137	0	639.106	86	1.0	N/A	N/A	56	3	
1152	15	647.5	87	↓	↓	↓	58	3	
1207	30	655.17	87	↓	↓	↓	59	3	
1222	45	663.24	88	↓	↓	↓	61	3	
1237	60	671.6105							

# Method 4 - Air Control Techniques, P.C.

Date 10/10/2013

Identification Information				
Client	Enviya		Job	2911
Plant Name	Wiggins		Process	DRYER #1
City	Wiggins		State	MS

Sampling Information				
Run Number			Balance Number	N1000
Sampling Date			Balance Type	Electronic
Recovery Date			Balance Level	✓
Personnel	TJB JB6		Recovery Area	✓

Location Moisture Data				
	Run Number	4	5	6
<u>Impinger 1</u>				
Final Weight, grams/mls		858.1	943.8	826.7
Initial Weight, grams/mls		743.0	822.7	722.7
Condensed Water, grams		115.1	121.1	104.0
<u>Impinger 2</u>				
Final Weight, grams/mls		736.5	630.7	744.4
Initial Weight, grams/mls		729.5	601.5	736.5
Condensed Water, grams		7.0	-30.8	7.9
<u>Impinger 3</u>				
Final Weight, grams/mls		597.1	599.5	597.8
Initial Weight, grams/mls		597.0	596.1	597.1
Condensed Water, grams		0.1	3.4	0.7
Condensed Water, grams				
<u>Silica Gel</u>				
Final Weight, grams		805.0	824.0	809.9
Initial Weight, grams		797.7	817.9	805.0
Adsorbed Water, grams		7.3	6.1	4.9
Adsorbed Water, grams		129.5	99.8	—
		↓	↓	
Total Water, grams				117.5

$V_m(\text{std}) = \text{Volume of gas sampled at standard conditions (dscf)}$   
 $V_m(\text{std}) = ((\text{Gamma} * 17.64 * V_m * (\text{Pbar} + (\Delta H / 13.6)))) / (\text{Tm} + 460)$   
 $V_{wc}(\text{std}) = \text{volume of water vapor at standard conditions (scf)}$   
 $V_{wc}(\text{std}) = (0.04707) * (\text{volume of water collected (mls)})$   
 $B_{ws} = \text{Mole fraction of water vapor}$   
 $B_{ws} = V_{wc}(\text{std}) / (V_m(\text{std}) + V_{wc}(\text{std}))$   
 $\text{Percent Moisture} = 100 * B_{ws}$

**Air Control Techniques, P.C.**  
**Moisture Sampling Train Field Data Sheet**

Date 10/11/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	ENVIVA	Umbilical ID	200
City, State	Wiggins MS	Meterbox ID	909833
Test Location	Polpet Mill Coolers # 2	ΔH@	1.917
Personnel	TIP JBB	Gamma (γ)	0.9828

Run Identification <u>M4-7</u>				Actual			Req'd		Vac
Pre Leak Check				0.000	< 0.02 or 4%		10		
Post Leak Check				0.000	< 0.02 or 4%		8		
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
1343	0	672.000	85	1.0	N/A	N/A	57	3	
1358	15	680.60	86				61	3	
1413	30	689.23	89	↓	↓	↓	61	3	
1428	45	698.1	89	↓	↓	↓	60	3	
1443	60	706.310							

Run Identification <u>M4-8</u>				Actual			Req'd		Vac
Pre Leak Check				0.000	< 0.02 or 4%		10		
Post Leak Check				0.000	< 0.02 or 4%		4		
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
1508	0	706.600	89	1.0	N/A	N/A	58	3	
1523	15	715.19	89				59	3	
1538	30	723.95	89	↓	↓	↓	59	3	
1553	45	732.97	90	↓	↓	↓	61	3	
1608	60	741.023							

Run Identification <u>M4-9</u>				Actual			Req'd		Vac
Pre Leak Check				0.000	< 0.02 or 4%		12		
Post Leak Check				0.000	< 0.02 or 4%		9		
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
0	1629	741.300	85	1.0	N/A	N/A	57	3	
15	1644	749.90	84	↓	↓	↓	60	3	
30	1659	758.29	83	↓	↓	↓	59	3	
45	1714	766.65	83	↓	↓	↓	60	3	
60	1729	774.98							

# Method 4 - Air Control Techniques, P.C.

Date

Identification Information			
Client	ENVIVA	Job	1911
Plant Name	Wiggins, MS	Process	Pellet mill #2 <span style="float: right; font-size: small;">codes</span>
City	Wiggins, MS	State	MS

Sampling Information			
Run Number		Balance Number	1620
Sampling Date		Balance Type	Electronic
Recovery Date		Balance Level	✓
Personnel	TTB JBG	Recovery Area	✓

Location Moisture Data				
	Run Number	7	8	9
<u>Impinger 1</u>				
Final Weight, grams/mls		719.2	852.1	746.3
Initial Weight, grams/mls		695.2	826.7	719.2
Condensed Water, grams		24.0	25.4	27.1
<u>Impinger 2</u>				
Final Weight, grams/mls		715.4	747.4	717.5
Initial Weight, grams/mls		712.2	744.4	715.4
Condensed Water, grams		3.2	3.0	2.1
<u>Impinger 3</u>				
Final Weight, grams/mls		603.6	598.2	603.8
Initial Weight, grams/mls		599.5	597.8	603.6
Condensed Water, grams		4.1	0.4	0.2
Condensed Water, grams				
<u>Silica Gel</u>				
Final Weight, grams		827.9	814.6	830.9
Initial Weight, grams		824.0	809.9	827.9
Adsorbed Water, grams		3.9	4.7	3.0
Adsorbed Water, grams		—	—	—
Total Water, grams		35.2	33.5	32.4

$V_m(\text{std}) = \text{Volume of gas sampled at standard conditions (dscf)}$   
 $V_m(\text{std}) = ((\text{Gamma} * 17.64 * V_m * (\text{Pbar} + (\Delta H / 13.6))) / (\text{Tm} + 460))$   
 $V_{wc}(\text{std}) = \text{volume of water vapor at standard conditions (scf)}$   
 $V_{wc}(\text{std}) = (0.04707) * (\text{volume of water collected (mls)})$   
 $B_{ws} = \text{Mole fraction of water vapor}$   
 $B_{ws} = V_{wc}(\text{std}) / (V_m(\text{std}) + V_{wc}(\text{std}))$   
 $\text{Percent Moisture} = 100 * B_{ws}$

**Air Control Techniques, P.C.**  
**Moisture Sampling Train Field Data Sheet**

Date 10/11/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	<u>ENUTVA</u>	Umbilical ID	<u>200</u>
City, State	<u>WIGALINE, MS</u>	Meterbox ID	<u>909033</u>
Test Location	<u>DRY Hammer Mill #2</u>	ΔH@	<u>1917</u>
Personnel	<u>MS JBS</u>	Gamma (γ)	<u>0.9828</u>

Run Identification				Actual					Req'd	Vac
<u>M4-10</u>				Pre Leak Check	<u>0.000</u>	< 0.02 or 4%		<u>10</u>		
				Post Leak Check	<u>0.000</u>	< 0.02 or 4%		<u>10</u>		
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)		
<u>1811</u>	<u>0</u>	<u>775.300</u>	<u>80</u>	<u>1.0</u>	<u>N/A</u>	<u>N/A</u>	<u>55</u>	<u>3</u>		
<u>1826</u>	<u>15</u>	<u>784.200</u>	<u>80</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>54</u>	<u>3</u>		
<u>1841</u>	<u>30</u>	<del>786.71</del>	<u>80</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>54</u>	<u>3</u>		
<u>1846</u>	<u>45</u>	<u>800.71</u>	<u>81</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>55</u>	<u>3</u>		
<u>1861</u>	<u>60</u>	<u>808.71</u>		<u>↓</u>	<u>↓</u>	<u>↓</u>				
		<u>795.100</u>								

1856  
1911

Run Identification				Actual					Req'd	Vac
<u>M4-11</u>				Pre Leak Check	<u>0.000</u>	< 0.02 or 4%		<u>10</u>		
				Post Leak Check	<u>0.000</u>	< 0.02 or 4%		<u>10</u>		
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)		
<u>1935</u>	<u>0</u>	<u>809.400</u>	<u>79</u>	<u>1.0</u>	<u>N/A</u>	<u>N/A</u>	<u>57</u>	<u>3</u>		
<u>1950</u>	<u>15</u>	<u>817.9</u>	<u>78</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>55</u>	<u>3</u>		
<u>2005</u>	<u>30</u>	<u>826.5</u>	<u>79</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>56</u>	<u>3</u>		
<u>2020</u>	<u>45</u>	<u>835.3</u>	<u>79</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>56</u>	<u>3</u>		
<u>2035</u>	<u>60</u>	<u>843.09</u>		<u>↓</u>	<u>↓</u>	<u>↓</u>				

Run Identification				Actual					Req'd	Vac
<u>M4-12</u>				Pre Leak Check	<u>0.000</u>	< 0.02 or 4%		<u>12</u>		
				Post Leak Check	<u>0.000</u>	< 0.02 or 4%		<u>9</u>		
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)		
<u>2048</u>	<u>0</u>	<u>843.360</u>	<u>78</u>	<u>1.0</u>	<u>N/A</u>	<u>N/A</u>	<u>57</u>	<u>3</u>		
<u>2103</u>	<u>15</u>	<u>852.17</u>	<u>78</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>57</u>	<u>3</u>		
<u>2118</u>	<u>30</u>	<u>860.25</u>	<u>79</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>57</u>	<u>3</u>		
<u>2133</u>	<u>45</u>	<u>868.82</u>	<u>78</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>56</u>	<u>3</u>		
<u>2148</u>	<u>60</u>	<u>877.176</u>		<u>↓</u>	<u>↓</u>	<u>↓</u>				

32.4  
33.5

# Method 4 - Air Control Techniques, P.C.

Date

## Identification Information

	Client <u>ENVIVA</u>	Job <u>1911</u>	
	Plant Name <u>Wiggins</u>	Process <u>DRY Hammermill #2</u>	
	City <u>Wiggins</u>	State <u>MS</u>	

## Sampling Information

Run Number		Balance Number	<u>V1000</u>
Sampling Date		Balance Type	<u>Electronic</u>
Recovery Date		Balance Level	<input checked="" type="checkbox"/>
Personnel	<u>TJB JBG</u>	Recovery Area	<input checked="" type="checkbox"/>

## Location Moisture Data

	Run Number		
	<u>10</u>	<u>11</u>	<u>12</u>
<u>Impinger 1</u>			
Final Weight, grams/mls	<u>875.7</u>	<u>770.2</u>	<u>898.8</u>
Initial Weight, grams/mls	<u>852.1</u>	<u>746.3</u>	<u>875.7</u>
Condensed Water, grams	<u>23.6</u>	<u>23.9</u>	<u>23.1</u>
<u>Impinger 2</u>			
Final Weight, grams/mls	<u>749.9</u>	<u>720.5</u>	<u>752.8</u>
Initial Weight, grams/mls	<u>747.4</u>	<u>717.5</u>	<u>749.9</u>
Condensed Water, grams	<u>2.5</u>	<u>3.0</u>	<u>2.9</u>
<u>Impinger 3</u>			
Final Weight, grams/mls	<u>598.4</u>	<u>604.4</u>	<u>598.8</u>
Initial Weight, grams/mls	<u>598.2</u>	<u>603.8</u>	<u>598.4</u>
Condensed Water, grams	<u>0.2</u>	<u>0.6</u>	<u>0.4</u>
Condensed Water, grams			
<u>Silica Gel</u>			
Final Weight, grams	<u>818.5</u>	<u>833.4</u>	<u>822.3</u>
Initial Weight, grams	<u>814.6</u>	<u>830.9</u>	<u>818.5</u>
Adsorbed Water, grams	<u>3.9</u>	<u>2.5</u>	<u>3.8</u>
Adsorbed Water, grams	<u>—</u>	<u>—</u>	<u>—</u>
Total Water, grams	<u>30.2</u>	<u>30.0</u>	<u>30.2</u>

$Vm(std) = \text{Volume of gas sampled at standard conditions (dscf)}$   
 $Vm(std) = ((\text{Gamma} * 17.64 * Vm * (Pbar + (\Delta H / 13.6))) / (Tm + 460))$   
 $Vwc(std) = \text{volume of water vapor at standard conditions (scf)}$   
 $Vwc(std) = (0.04707) * (\text{volume of water collected (mls)})$   
 $Bws = \text{Mole fraction of water vapor}$   
 $Bws = Vwc(std) / (Vm(std) + Vwc(std))$   
 $\text{Percent Moisture} = 100 * Bws$

**Air Control Techniques, P.C.**  
**Moisture Sampling Train Field Data Sheet**

Date 10/14/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	ENVIVA	Umbilical ID	200
City, State	Wiggins MS	Meterbox ID	09033
Test Location	Pellet Mill #1 Cooler	$\Delta H @$	1.917
Personnel	TIA JBB	Gamma ( $\gamma$ )	0.9808

Run Identification				Actual			Req'd		Vac
M4-13				Pre Leak Check	0.000	< 0.02 or 4%	12		
				Post Leak Check	0.000	< 0.02 or 4%	8		
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	$\Delta H$ (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
8:58	0	877.400	67	1.0	N/A	N/A	52	3	
9:13	15	886.03	70	↓	↓	↓	55	3	
9:28	30	895.1	73	↓	↓	↓	56	3	
9:43	45	903.1	77	↓	↓	↓	58	3	
9:58	60	911.268							

Run Identification				Actual			Req'd		Vac
M4-14				Pre Leak Check	0.000	< 0.02 or 4%	10		
				Post Leak Check	0.000	< 0.02 or 4%	10		
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	$\Delta H$ (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
10:22	0	911.500	74	1.0	N/A	N/A	59	3	
10:37	15	920.39	82	↓	↓	↓	60	3	
10:52	30	929.10	86	↓	↓	↓	54	3	
11:07	45	938.32	88	↓	↓	↓	55	3	
11:22	60	947.345							

Run Identification				Actual			Req'd		Vac
M4-15				Pre Leak Check	0.000	< 0.02 or 4%	11		
				Post Leak Check	0.010	< 0.02 or 4%	9		
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	$\Delta H$ (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
11:41	0	947.600	89	1.0	N/A	N/A	56	3	
11:56	15	956.32	89	↓	↓	↓	60	3	
12:11	30	964.92	89	↓	↓	↓	60	3	
12:26	45	973.55	89	↓	↓	↓	61	3	
12:41	60	982.167							

# Method 4 - Air Control Techniques, P.C.

Date

Identification Information				
Client	Envira		Job	1911
Plant Name	Wiggins		Process	Relief Codes # 1
City	Wiggins		State	MS

Sampling Information					
Run Number	<input type="text"/>	<input type="text"/>	<input type="text"/>	Balance Number	<input type="text"/>
Sampling Date	<input type="text"/>	<input type="text"/>	<input type="text"/>	Balance Type	<input type="text"/>
Recovery Date	<input type="text"/>	<input type="text"/>	<input type="text"/>	Balance Level	<input type="text"/>
Personnel	TTB JBG			Recovery Area	<input type="text"/>

Location Moisture Data			
Run Number	13	14	15
<u>Impinger 1</u>			
Final Weight, grams/mls	748.2	787.3	765.0
Initial Weight, grams/mls	728.1	763.4	748.2
Condensed Water, grams	20.1	23.9	16.8
<u>Impinger 2</u>			
Final Weight, grams/mls	722.1	754.0	722.9
Initial Weight, grams/mls	720.5	752.8	722.1
Condensed Water, grams	1.6	1.2	0.8
<u>Impinger 3</u>			
Final Weight, grams/mls	604.4	598.6	604.9
Initial Weight, grams/mls	604.4	598.8	604.4
Condensed Water, grams	0.0	-0.2	0.5
Condensed Water, grams	<input type="text"/>	<input type="text"/>	<input type="text"/>
<u>Silica Gel</u>			
Final Weight, grams	830.0	825.2	837.9
Initial Weight, grams	833.4	822.3	836.0
Adsorbed Water, grams	2.6	2.9	1.9
Adsorbed Water, grams	<input type="text"/>	<input type="text"/>	<input type="text"/>
Total Water, grams	24.3	27.8	19.9

$Vm(std) = \text{Volume of gas sampled at standard conditions (dscf)}$   
 $Vm(std) = ((\text{Gamma} * 17.64 * Vm * (Pbar + (\Delta H / 13.6)))) / (Tm + 460)$   
 $Vwc(std) = \text{volume of water vapor at standard conditions (scf)}$   
 $Vwc(std) = (0.04707) * (\text{volume of water collected (mls)})$   
 $Bws = \text{Mole fraction of water vapor}$   
 $Bws = Vwc(std) / (Vm(std) + Vwc(std))$   
 $\text{Percent Moisture} = 100 * Bws$

Method 4 - Air Control Techniques, P.C.

Date

Identification Information			
Client	ENVIVA	Job	1911
Plant Name	Wiggins	Process	ASPIRATOR
City	Wiggins	State	MS

Sampling Information			
Run Number		Balance Number	
Sampling Date		Balance Type	
Recovery Date		Balance Level	
Personnel	TB JBG	Recovery Area	

Location Moisture Data				
	Run Number	16	17	18
<u>Impinger 1</u>				
Final Weight, grams/mls		914.9	958.8	946.7
Initial Weight, grams/mls		787.3	760.0	743.8
Condensed Water, grams		127.6	198.8	202.9
<u>Impinger 2</u>				
Final Weight, grams/mls		877.1	790.3	814.9
Initial Weight, grams/mls		754.0	722.9	746.0
Condensed Water, grams		123.1	67.4	68.9
<u>Impinger 3</u>				
Final Weight, grams/mls		599.7	605.0	600.3
Initial Weight, grams/mls		598.6	604.9	599.7
Condensed Water, grams		1.1	0.1	0.6
Condensed Water, grams				
<u>Silica Gel</u>				
Final Weight, grams		830.2	841.2	832.2
Initial Weight, grams		825.2	837.9	830.2
Adsorbed Water, grams		5.0	3.3	2.0
Adsorbed Water, grams		—	—	—
Total Water, grams		256.8	269.6	274.4

$Vm(std) = \text{Volume of gas sampled at standard conditions (dscf)}$   
 $Vm(std) = ((\text{Gamma} * 17.64 * Vm * (Pbar + (\Delta H / 13.6)))) / (Tm + 460)$   
 $Vwc(std) = \text{volume of water vapor at standard conditions (scf)}$   
 $Vwc(std) = (0.04707) * (\text{volume of water collected (mls)})$   
 $Bws = \text{Mole fraction of water vapor}$   
 $Bws = Vwc(std) / (Vm(std) + Vwc(std))$   
 $\text{Percent Moisture} = 100 * Bws$

24.7  
1016

**Air Control Techniques, P.C.**  
**Moisture Sampling Train Field Data Sheet**

Date 10/12/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	ENVIVA	Umbilical ID	30
City, State	Wiggins, MS	Meterbox ID	98033
Test Location	Relief Mill Aspirator	$\Delta H@$	1.917
Personnel	TIB JBG	Gamma ( $\gamma$ )	0.9808

Run Identification <u>M4-16</u>				Actual			Req'd		Vac
Pre Leak Check				0.000	< 0.02 or 4%		12		
Post Leak Check				0.000	< 0.02 or 4%		9		
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	$\Delta H$ (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
1509	0	982.400	83	1.0	N/A	N/A	54	3	
1524	15	989.81	85				60	3	
1539	30	998.62	86				62	3	
1554	45	1007.31	86				65	3	
1609	60	1015.64							

Run Identification <u>M4-17</u>				Actual			Req'd		Vac
Pre Leak Check				0.000	< 0.02 or 4%		10		
Post Leak Check				0.000	< 0.02 or 4%		11		
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	$\Delta H$ (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
1636	0	16.000	85	1.0	N/A	N/A	56	3	
1651	15	24.21	84				65	3	
1706	30	32.27	85				59	3	
1721	45	40.18	85				61	3	
1736	60	48.49							

Run Identification <u>M4-18</u>				Actual			Req'd		Vac
Pre Leak Check				0.000	< 0.02 or 4%		12		
Post Leak Check				0.000	< 0.02 or 4%		8		
Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	$\Delta H$ (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
1800	0	48.300	84	1.0	N/A	N/A	57	3	
1815	15	57.41	82				51	3	
1830	30	66.20	81				52	3	
1845	45	79.55	80				52	3	
1900	60	82.708							

**Air Control Techniques, P.C.**  
**Moisture Sampling Train Field Data Sheet**

Date 10/13/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	<u>AVIVA</u>	Umbilical ID	<u>200</u>
City, State	<u>Wiggins, MS</u>	Meterbox ID	<u>981033</u>
Test Location	<u>DRYER #2</u>	ΔH@	<u>1.917</u>
Personnel	<u>115 JBG</u>	Gamma (γ)	<u>0.9828</u>

Run Identification <u>M4-19</u>				Actual	Req'd	Vac
Pre Leak Check				<u>0.000</u>	< 0.02 or 4%	<u>15</u>
Post Leak Check				<u>0.000</u>	< 0.02 or 4%	<u>10</u>

Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
<u>921</u>	<u>0</u>	<u>82.900</u>	<u>72</u>	<u>1.0</u>	<u>N/A</u>	<u>N/A</u>	<u>56</u>	<u>3</u>
<u>936</u>	<u>15</u>	<u>90.93</u>	<u>76</u>	↓	↓	↓	<u>58</u>	<u>3</u>
<u>951</u>	<u>30</u>	<u>99.15</u>	<u>79</u>	↓	↓	↓	<u>59</u>	<u>3</u>
<u>1006</u>	<u>45</u>	<u>106.85</u>	<u>83</u>	↓	↓	↓	<u>60</u>	<u>3</u>
<u>1021</u>	<u>60</u>	<u>114.788</u>						

Run Identification <u>M4-20</u>				Actual	Req'd	Vac
Pre Leak Check				<u>0.000</u>	< 0.02 or 4%	<u>2</u>
Post Leak Check				<u>0.000</u>	< 0.02 or 4%	<u>2</u>

Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
<u>1104</u>	<u>0</u>	<u>115.000</u>	<u>88</u>	<u>1.0</u>	<u>N/A</u>	<u>N/A</u>	<u>57</u>	<u>3</u>
<u>1119</u>	<u>15</u>	<u>123.65</u>	<u>89</u>	↓	↓	↓	<u>61</u>	<u>3</u>
<u>1134</u>	<u>30</u>	<u>131.976</u>	<u>90</u>	↓	↓	↓	<u>61</u>	<u>3</u>
<u>1149</u>	<u>45</u>	<u>140.32</u>	<u>91</u>	↓	↓	↓	<u>62</u>	<u>3</u>
<u>1204</u>	<u>60</u>	<u>148.650</u>						

Run Identification <u>M4-21</u>				Actual	Req'd	Vac
Pre Leak Check				<u>0.000</u>	< 0.02 or 4%	<u>10</u>
Post Leak Check					< 0.02 or 4%	

Clock Time	Elapsed Time (min)	Volume Metered (ft <sup>3</sup> )	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
<u>1231</u>	<u>0</u>	<u>149.200</u>	<u>89</u>	<u>1.0</u>	<u>N/A</u>	<u>N/A</u>	<u>51</u>	<u>3</u>
<u>1301</u>	<u>15</u>	<u>157.72</u>	<u>90</u>	↓	↓	↓	<u>58</u>	<u>4</u>
<u>1316</u>	<u>30</u>	<u>166.39</u>	<u>91</u>	↓	↓	↓	<u>60</u>	<u>7</u>
<u>1341</u>	<u>45</u>	<u>172.82</u>	<u>91</u>	↓	↓	↓	<u>59</u>	<u>10</u>
<u>1346</u>	<u>60</u>	<u>179.996</u>						

1346

off 1238 upset condition  
 ON 1252

Method 4 - Air Control Techniques, P.C.

Date 10/13/13

Identification Information				
Client	ENVIVA		Job	1911
Plant Name	Wiggins		Process	DRYER #2
City	Wiggins		State	MS

Sampling Information				
Run Number			Balance Number	V1200
Sampling Date			Balance Type	Electronic
Recovery Date			Balance Level	✓
Personnel			Recovery Area	✓

Location Moisture Data				
	Run Number	19	20	21
<u>Impinger 1</u>				
Final Weight, grams/mls		970.0	908.2	922.2
Initial Weight, grams/mls		749.2	748.2	681.2
Condensed Water, grams		220.8	160	241.0
<u>Impinger 2</u>				
Final Weight, grams/mls		829.0	800.3	687.8
Initial Weight, grams/mls		790.3	680.0	674.0
Condensed Water, grams		38.7	120.3	13.8
<u>Impinger 3</u>				
Final Weight, grams/mls		609.3	<del>603.1</del>	612.5
Initial Weight, grams/mls		605.0	600.4	609.3
Condensed Water, grams		4.3	2.7	3.2
Condensed Water, grams				
<u>Silica Gel</u>				
Final Weight, grams		845.1	835.7	847.1
Initial Weight, grams		841.2	832.2	845.1
Adsorbed Water, grams		3.9	3.5	2.0
Adsorbed Water, grams				
Total Water, grams		267.7	286.5	260.0

$Vm(std) = \text{Volume of gas sampled at standard conditions (dscf)}$   
 $Vm(std) = ((\text{Gamma} * 17.64 * Vm * (Pbar + (\Delta H / 13.6))) / (Tm + 460))$   
 $Vwc(std) = \text{volume of water vapor at standard conditions (scf)}$   
 $Vwc(std) = (0.04707) * (\text{volume of water collected (mls)})$   
 $Bws = \text{Mole fraction of water vapor}$   
 $Bws = Vwc(std) / (Vm(std) + Vwc(std))$   
 $\text{Percent Moisture} = 100 * Bws$

## **APPENDIX B**

### **Method 25A Data**

Test Run 1 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins  
THC  
ppm

Start Averaging

10/10/2013	10:17:27	29.2
10/10/2013	10:18:26	29.1
10/10/2013	10:19:26	29.4
10/10/2013	10:20:26	28.5
10/10/2013	10:21:26	29.2
10/10/2013	10:22:27	29.8
10/10/2013	10:23:27	30.5
10/10/2013	10:24:27	31.5
10/10/2013	10:25:27	30.8
10/10/2013	10:26:26	29.3
10/10/2013	10:27:26	29.3
10/10/2013	10:28:26	28.9
10/10/2013	10:29:27	29.5
10/10/2013	10:30:27	31.4
10/10/2013	10:31:27	31.1
10/10/2013	10:32:26	31.3
10/10/2013	10:33:26	31.2
10/10/2013	10:34:26	30.4
10/10/2013	10:35:27	30.4
10/10/2013	10:36:27	30.1
10/10/2013	10:37:27	29.7
10/10/2013	10:38:27	30.2
10/10/2013	10:39:26	29.2
10/10/2013	10:40:26	30.1
10/10/2013	10:41:26	30.3
10/10/2013	10:42:26	29.1
10/10/2013	10:43:27	29.5
10/10/2013	10:44:27	30.6
10/10/2013	10:45:27	29.7
10/10/2013	10:46:25	31
10/10/2013	10:47:26	30.1
10/10/2013	10:48:26	30.7
10/10/2013	10:49:26	31.6
10/10/2013	10:50:27	31.6
10/10/2013	10:51:27	32.3
10/10/2013	10:52:27	31.4
10/10/2013	10:53:27	30.4
10/10/2013	10:54:26	31.9
10/10/2013	10:55:26	31.8
10/10/2013	10:56:26	33.1
10/10/2013	10:57:26	32.8
10/10/2013	10:58:27	31.8
10/10/2013	10:59:27	32.5
10/10/2013	11:00:27	32.8
10/10/2013	11:01:26	30.2

10/10/2013	11:02:26	31.2
10/10/2013	11:03:26	30.7
10/10/2013	11:04:26	31.2
10/10/2013	11:05:27	32.7
10/10/2013	11:06:27	31.6
10/10/2013	11:07:27	31.2
10/10/2013	11:08:25	32.5
10/10/2013	11:09:26	31
10/10/2013	11:10:26	30.8
10/10/2013	11:11:26	28.9
10/10/2013	11:12:26	30.9
10/10/2013	11:13:27	31.9
10/10/2013	11:14:27	32.1
10/10/2013	11:15:27	32.6
10/10/2013	11:16:26	34
Average	1807 sampl	30.8
Test Run 1 End		

Test Run 2 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/10/2013	10:37:12	33.22
10/10/2013	10:38:13	32.73
10/10/2013	10:39:13	33.22
10/10/2013	10:40:13	33.21
10/10/2013	10:41:13	31.78
10/10/2013	10:42:14	29.83
10/10/2013	10:43:14	31.37
10/10/2013	10:44:12	31.5
10/10/2013	10:45:13	33.24
10/10/2013	10:46:13	32.96
10/10/2013	10:47:13	32.52
10/10/2013	10:48:13	32.17
10/10/2013	10:49:14	31.8
10/10/2013	10:50:14	30.68
10/10/2013	10:51:12	29.76
10/10/2013	10:52:12	31.03
10/10/2013	10:53:13	31.9
10/10/2013	10:54:13	32.57
10/10/2013	10:55:13	32.4
10/10/2013	10:56:14	32.68
10/10/2013	10:57:14	33.18
10/10/2013	10:58:12	33.26
10/10/2013	10:59:12	32.76
10/10/2013	11:00:13	31.1
10/10/2013	11:01:12	30.85
10/10/2013	11:02:14	30.84
10/10/2013	11:03:13	30.27
10/10/2013	11:04:12	30.6
10/10/2013	11:05:14	32.18
10/10/2013	11:06:13	30.96
10/10/2013	11:07:12	31.41
10/10/2013	11:08:12	30.82
10/10/2013	11:09:13	31.24
10/10/2013	11:10:13	31.94
10/10/2013	11:11:14	31.25
10/10/2013	11:12:13	30.81
10/10/2013	11:13:12	32.84
10/10/2013	11:14:12	32.11
10/10/2013	11:15:14	32.71
10/10/2013	11:16:13	32.57
10/10/2013	11:17:12	33.7
10/10/2013	11:18:14	33.87
10/10/2013	11:19:13	32.8
10/10/2013	11:20:13	31.93
10/10/2013	11:21:14	33.89

10/10/2013	11:22:13	33.12
10/10/2013	11:23:13	32.56
10/10/2013	11:24:14	32.31
10/10/2013	11:25:13	33.49
10/10/2013	11:26:12	34.83
10/10/2013	11:27:14	34.8
10/10/2013	11:28:13	33.96
10/10/2013	11:29:13	33.5
10/10/2013	11:30:14	34.21
10/10/2013	11:31:13	32.7
10/10/2013	11:32:13	31.67
10/10/2013	11:33:12	31.32
10/10/2013	11:34:13	31.95
10/10/2013	11:35:13	31.59
10/10/2013	11:36:14	31.24
10/10/2013	11:37:13	32.88

Test Run 3 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/10/2013	11:51:37	27.47
10/10/2013	11:52:37	25.81
10/10/2013	11:53:37	25.62
10/10/2013	11:54:38	26.13
10/10/2013	11:55:36	27.21
10/10/2013	11:56:36	27.54
10/10/2013	11:57:36	27.06
10/10/2013	11:58:37	27.89
10/10/2013	11:59:37	27.66
10/10/2013	12:00:37	26.76
10/10/2013	12:01:38	26.92
10/10/2013	12:02:38	26.42
10/10/2013	12:03:36	25.01
10/10/2013	12:04:36	25.47
10/10/2013	12:05:37	25.98
10/10/2013	12:06:37	26.95
10/10/2013	12:07:37	27.79
10/10/2013	12:08:37	26.71
10/10/2013	12:09:38	27.38
10/10/2013	12:10:38	27.84
10/10/2013	12:11:36	25.99
10/10/2013	12:12:36	25.7
10/10/2013	12:13:37	24.64
10/10/2013	12:14:37	25.2
10/10/2013	12:15:37	25.22
10/10/2013	12:16:37	24.65
10/10/2013	12:17:38	24.05
10/10/2013	12:18:36	23.8
10/10/2013	12:19:36	22.94
10/10/2013	12:20:36	23.17
10/10/2013	12:21:37	24.1
10/10/2013	12:22:37	25.63
10/10/2013	12:23:37	26.37
10/10/2013	12:24:37	26.85
10/10/2013	12:25:38	26.02
10/10/2013	12:26:36	25.65
10/10/2013	12:27:36	25.72
10/10/2013	12:28:37	27.03
10/10/2013	12:29:37	26.23
10/10/2013	12:30:37	25.87
10/10/2013	12:31:37	25.97
10/10/2013	12:32:38	25.53
10/10/2013	12:33:38	25.25
10/10/2013	12:34:36	26.76
10/10/2013	12:35:36	27.16

10/10/2013	12:36:37	27.29
10/10/2013	12:37:37	27.02
10/10/2013	12:38:37	27.31
10/10/2013	12:39:37	28.11
10/10/2013	12:40:38	28.86
10/10/2013	12:41:36	28.19
10/10/2013	12:42:36	27.22
10/10/2013	12:43:37	27.74
10/10/2013	12:44:37	28.08
10/10/2013	12:45:37	26.91
10/10/2013	12:46:38	26.97
10/10/2013	12:47:38	27.99
10/10/2013	12:48:36	27.63
10/10/2013	12:49:36	26.3
10/10/2013	12:50:37	25.95
Average	1802 sampl	26.38

Test Run 3 End

Test Run 4 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/10/2013	17:39:30	73.6
10/10/2013	17:40:31	73.7
10/10/2013	17:41:31	74.2
10/10/2013	17:42:31	74.3
10/10/2013	17:43:31	74.4
10/10/2013	17:44:32	74.6
10/10/2013	17:45:32	75.3
10/10/2013	17:46:32	75.7
10/10/2013	17:47:30	75.7
10/10/2013	17:48:31	75.6
10/10/2013	17:49:31	75
10/10/2013	17:50:31	74.2
10/10/2013	17:51:31	72.5
10/10/2013	17:52:32	71.5
10/10/2013	17:53:32	70.7
10/10/2013	17:54:30	70
10/10/2013	17:55:30	69.3
10/10/2013	17:56:31	68.6
10/10/2013	17:57:31	68
10/10/2013	17:58:31	67.7
10/10/2013	17:59:32	67.1
10/10/2013	18:00:32	66.8
10/10/2013	18:01:30	66.4
10/10/2013	18:02:30	66
10/10/2013	18:03:31	65
10/10/2013	18:04:31	64.5
10/10/2013	18:05:31	64.3
10/10/2013	18:06:31	64.1
10/10/2013	18:07:32	64.8
10/10/2013	18:08:32	65.5
10/10/2013	18:09:30	65.6
10/10/2013	18:10:31	65.7
10/10/2013	18:11:31	65.8
10/10/2013	18:12:31	65.8
10/10/2013	18:13:31	66.6
10/10/2013	18:14:32	66.7
10/10/2013	18:15:32	67
10/10/2013	18:16:30	67
10/10/2013	18:17:30	66.2
10/10/2013	18:18:31	65.5
10/10/2013	18:19:31	65
10/10/2013	18:20:31	64.5
10/10/2013	18:21:32	63.4
10/10/2013	18:22:32	62.8
10/10/2013	18:23:30	62.2

10/10/2013	18:24:30	62
10/10/2013	18:25:31	62.2
10/10/2013	18:26:31	62.2
10/10/2013	18:27:31	62.6
10/10/2013	18:28:31	62.4
10/10/2013	18:29:32	61.7
10/10/2013	18:30:32	61.8
10/10/2013	18:31:30	61.4
10/10/2013	18:32:30	61.5
10/10/2013	18:33:31	61.3
10/10/2013	18:34:31	61.3
10/10/2013	18:35:31	61.1
10/10/2013	18:36:31	61.3
10/10/2013	18:37:32	60.8
10/10/2013	18:38:30	60.2
10/10/2013	18:39:30	60.4
Average	1837 samç	66.7
Test Run 4 End		

Test Run 5 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC  
ppm

Start Averaging

10/11/2013	10:00:39	59.48
10/11/2013	10:01:40	59.35
10/11/2013	10:02:40	59.64
10/11/2013	10:03:40	59.19
10/11/2013	10:04:40	59.7
10/11/2013	10:05:41	60.45
10/11/2013	10:06:41	60.54
10/11/2013	10:07:41	60.86
10/11/2013	10:08:40	61.28
10/11/2013	10:09:40	62.22
10/11/2013	10:10:40	62.62
10/11/2013	10:11:40	62.46
10/11/2013	10:12:40	62.22
10/11/2013	10:13:41	61.96
10/11/2013	10:14:41	61.71
10/11/2013	10:15:39	61.79
10/11/2013	10:16:40	61.65
10/11/2013	10:17:40	61.76
10/11/2013	10:18:40	61.82
10/11/2013	10:19:40	61.41
10/11/2013	10:20:41	60.91
10/11/2013	10:21:41	60.34
10/11/2013	10:22:41	60.35
10/11/2013	10:23:39	60.17
10/11/2013	10:24:40	60.48
10/11/2013	10:25:40	60.31
10/11/2013	10:26:40	60.03
10/11/2013	10:27:40	60.26
10/11/2013	10:28:41	60.17
10/11/2013	10:29:41	59.83
10/11/2013	10:30:41	59.58
10/11/2013	10:31:40	60.56
10/11/2013	10:32:40	60.96
10/11/2013	10:33:40	60.79
10/11/2013	10:34:40	61.26
10/11/2013	10:35:41	61.22
10/11/2013	10:36:41	61.09
10/11/2013	10:37:41	61.12
10/11/2013	10:38:39	61.86
10/11/2013	10:39:40	62.32
10/11/2013	10:40:40	62.49
10/11/2013	10:41:40	62.15
10/11/2013	10:42:41	62.22
10/11/2013	10:43:41	62.04
10/11/2013	10:44:41	61.73

10/11/2013	10:45:41	60.99
10/11/2013	10:46:40	61.3
10/11/2013	10:47:40	61.17
10/11/2013	10:48:40	62.35
10/11/2013	10:49:40	63.58
10/11/2013	10:50:41	63.57
10/11/2013	10:51:41	65.12
10/11/2013	10:52:41	67.32
10/11/2013	10:53:39	67.58
10/11/2013	10:54:40	67.4
10/11/2013	10:55:40	66.77
10/11/2013	10:56:40	66
10/11/2013	10:57:40	65.74
10/11/2013	10:58:41	64.85
10/11/2013	10:59:41	64.09
Average	1810 sampl	61.92
Test Run 5 End		

Test Run 6 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	11:37:39	62.85
10/11/2013	11:38:39	63.21
10/11/2013	11:39:40	63.49
10/11/2013	11:40:38	63.72
10/11/2013	11:41:38	64.5
10/11/2013	11:42:38	65.32
10/11/2013	11:43:39	66.16
10/11/2013	11:44:39	66.6
10/11/2013	11:45:39	66.81
10/11/2013	11:46:40	66.6
10/11/2013	11:47:38	64.85
10/11/2013	11:48:38	62.59
10/11/2013	11:49:38	60.21
10/11/2013	11:50:38	58.27
10/11/2013	11:51:39	56.95
10/11/2013	11:52:39	55.02
10/11/2013	11:53:39	53.86
10/11/2013	11:54:39	52.91
10/11/2013	11:55:40	52.4
10/11/2013	11:56:38	52.38
10/11/2013	11:57:38	52.86
10/11/2013	11:58:39	53.87
10/11/2013	11:59:39	54.56
10/11/2013	12:00:39	53.55
10/11/2013	12:01:39	52.72
10/11/2013	12:02:39	52.05
10/11/2013	12:03:40	51.53
10/11/2013	12:04:38	51.4
10/11/2013	12:05:38	52.07
10/11/2013	12:06:38	52.86
10/11/2013	12:07:39	53.12
10/11/2013	12:08:39	53.31
10/11/2013	12:09:39	52.77
10/11/2013	12:10:40	51.76
10/11/2013	12:11:40	51.02
10/11/2013	12:12:38	51.05
10/11/2013	12:13:38	52.13
10/11/2013	12:14:39	52.93
10/11/2013	12:15:39	53.34
10/11/2013	12:16:39	53.7
10/11/2013	12:17:39	53.91
10/11/2013	12:18:40	54.85
10/11/2013	12:19:38	55.39
10/11/2013	12:20:38	55.82
10/11/2013	12:21:38	55.66

10/11/2013	12:22:39	55.8
10/11/2013	12:23:39	56.58
10/11/2013	12:24:39	57.45
10/11/2013	12:25:40	58.57
10/11/2013	12:26:40	59.56
10/11/2013	12:27:38	60.26
10/11/2013	12:28:38	60.52
10/11/2013	12:29:39	60.23
10/11/2013	12:30:39	59.97
10/11/2013	12:31:39	59.98
10/11/2013	12:32:39	58.38
10/11/2013	12:33:40	57.52
10/11/2013	12:34:38	58.26
10/11/2013	12:35:38	59.53
10/11/2013	12:36:38	60.41
Average	1796 sampl	57.17
Test Run 6 End		

Test Run 7 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	13:43:41	29.28
10/11/2013	13:44:42	27.18
10/11/2013	13:45:42	25.85
10/11/2013	13:46:40	24.55
10/11/2013	13:47:40	23.31
10/11/2013	13:48:41	22.64
10/11/2013	13:49:41	22.37
10/11/2013	13:50:41	22.49
10/11/2013	13:51:42	22.37
10/11/2013	13:52:42	22.04
10/11/2013	13:53:40	22.25
10/11/2013	13:54:40	22.98
10/11/2013	13:55:41	22.9
10/11/2013	13:56:41	22.72
10/11/2013	13:57:41	23.05
10/11/2013	13:58:42	23.38
10/11/2013	13:59:42	23.44
10/11/2013	14:00:40	24.2
10/11/2013	14:01:40	24.19
10/11/2013	14:02:41	23.32
10/11/2013	14:03:41	22.78
10/11/2013	14:04:41	22.4
10/11/2013	14:05:41	22.24
10/11/2013	14:06:42	22.53
10/11/2013	14:07:40	22.54
10/11/2013	14:08:40	22
10/11/2013	14:09:40	21.36
10/11/2013	14:10:41	20.81
10/11/2013	14:11:41	20.6
10/11/2013	14:12:41	20.52
10/11/2013	14:13:41	20.67
10/11/2013	14:14:42	21.18
10/11/2013	14:15:40	22.48
10/11/2013	14:16:40	23.46
10/11/2013	14:17:41	23.6
10/11/2013	14:18:41	24.02
10/11/2013	14:19:41	24.31
10/11/2013	14:20:41	24.25
10/11/2013	14:21:42	24.44
10/11/2013	14:22:42	24.59
10/11/2013	14:23:40	24.59
10/11/2013	14:24:40	25.03
10/11/2013	14:25:40	25.21
10/11/2013	14:26:41	25.16
10/11/2013	14:27:41	25.61

10/11/2013	14:28:41	25.91
10/11/2013	14:29:42	24.74
10/11/2013	14:30:42	24.82
10/11/2013	14:31:40	24.18
10/11/2013	14:32:40	23.94
10/11/2013	14:33:41	24.63
10/11/2013	14:34:41	25.19
10/11/2013	14:35:41	25.92
10/11/2013	14:36:41	26.43
10/11/2013	14:37:42	25.26
10/11/2013	14:38:42	24.93
10/11/2013	14:39:40	25.61
10/11/2013	14:40:40	25.25
10/11/2013	14:41:41	24.92
10/11/2013	14:42:41	24.81
Average	1795 sampl	23.8
Test Run 7 End		

Test Run 8 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	15:08:58	20.89
10/11/2013	15:09:58	21.18
10/11/2013	15:10:56	21.36
10/11/2013	15:11:57	21.39
10/11/2013	15:12:57	21.49
10/11/2013	15:13:57	21.51
10/11/2013	15:14:58	21.66
10/11/2013	15:15:58	21.02
10/11/2013	15:16:58	20.12
10/11/2013	15:17:56	19.71
10/11/2013	15:18:57	19.67
10/11/2013	15:19:57	19.07
10/11/2013	15:20:57	19.24
10/11/2013	15:21:57	19.85
10/11/2013	15:22:58	20.21
10/11/2013	15:23:58	20.9
10/11/2013	15:24:56	21.72
10/11/2013	15:25:57	22.45
10/11/2013	15:26:57	23.3
10/11/2013	15:27:57	23.07
10/11/2013	15:28:57	22.47
10/11/2013	15:29:58	22.24
10/11/2013	15:30:58	22.14
10/11/2013	15:31:58	21.87
10/11/2013	15:32:56	22.09
10/11/2013	15:33:57	22.17
10/11/2013	15:34:57	22.55
10/11/2013	15:35:57	22.32
10/11/2013	15:36:57	21.72
10/11/2013	15:37:58	21.14
10/11/2013	15:38:58	21.1
10/11/2013	15:39:58	21.29
10/11/2013	15:40:56	21.44
10/11/2013	15:41:57	21.58
10/11/2013	15:42:57	22.64
10/11/2013	15:43:57	22.48
10/11/2013	15:44:57	22.65
10/11/2013	15:45:58	22.37
10/11/2013	15:46:58	22.73
10/11/2013	15:47:56	22.8
10/11/2013	15:48:57	22.34
10/11/2013	15:49:57	21.76
10/11/2013	15:50:57	21.83
10/11/2013	15:51:57	22.04
10/11/2013	15:52:58	22.15

10/11/2013	15:53:58	22.07
10/11/2013	15:54:58	22.66
10/11/2013	15:55:58	22.99
10/11/2013	15:56:57	22.84
10/11/2013	15:57:57	22.83
10/11/2013	15:58:57	22.2
10/11/2013	15:59:58	21.03
10/11/2013	16:00:58	19.77
10/11/2013	16:01:58	18.88
10/11/2013	16:02:56	18.32
10/11/2013	16:03:57	17.86
10/11/2013	16:04:57	18.62
10/11/2013	16:05:57	18.41
10/11/2013	16:06:57	18.6
10/11/2013	16:07:58	19.1
Average	1796 sampl	21.29
Test Run 8 End		

Test Run 9 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	16:29:59	22.84
10/11/2013	16:30:59	21.54
10/11/2013	16:31:59	21.11
10/11/2013	16:33:00	21.4
10/11/2013	16:34:00	21.21
10/11/2013	16:35:00	21.39
10/11/2013	16:36:00	21.79
10/11/2013	16:36:59	23.24
10/11/2013	16:37:59	23.79
10/11/2013	16:38:59	24.8
10/11/2013	16:39:59	25.11
10/11/2013	16:41:00	26.01
10/11/2013	16:42:00	28.05
10/11/2013	16:43:00	29.59
10/11/2013	16:44:00	29.65
10/11/2013	16:44:59	29.74
10/11/2013	16:45:59	29.86
10/11/2013	16:46:59	33.48
10/11/2013	16:48:00	32.59
10/11/2013	16:49:00	28.94
10/11/2013	16:49:59	26.37
10/11/2013	16:50:59	25.7
10/11/2013	16:51:59	24.69
10/11/2013	16:53:00	24.55
10/11/2013	16:54:00	24.78
10/11/2013	16:55:00	25.37
10/11/2013	16:55:59	26.6
10/11/2013	16:56:59	27.42
10/11/2013	16:57:59	26.35
10/11/2013	16:58:59	25.6
10/11/2013	17:00:00	25.52
10/11/2013	17:01:00	25.32
10/11/2013	17:02:00	24.67
10/11/2013	17:03:00	24.39
10/11/2013	17:04:01	24.2
10/11/2013	17:04:59	23.43
10/11/2013	17:05:59	22.29
10/11/2013	17:06:59	21.55
10/11/2013	17:08:00	21.18
10/11/2013	17:09:00	21.33
10/11/2013	17:10:00	21.67
10/11/2013	17:10:59	21.91
10/11/2013	17:11:59	22.59
10/11/2013	17:12:59	22.87
10/11/2013	17:14:00	23.27

10/11/2013	17:15:00	23.85
10/11/2013	17:16:00	23.83
10/11/2013	17:17:00	23.05
10/11/2013	17:17:59	23.11
10/11/2013	17:18:59	23.12
10/11/2013	17:19:59	24.45
10/11/2013	17:21:00	24.59
10/11/2013	17:22:00	24.41
10/11/2013	17:23:00	24.36
10/11/2013	17:24:00	25.25
10/11/2013	17:24:59	25.58
10/11/2013	17:25:59	26.03
10/11/2013	17:26:59	26.29
10/11/2013	17:27:59	26.55
10/11/2013	17:29:00	26.07
10/11/2013	17:30:00	25.36
10/11/2013	17:31:00	24.68
10/11/2013	17:32:00	24.5
10/11/2013	17:32:59	24.26
10/11/2013	17:33:59	24.15
Average	1951 sampl	24.82

Test Run 9 End

Test Run 10 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	18:11:17	29.88
10/11/2013	18:12:18	33.18
10/11/2013	18:13:18	31
10/11/2013	18:14:18	22.29
10/11/2013	18:15:18	19.06
10/11/2013	18:16:19	19
10/11/2013	18:17:19	21.06
10/11/2013	18:18:19	23.21
10/11/2013	18:19:17	22.71
10/11/2013	18:20:18	23.92
10/11/2013	18:21:18	23.38
10/11/2013	18:22:18	22.46
10/11/2013	18:23:19	23.73
10/11/2013	18:24:19	27.16
10/11/2013	18:25:19	28.89
10/11/2013	18:26:17	27.17
10/11/2013	18:27:18	22.65
10/11/2013	18:28:18	22.36
10/11/2013	18:29:18	23.07
10/11/2013	18:30:18	23.39
10/11/2013	18:31:19	21.74
10/11/2013	18:32:19	21
10/11/2013	18:33:19	21.29
10/11/2013	18:34:17	20.98
10/11/2013	18:35:18	18.39
10/11/2013	18:36:18	18.16
10/11/2013	18:37:18	18.91
10/11/2013	18:38:19	19.32
10/11/2013	18:39:19	21.57
10/11/2013	18:40:19	25.3
10/11/2013	18:41:17	31.9
10/11/2013	18:42:18	38.29
10/11/2013	18:43:18	33.17
10/11/2013	18:44:18	31.99
10/11/2013	18:45:19	25.13
10/11/2013	18:46:19	21.93
10/11/2013	18:47:19	19.45
10/11/2013	18:48:19	19.52
10/11/2013	18:49:18	18.88
10/11/2013	18:50:18	20.12
10/11/2013	18:51:18	20.89
10/11/2013	18:52:18	21.09
10/11/2013	18:53:19	21.01
10/11/2013	18:54:19	19.4
10/11/2013	18:55:17	19.85

10/11/2013	18:56:18	24.65
10/11/2013	18:57:18	24.98
10/11/2013	18:58:18	22.99
10/11/2013	18:59:18	23.31
10/11/2013	19:00:19	25.22
10/11/2013	19:01:19	25.84
10/11/2013	19:02:19	27.93
10/11/2013	19:03:17	30.86
10/11/2013	19:04:18	37.73
10/11/2013	19:05:18	41.49
10/11/2013	19:06:18	33.42
10/11/2013	19:07:19	28.12
10/11/2013	19:08:19	24.42
10/11/2013	19:09:19	28.47
10/11/2013	19:10:17	32.11
10/11/2013	19:11:18	35.91
10/11/2013	19:12:18	31.9
Average	1881 sampl	25.19
Test Run 10 End		

Test Run 11 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	19:35:45	16.3
10/11/2013	19:36:45	16.9
10/11/2013	19:37:45	19.2
10/11/2013	19:38:46	19.43
10/11/2013	19:39:46	20.92
10/11/2013	19:40:46	21.44
10/11/2013	19:41:45	23.07
10/11/2013	19:42:45	23.32
10/11/2013	19:43:45	24.41
10/11/2013	19:44:46	25.71
10/11/2013	19:45:46	30.06
10/11/2013	19:46:46	36.61
10/11/2013	19:47:46	35.99
10/11/2013	19:48:46	29.55
10/11/2013	19:49:45	23.62
10/11/2013	19:50:45	23.25
10/11/2013	19:51:45	22.61
10/11/2013	19:52:45	23.8
10/11/2013	19:53:46	21.47
10/11/2013	19:54:46	20.75
10/11/2013	19:55:46	21.14
10/11/2013	19:56:46	22.12
10/11/2013	19:57:45	23.08
10/11/2013	19:58:45	22.57
10/11/2013	19:59:46	25.43
10/11/2013	20:00:46	26.18
10/11/2013	20:01:46	27.36
10/11/2013	20:02:46	26.43
10/11/2013	20:03:45	32.28
10/11/2013	20:04:45	29.23
10/11/2013	20:05:45	34.45
10/11/2013	20:06:45	34.13
10/11/2013	20:07:46	30.96
10/11/2013	20:08:46	30.2
10/11/2013	20:09:46	32.75
10/11/2013	20:10:47	36.19
10/11/2013	20:11:45	38.78
10/11/2013	20:12:45	37.58
10/11/2013	20:13:45	34.83
10/11/2013	20:14:46	30.77
10/11/2013	20:15:46	30.88
10/11/2013	20:16:46	31.74
10/11/2013	20:17:46	34.53
10/11/2013	20:18:45	42.51
10/11/2013	20:19:45	44.65

10/11/2013	20:20:45	35.45
10/11/2013	20:21:46	25.21
10/11/2013	20:22:46	23.77
10/11/2013	20:23:46	28.87
10/11/2013	20:24:46	36.75
10/11/2013	20:25:45	45.05
10/11/2013	20:26:45	45.64
10/11/2013	20:27:45	41.52
10/11/2013	20:28:45	35.53
10/11/2013	20:29:46	33.91
10/11/2013	20:30:46	34.59
10/11/2013	20:31:46	29.84
10/11/2013	20:32:46	31.48
10/11/2013	20:33:45	39.63
10/11/2013	20:34:45	36.38
Average	1794 sampl	29.72
Test Run 11 End		

Test Run 12 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	20:49:06	22.17
10/11/2013	20:50:04	21.67
10/11/2013	20:51:04	23.4
10/11/2013	20:52:05	24.29
10/11/2013	20:53:05	25.04
10/11/2013	20:54:05	26.33
10/11/2013	20:55:05	26.92
10/11/2013	20:56:06	25.87
10/11/2013	20:57:06	25.72
10/11/2013	20:58:04	25.14
10/11/2013	20:59:04	25.52
10/11/2013	21:00:05	25.37
10/11/2013	21:01:05	25.64
10/11/2013	21:02:05	26.15
10/11/2013	21:03:05	26.08
10/11/2013	21:04:06	24.52
10/11/2013	21:05:04	25.79
10/11/2013	21:06:04	26.55
10/11/2013	21:07:04	27.79
10/11/2013	21:08:05	28.72
10/11/2013	21:09:05	27.24
10/11/2013	21:10:05	30.06
10/11/2013	21:11:05	33.03
10/11/2013	21:12:06	28.99
10/11/2013	21:13:04	20.95
10/11/2013	21:14:04	19.34
10/11/2013	21:15:05	19.67
10/11/2013	21:16:05	21.55
10/11/2013	21:17:05	26.17
10/11/2013	21:18:05	34.11
10/11/2013	21:19:06	29.02
10/11/2013	21:20:06	23.47
10/11/2013	21:21:04	18.29
10/11/2013	21:22:04	20.47
10/11/2013	21:23:05	20.63
10/11/2013	21:24:05	18.82
10/11/2013	21:25:05	18.74
10/11/2013	21:26:06	17.07
10/11/2013	21:27:04	17.1
10/11/2013	21:28:04	18.57
10/11/2013	21:29:05	22.44
10/11/2013	21:30:05	23.51
10/11/2013	21:31:05	23.1
10/11/2013	21:32:05	23.66
10/11/2013	21:33:05	26.36

10/11/2013	21:34:06	29.16
10/11/2013	21:35:04	30.42
10/11/2013	21:36:04	24.58
10/11/2013	21:37:05	22.02
10/11/2013	21:38:05	21.27
10/11/2013	21:39:05	22.01
10/11/2013	21:40:05	21.7
10/11/2013	21:41:06	25.89
10/11/2013	21:42:06	27.16
10/11/2013	21:43:04	26.97
10/11/2013	21:44:04	27.62
10/11/2013	21:45:04	25.38
10/11/2013	21:46:05	22.73
10/11/2013	21:47:05	22.71
10/11/2013	21:48:05	24.06
Average	1802 samp	24.43
Test Run 12 End		

Test Run 13 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/12/2013	8:58:20	33.01
10/12/2013	8:59:20	33.09
10/12/2013	9:00:21	33.69
10/12/2013	9:01:21	33.38
10/12/2013	9:02:19	34.58
10/12/2013	9:03:19	34.24
10/12/2013	9:04:20	32.82
10/12/2013	9:05:20	31.76
10/12/2013	9:06:20	31.56
10/12/2013	9:07:20	32.43
10/12/2013	9:08:21	32.07
10/12/2013	9:09:21	33.62
10/12/2013	9:10:21	35.22
10/12/2013	9:11:19	35.73
10/12/2013	9:12:20	36.7
10/12/2013	9:13:20	38.36
10/12/2013	9:14:20	39.65
10/12/2013	9:15:20	36.74
10/12/2013	9:16:21	34.73
10/12/2013	9:17:21	37.06
10/12/2013	9:18:19	39.31
10/12/2013	9:19:19	40.7
10/12/2013	9:20:20	41.32
10/12/2013	9:21:20	42.72
10/12/2013	9:22:20	44.45
10/12/2013	9:23:21	41.77
10/12/2013	9:24:21	41.75
10/12/2013	9:25:19	40.84
10/12/2013	9:26:19	40.01
10/12/2013	9:27:20	39.81
10/12/2013	9:28:20	38.16
10/12/2013	9:29:20	36.14
10/12/2013	9:30:20	33.8
10/12/2013	9:31:21	42.88
10/12/2013	9:32:21	44.68
10/12/2013	9:33:19	48.06
10/12/2013	9:34:19	48.98
10/12/2013	9:35:20	49.89
10/12/2013	9:36:20	50.59
10/12/2013	9:37:20	48.17
10/12/2013	9:38:20	42.62
10/12/2013	9:39:21	41.05
10/12/2013	9:40:21	40.93
10/12/2013	9:41:19	38.08
10/12/2013	9:42:19	36.88

10/12/2013	9:43:20	38.28
10/12/2013	9:44:20	37.83
10/12/2013	9:45:20	38.96
10/12/2013	9:46:20	39.74
10/12/2013	9:47:21	39.65
10/12/2013	9:48:21	38.16
10/12/2013	9:49:19	36.49
10/12/2013	9:50:19	37.79
10/12/2013	9:51:20	38.86
10/12/2013	9:52:20	38.2
10/12/2013	9:53:20	39.36
10/12/2013	9:54:21	42.28
10/12/2013	9:55:21	42.37
10/12/2013	9:56:19	42.48
10/12/2013	9:57:19	42.15
10/12/2013	9:58:20	42.58
Average	1843 sampl	39.05
Test Run 13 End		

Test Run 14 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/12/2013	10:23:19	38.78
10/12/2013	10:24:19	38.95
10/12/2013	10:25:20	37.38
10/12/2013	10:26:20	35.26
10/12/2013	10:27:20	33.47
10/12/2013	10:28:21	33.54
10/12/2013	10:29:21	35.1
10/12/2013	10:30:19	36.39
10/12/2013	10:31:19	38.16
10/12/2013	10:32:20	37.83
10/12/2013	10:33:20	38.5
10/12/2013	10:34:20	39.8
10/12/2013	10:35:20	41.11
10/12/2013	10:36:20	43.31
10/12/2013	10:37:21	43.12
10/12/2013	10:38:19	41.6
10/12/2013	10:39:19	40.09
10/12/2013	10:40:20	41.76
10/12/2013	10:41:20	37.42
10/12/2013	10:42:20	35.32
10/12/2013	10:43:20	36.85
10/12/2013	10:44:21	37.03
10/12/2013	10:45:21	37.63
10/12/2013	10:46:19	37.23
10/12/2013	10:47:19	36.6
10/12/2013	10:48:20	36.58
10/12/2013	10:49:20	34.3
10/12/2013	10:50:20	32.95
10/12/2013	10:51:20	35.86
10/12/2013	10:52:21	40.36
10/12/2013	10:53:21	41.13
10/12/2013	10:54:19	40.92
10/12/2013	10:55:19	38.94
10/12/2013	10:56:20	35.9
10/12/2013	10:57:20	34.71
10/12/2013	10:58:20	35.12
10/12/2013	10:59:20	38.4
10/12/2013	11:00:21	38.46
10/12/2013	11:01:19	38.96
10/12/2013	11:02:19	39.11
10/12/2013	11:03:20	39.66
10/12/2013	11:04:20	37.43
10/12/2013	11:05:20	32.13
10/12/2013	11:06:20	25.88
10/12/2013	11:07:21	22.76

10/12/2013	11:08:19	20.44
10/12/2013	11:09:19	21.39
10/12/2013	11:10:20	19.1
10/12/2013	11:11:20	20.05
10/12/2013	11:12:20	19.67
10/12/2013	11:13:20	20.48
10/12/2013	11:14:21	23.27
10/12/2013	11:15:21	23.34
10/12/2013	11:16:19	22.56
10/12/2013	11:17:19	20.89
10/12/2013	11:18:20	21.23
10/12/2013	11:19:20	22.61
10/12/2013	11:20:20	24.32
10/12/2013	11:21:20	25.83
10/12/2013	11:22:21	25.38
Average	1802 sampl	33.29
Test Run 14 End		

Test Run 15 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/12/2013	11:41:41	42.04
10/12/2013	11:42:42	38.71
10/12/2013	11:43:42	37.78
10/12/2013	11:44:42	33.87
10/12/2013	11:45:42	33.86
10/12/2013	11:46:43	38.57
10/12/2013	11:47:43	38.29
10/12/2013	11:48:41	37.43
10/12/2013	11:49:41	35.42
10/12/2013	11:50:42	35.35
10/12/2013	11:51:42	36.29
10/12/2013	11:52:42	36.18
10/12/2013	11:53:42	39.17
10/12/2013	11:54:43	41.21
10/12/2013	11:55:43	45.09
10/12/2013	11:56:41	44.99
10/12/2013	11:57:42	42.66
10/12/2013	11:58:42	41.22
10/12/2013	11:59:42	40.64
10/12/2013	12:00:42	41.76
10/12/2013	12:01:43	41.25
10/12/2013	12:02:43	40.48
10/12/2013	12:03:41	40.5
10/12/2013	12:04:41	35.92
10/12/2013	12:05:42	39.32
10/12/2013	12:06:42	39.55
10/12/2013	12:07:42	37.98
10/12/2013	12:08:42	37.41
10/12/2013	12:09:43	34.56
10/12/2013	12:10:43	32.14
10/12/2013	12:11:41	30.17
10/12/2013	12:12:42	29.4
10/12/2013	12:13:42	31.84
10/12/2013	12:14:42	31.63
10/12/2013	12:15:42	30.68
10/12/2013	12:16:43	30.88
10/12/2013	12:17:43	31.21
10/12/2013	12:18:41	33.29
10/12/2013	12:19:41	35.08
10/12/2013	12:20:42	36.57
10/12/2013	12:21:42	34.06
10/12/2013	12:22:42	32.44
10/12/2013	12:23:43	31.77
10/12/2013	12:24:43	31.01
10/12/2013	12:25:41	31.56

10/12/2013	12:26:41	32.83
10/12/2013	12:27:42	31.92
10/12/2013	12:28:42	33.46
10/12/2013	12:29:42	33.76
10/12/2013	12:30:43	33.98
10/12/2013	12:31:43	33.51
10/12/2013	12:32:41	33.07
10/12/2013	12:33:41	32.11
10/12/2013	12:34:41	34.32
10/12/2013	12:35:42	32.87
10/12/2013	12:36:42	33.76
10/12/2013	12:37:42	35.71
10/12/2013	12:38:42	32.83
10/12/2013	12:39:43	31.48
10/12/2013	12:40:43	32.15
Average	1794 sampl	35.65
Test Run 15 End		

Test Run 1 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/12/2013	15:09:26	1001.1
10/12/2013	15:10:26	1022.4
10/12/2013	15:11:26	1009.4
10/12/2013	15:12:26	1027.4
10/12/2013	15:13:27	1045.1
10/12/2013	15:14:27	1073.3
10/12/2013	15:15:26	1039.6
10/12/2013	15:16:26	1038.3
10/12/2013	15:17:26	1049.6
10/12/2013	15:18:26	1074.6
10/12/2013	15:19:27	1072.1
10/12/2013	15:20:27	1010.8
10/12/2013	15:21:27	962.7
10/12/2013	15:22:25	922.6
10/12/2013	15:23:26	912.5
10/12/2013	15:24:26	885.5
10/12/2013	15:25:26	971
10/12/2013	15:26:27	1016
10/12/2013	15:27:27	1059.8
10/12/2013	15:28:27	1099.5
10/12/2013	15:29:25	1128.8
10/12/2013	15:30:26	1126.8
10/12/2013	15:31:26	1103.4
10/12/2013	15:32:26	1069.6
10/12/2013	15:33:27	1011.3
10/12/2013	15:34:27	1040.7
10/12/2013	15:35:27	1079.2
10/12/2013	15:36:25	1094
10/12/2013	15:37:26	1082.4
10/12/2013	15:38:26	1112.7
10/12/2013	15:39:26	1120.2
10/12/2013	15:40:26	1154.1
10/12/2013	15:41:27	1168.4
10/12/2013	15:42:27	1163.2
10/12/2013	15:43:27	1133.2
10/12/2013	15:44:26	1049.9
10/12/2013	15:45:26	1053.5
10/12/2013	15:46:26	1027
10/12/2013	15:47:26	1020.1
10/12/2013	15:48:27	1022.4
10/12/2013	15:49:27	1050
10/12/2013	15:50:27	1065.4
10/12/2013	15:51:25	1040.1
10/12/2013	15:52:26	1079.5
10/12/2013	15:53:26	1113.1

10/12/2013	15:54:26	1144
10/12/2013	15:55:26	1128.2
10/12/2013	15:56:27	1054
10/12/2013	15:57:27	993.8
10/12/2013	15:58:27	1039.7
10/12/2013	15:59:25	1073
10/12/2013	16:00:26	1061.5
10/12/2013	16:01:26	1101.2
10/12/2013	16:02:26	1085.7
10/12/2013	16:03:26	1125.9
10/12/2013	16:04:27	1169.1
10/12/2013	16:05:27	1190.6
10/12/2013	16:06:27	1218.4
10/12/2013	16:07:26	1252.7
10/12/2013	16:08:26	1293.9
Average	1811 sampl	1074.7
Test Run 1 End		

Test Run 2 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/12/2013	16:36:23	989.3
10/12/2013	16:37:21	1058.5
10/12/2013	16:38:22	1059.2
10/12/2013	16:39:22	1090.3
10/12/2013	16:40:22	1113.4
10/12/2013	16:41:23	1157.2
10/12/2013	16:42:23	1148.6
10/12/2013	16:43:23	1105.5
10/12/2013	16:44:21	1046.7
10/12/2013	16:45:22	1012.7
10/12/2013	16:46:22	968.8
10/12/2013	16:47:22	963.1
10/12/2013	16:48:22	949.2
10/12/2013	16:49:23	960.6
10/12/2013	16:50:23	959
10/12/2013	16:51:21	942.5
10/12/2013	16:52:22	962.3
10/12/2013	16:53:22	925.5
10/12/2013	16:54:22	960.7
10/12/2013	16:55:23	971.3
10/12/2013	16:56:23	990.3
10/12/2013	16:57:23	949.2
10/12/2013	16:58:21	891.5
10/12/2013	16:59:22	905.3
10/12/2013	17:00:22	914.1
10/12/2013	17:01:22	914.2
10/12/2013	17:02:23	926.1
10/12/2013	17:03:23	930.9
10/12/2013	17:04:23	895.7
10/12/2013	17:05:21	943.1
10/12/2013	17:06:22	943.9
10/12/2013	17:07:22	978.3
10/12/2013	17:08:22	940.6
10/12/2013	17:09:23	993.2
10/12/2013	17:10:23	996.5
10/12/2013	17:11:23	986.9
10/12/2013	17:12:21	952
10/12/2013	17:13:22	875.5
10/12/2013	17:14:22	916.5
10/12/2013	17:15:22	939.4
10/12/2013	17:16:23	930.8
10/12/2013	17:17:23	919.8
10/12/2013	17:18:23	938.6
10/12/2013	17:19:21	999.3
10/12/2013	17:20:22	986.2

10/12/2013	17:21:22	963
10/12/2013	17:22:22	910.9
10/12/2013	17:23:23	886.5
10/12/2013	17:24:23	873.2
10/12/2013	17:25:21	870.2
10/12/2013	17:26:21	876.3
10/12/2013	17:27:22	925.8
10/12/2013	17:28:22	911.6
10/12/2013	17:29:22	865.7
10/12/2013	17:30:22	850
10/12/2013	17:31:23	893.9
10/12/2013	17:32:23	913.1
10/12/2013	17:33:21	915.1
10/12/2013	17:34:21	918.1
10/12/2013	17:35:22	960.6
10/12/2013	17:36:22	942.2
Average	1824 sampl	957
Test Run 2 End		

Test Run 3 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/12/2013	18:00:49	1126.2
10/12/2013	18:01:49	1091.3
10/12/2013	18:02:49	1034.6
10/12/2013	18:03:49	996.3
10/12/2013	18:04:50	1063.4
10/12/2013	18:05:50	1027.2
10/12/2013	18:06:50	995.6
10/12/2013	18:07:48	1085.5
10/12/2013	18:08:49	1133.7
10/12/2013	18:09:49	1177.7
10/12/2013	18:10:49	1174.3
10/12/2013	18:11:50	1169.6
10/12/2013	18:12:50	1112.9
10/12/2013	18:13:50	1135.7
10/12/2013	18:14:50	1102.2
10/12/2013	18:15:49	1176.6
10/12/2013	18:16:49	1201.9
10/12/2013	18:17:49	1217
10/12/2013	18:18:49	1248
10/12/2013	18:19:50	1297.6
10/12/2013	18:20:50	1351.7
10/12/2013	18:21:50	1412.8
10/12/2013	18:22:49	1417.9
10/12/2013	18:23:49	1368.5
10/12/2013	18:24:49	1287.4
10/12/2013	18:25:49	1173.7
10/12/2013	18:26:50	1198.4
10/12/2013	18:27:50	1205.2
10/12/2013	18:28:50	1198.8
10/12/2013	18:29:50	1194.9
10/12/2013	18:30:49	1174.8
10/12/2013	18:31:49	1184.2
10/12/2013	18:32:49	1161.6
10/12/2013	18:33:50	1200.8
10/12/2013	18:34:50	1239.5
10/12/2013	18:35:50	1260.8
10/12/2013	18:36:50	1242.4
10/12/2013	18:37:49	1230.9
10/12/2013	18:38:49	1200.6
10/12/2013	18:39:49	1159
10/12/2013	18:40:49	1156.6
10/12/2013	18:41:50	1183.6
10/12/2013	18:42:50	1112.7
10/12/2013	18:43:50	1146.3
10/12/2013	18:44:48	1178.5

10/12/2013	18:45:49	1184.8
10/12/2013	18:46:49	1190.2
10/12/2013	18:47:49	1236.3
10/12/2013	18:48:50	1229.3
10/12/2013	18:49:50	1299.9
10/12/2013	18:50:50	1314.9
10/12/2013	18:51:48	1303.2
10/12/2013	18:52:49	1305.8
10/12/2013	18:53:49	1308.6
10/12/2013	18:54:49	1314
10/12/2013	18:55:50	1277
10/12/2013	18:56:50	1203.3
10/12/2013	18:57:50	1144.9
10/12/2013	18:58:48	1242.6
10/12/2013	18:59:49	1242.4
Average	1796 sampl	1200
Test Run 3 End		

Test Run 9 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/13/2013	9:22:03	71.7
10/13/2013	9:23:03	73.9
10/13/2013	9:24:04	76.1
10/13/2013	9:25:04	78.7
10/13/2013	9:26:04	80.4
10/13/2013	9:27:04	82.1
10/13/2013	9:28:05	83.8
10/13/2013	9:29:03	85.1
10/13/2013	9:30:03	85.8
10/13/2013	9:31:03	86.3
10/13/2013	9:32:04	86.9
10/13/2013	9:33:04	87.8
10/13/2013	9:34:04	88
10/13/2013	9:35:05	89.5
10/13/2013	9:36:03	87.7
10/13/2013	9:37:03	87
10/13/2013	9:38:03	86.1
10/13/2013	9:39:04	85.2
10/13/2013	9:40:04	84.8
10/13/2013	9:41:04	85.1
10/13/2013	9:42:04	85.9
10/13/2013	9:43:05	87.4
10/13/2013	9:44:03	88.9
10/13/2013	9:45:03	89.8
10/13/2013	9:46:03	90.7
10/13/2013	9:47:04	90.6
10/13/2013	9:48:04	90.8
10/13/2013	9:49:04	92.2
10/13/2013	9:50:05	93.7
10/13/2013	9:51:03	93.8
10/13/2013	9:52:03	94.6
10/13/2013	9:53:03	95.6
10/13/2013	9:54:04	96
10/13/2013	9:55:04	96.3
10/13/2013	9:56:04	97
10/13/2013	9:57:04	97.5
10/13/2013	9:58:05	98
10/13/2013	9:59:03	98.3
10/13/2013	10:00:03	99.7
10/13/2013	10:01:03	100.8
10/13/2013	10:02:04	101.7
10/13/2013	10:03:04	102.4
10/13/2013	10:04:04	103
10/13/2013	10:05:05	102.3
10/13/2013	10:06:03	101.1

10/13/2013	10:07:03	100
10/13/2013	10:08:03	98.6
10/13/2013	10:09:04	98.2
10/13/2013	10:10:04	98.4
10/13/2013	10:11:04	98.1
10/13/2013	10:12:04	97.6
10/13/2013	10:13:05	96.8
10/13/2013	10:14:03	95.4
10/13/2013	10:15:03	92.2
10/13/2013	10:16:03	91.5
10/13/2013	10:17:04	93.1
10/13/2013	10:18:04	94.6
10/13/2013	10:19:04	97.1
10/13/2013	10:20:04	97.7
10/13/2013	10:21:05	97.5
Average	1797 sampl	91.8
Test Run 9 End		

Test Run 10 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/13/2013	11:04:49	77.08
10/13/2013	11:05:50	78.11
10/13/2013	11:06:50	78.19
10/13/2013	11:07:50	77.63
10/13/2013	11:08:50	77.56
10/13/2013	11:09:51	77.71
10/13/2013	11:10:51	77.97
10/13/2013	11:11:49	77.89
10/13/2013	11:12:49	78.97
10/13/2013	11:13:50	79.14
10/13/2013	11:14:50	77.97
10/13/2013	11:15:51	76.86
10/13/2013	11:16:49	76.19
10/13/2013	11:17:49	76.58
10/13/2013	11:18:50	76.82
10/13/2013	11:19:50	77.53
10/13/2013	11:20:50	78.27
10/13/2013	11:21:50	79.01
10/13/2013	11:22:51	79.04
10/13/2013	11:23:51	78.95
10/13/2013	11:24:49	78.85
10/13/2013	11:25:50	78.45
10/13/2013	11:26:50	78.1
10/13/2013	11:27:50	78.55
10/13/2013	11:28:50	78.58
10/13/2013	11:29:51	78.39
10/13/2013	11:30:51	78.37
10/13/2013	11:31:49	79.42
10/13/2013	11:32:49	81.98
10/13/2013	11:33:50	84.04
10/13/2013	11:34:50	83.84
10/13/2013	11:35:50	83.55
10/13/2013	11:36:50	83.19
10/13/2013	11:37:51	82.62
10/13/2013	11:38:51	82.45
10/13/2013	11:39:49	82.09
10/13/2013	11:40:49	81.91
10/13/2013	11:41:50	81.54
10/13/2013	11:42:50	81.56
10/13/2013	11:43:50	82.21
10/13/2013	11:44:51	82.55
10/13/2013	11:45:51	82.6
10/13/2013	11:46:49	82.99
10/13/2013	11:47:49	83.33
10/13/2013	11:48:50	83.22

10/13/2013	11:49:50	83.17
10/13/2013	11:50:50	84.26
10/13/2013	11:51:50	86.33
10/13/2013	11:52:51	87.37
10/13/2013	11:53:51	85.99
10/13/2013	11:54:49	85.29
10/13/2013	11:55:49	85.22
10/13/2013	11:56:50	86.39
10/13/2013	11:57:50	86.43
10/13/2013	11:58:50	85.81
10/13/2013	11:59:50	86.1
10/13/2013	12:00:51	86.23
10/13/2013	12:01:51	84.93
10/13/2013	12:02:49	82.97
10/13/2013	12:03:50	82.23
10/13/2013	12:04:50	84.21
Average	1825 sampl	81.24
Test Run 10 End		

Test Run 11 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/13/2013	12:31:14	107.99
10/13/2013	12:32:14	108.6
10/13/2013	12:33:15	109.57
10/13/2013	12:34:15	112.47
10/13/2013	12:35:15	115.91

Pause

10/13/2013	12:36:15	115.09
10/13/2013	12:37:14	112.39
10/13/2013	12:38:14	111.26
10/13/2013	12:39:14	112.42
10/13/2013	12:40:14	113.56
10/13/2013	12:41:15	114.42
10/13/2013	12:42:15	113.98
10/13/2013	12:43:15	112.12
10/13/2013	12:44:15	110.5
10/13/2013	12:45:14	109.3
10/13/2013	12:46:14	108.63
10/13/2013	12:47:14	110.13
10/13/2013	12:48:14	112.11
10/13/2013	12:49:15	112.2
10/13/2013	12:50:15	111.62
10/13/2013	12:51:15	111.91

End Pause

10/13/2013	12:52:15	111.76
10/13/2013	12:53:14	110.85
10/13/2013	12:54:14	109.25
10/13/2013	12:55:14	107.32
10/13/2013	12:56:15	105.6
10/13/2013	12:57:15	105.51
10/13/2013	12:58:15	105.13
10/13/2013	12:59:15	103.83
10/13/2013	13:00:15	101.32
10/13/2013	13:01:14	100.13
10/13/2013	13:02:14	99.2
10/13/2013	13:03:14	99
10/13/2013	13:04:14	99.6
10/13/2013	13:05:15	100.72
10/13/2013	13:06:15	100.21
10/13/2013	13:07:15	99.39
10/13/2013	13:08:15	99
10/13/2013	13:09:14	98.91
10/13/2013	13:10:14	98.55
10/13/2013	13:11:14	99.06
10/13/2013	13:12:15	99.18
10/13/2013	13:13:15	99.24

10/13/2013	13:14:15	100.67
10/13/2013	13:15:15	101.29
10/13/2013	13:16:14	100.86
10/13/2013	13:17:14	100.04
10/13/2013	13:18:14	99.03
10/13/2013	13:19:14	99.26
10/13/2013	13:20:15	100.68
10/13/2013	13:21:15	100.36
10/13/2013	13:22:15	99.65
10/13/2013	13:23:15	98.28
10/13/2013	13:24:14	96.42
10/13/2013	13:25:14	96.23
10/13/2013	13:26:14	96.14
10/13/2013	13:27:14	94.87
10/13/2013	13:28:15	95.34
10/13/2013	13:29:15	94.94
10/13/2013	13:30:15	94.01
10/13/2013	13:31:14	92.64
10/13/2013	13:32:14	91.56
10/13/2013	13:33:14	89.78
10/13/2013	13:34:14	87.93
10/13/2013	13:35:15	86.12
10/13/2013	13:36:15	85.57
10/13/2013	13:37:15	85.8
10/13/2013	13:38:14	85.88
10/13/2013	13:39:14	85.76
10/13/2013	13:40:14	85.56
10/13/2013	13:41:14	85.49
10/13/2013	13:42:15	84.8
10/13/2013	13:43:15	84.44
10/13/2013	13:44:15	83.05
10/13/2013	13:45:15	81.96
10/13/2013	13:46:14	81
10/13/2013	13:47:14	81.22
Average	1833 sampl	97.19
Test Run 11 End		

Enviva - Wiggins  
Run 1

Date: 10-Oct  
Run Time: 0917-1017  
(CEM Run Time Eastern)

Parameter	Symbol	Green Hammermill
		THC (as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, zero}$	0.0
Low-Level Gas	$C_{v, low}$	27.99
Mid-Level Gas	$C_{v, mid}$	50
High-Level Gas	$C_{v, high}$	86.13
Calibration Span	CS	100

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.3
Mid-Level Gas	$C_{Dir, mid}$	50.8
High-Level Gas	$C_{Dir, high}$	86.5

0900

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.0
Low-Level Gas	$ACE_{low}$	1.1
Mid-Level Gas	$ACE_{mid}$	1.6
High-Level Gas	$ACE_{high}$	0.4
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0
Final Zero	$C_{s, zero (post)}$	0.11
Upscale Gas Standard	$C_{MA}$	50.0
Initial Upscale	$C_{v, up (pre)}$	50.8
Final Upscale	$C_{v, up (post)}$	50.65

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.0
Zero (post)	$SB_{final} (zero)$	0.1
Upscale (pre)	$SB_i (upscale)$	0.0
Upscale (post)	$SB_{final} (upscale)$	-0.1
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	0.1
Upscale	$D_{upscale}$	-0.1
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	30.8
Bias Average - Zero	$C_0$	N/A
Bias Average - Upscale	$C_M$	N/A
Corrected Run Average	$C_{Gas}$	30.8

Enviva - Wiggins  
Run 2

Date: 10-Oct  
Run Time: 1036-1136

Parameter	Symbol	Green Hammermill
		THC (as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.3
Mid-Level Gas	$C_{Dir, mid}$	50.8
High-Level Gas	$C_{Dir, high}$	86.5

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.0
Low-Level Gas	$ACE_{low}$	1.1
Mid-Level Gas	$ACE_{mid}$	1.6
High-Level Gas	$ACE_{high}$	0.4
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.11
Final Zero	$C_{s, zero (post)}$	0.05
Upscale Gas Standard	$C_{MA}$	50.0
Initial Upscale	$C_{v, up (pre)}$	50.65
Final Upscale	$C_{v, up (post)}$	50.1

System Bias - Results (Percent)		
Zero (pre)	$SB_{i (zero)}$	0.1
Zero (post)	$SB_{final (zero)}$	0.1
Upscale (pre)	$SB_{i (upscale)}$	-0.1
Upscale (post)	$SB_{final (upscale)}$	-0.7
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	-0.1
Upscale	$D_{upscale}$	-0.5
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	32.23
Bias Average - Zero	$C_0$	N/A
Bias Average - Upscale	$C_M$	N/A
Corrected Run Average	$C_{Gas}$	<b>32.2</b>

Enviva - Wiggins  
Run 3

Date: 10-Oct  
Run Time: 1150-1250

Parameter	Symbol	Green Hammermill
		THC (as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.3
Mid-Level Gas	$C_{Dir, mid}$	50.8
High-Level Gas	$C_{Dir, high}$	86.5

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.0
Low-Level Gas	$ACE_{low}$	1.1
Mid-Level Gas	$ACE_{mid}$	1.6
High-Level Gas	$ACE_{high}$	0.4
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.05
Final Zero	$C_{s, zero (post)}$	0.1
Upscale Gas Standard	$C_{MA}$	50.0
Initial Upscale	$C_{v, up (pre)}$	50.1
Final Upscale	$C_{v, up (post)}$	49.8

System Bias - Results (Percent)		
Zero (pre)	$SB_{i (zero)}$	0.1
Zero (post)	$SB_{final (zero)}$	0.1
Upscale (pre)	$SB_{i (upscale)}$	-0.7
Upscale (post)	$SB_{final (upscale)}$	-1.0
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	0.1
Upscale	$D_{upscale}$	-0.3
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	26.38
Bias Average - Zero	$C_0$	N/A
Bias Average - Upscale	$C_M$	N/A
Corrected Run Average	$C_{Gas}$	<b>26.4</b>

Enviva - Wiggins  
Run #7

Date: 11-Oct  
Run Time: 1343-1443

Parameter	Symbol	Pellet Cooler 2
		THC (as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, zero}$	0.0
Low-Level Gas	$C_{v, low}$	27.99
Mid-Level Gas	$C_{v, mid}$	50
High-Level Gas	$C_{v, high}$	86.13
Calibration Span	CS	100

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.15

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.0
Low-Level Gas	$ACE_{low}$	0.4
Mid-Level Gas	$ACE_{mid}$	2.2
High-Level Gas	$ACE_{high}$	0.0
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.04
Final Zero	$C_{s, zero (post)}$	0.35
Upscale Gas Standard	$C_{MA}$	50.0
Initial Upscale	$C_{v, up (pre)}$	50.14
Final Upscale	$C_{v, up (post)}$	50.2

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.0
Zero (post)	$SB_{final} (zero)$	0.3
Upscale (pre)	$SB_i (upscale)$	-1.0
Upscale (post)	$SB_{final} (upscale)$	-0.9
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	0.3
Upscale	$D_{upscale}$	0.1
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	23.80
Bias Average - Zero	$C_0$	N/A
Bias Average - Upscale	$C_M$	N/A
Corrected Run Average	$C_{Gas}$	23.8

Enviva - Wiggins  
Run #8

Date: 11-Oct  
Run Time: 1508-1608

Parameter	Symbol	Pellet Cooler 2
		THC (as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.0
Low-Level Gas	$ACE_{low}$	0.4
Mid-Level Gas	$ACE_{mid}$	2.2
High-Level Gas	$ACE_{high}$	0.0
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.35
Final Zero	$C_{s, zero (post)}$	0.18
Upscale Gas Standard	$C_{MA}$	50.0
Initial Upscale	$C_{v, up (pre)}$	50.2
Final Upscale	$C_{v, up (post)}$	50.1

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.3
Zero (post)	$SB_{final} (zero)$	0.1
Upscale (pre)	$SB_i (upscale)$	-0.9
Upscale (post)	$SB_{final} (upscale)$	-1.0
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	-0.2
Upscale	$D_{upscale}$	-0.1
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	21.29
Bias Average - Zero	$C_0$	NA
Bias Average - Upscale	$C_M$	NA
Corrected Run Average	$C_{Gas}$	21.3

Enviva - Wiggins  
Run #9

Date: 11-Oct  
Run Time: 29-1729

Parameter	Symbol	Pellet Cooler 2
		THC
		(as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.0
Low-Level Gas	$ACE_{low}$	0.4
Mid-Level Gas	$ACE_{mid}$	2.2
High-Level Gas	$ACE_{high}$	0.0
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.18
Final Zero	$C_{s, zero (post)}$	0.2
Upscale Gas Standard	$C_{MA}$	50.0
Initial Upscale	$C_{v, up (pre)}$	50.1
Final Upscale	$C_{v, up (post)}$	49.8

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.1
Zero (post)	$SB_{final} (zero)$	0.2
Upscale (pre)	$SB_i (upscale)$	-1.0
Upscale (post)	$SB_{final} (upscale)$	-1.3
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	0.0
Upscale	$D_{upscale}$	-0.3
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	24.84
Bias Average - Zero	$C_0$	N/A
Bias Average - Upscale	$C_M$	N/A
Corrected Run Average	$C_{Gas}$	<b>24.8</b>

Enviva - Wiggins  
Run #4

Date: 10-Oct  
Run Time: 1738-1838

Parameter	Symbol	Dryer 1
		THC (as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, zero}$	0.0
Low-Level Gas	$C_{v, low}$	27.99
Mid-Level Gas	$C_{v, mid}$	50
High-Level Gas	$C_{v, high}$	86.13
Calibration Span	CS	100

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.3
Mid-Level Gas	$C_{Dir, mid}$	50.8
High-Level Gas	$C_{Dir, high}$	86.5

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.0
Low-Level Gas	$ACE_{low}$	1.1
Mid-Level Gas	$ACE_{mid}$	1.6
High-Level Gas	$ACE_{high}$	0.4
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0
Final Zero	$C_{s, zero (post)}$	0.85
Upscale Gas Standard	$C_{MA}$	50.0
Initial Upscale	$C_{v, up (pre)}$	50.8
Final Upscale	$C_{v, up (post)}$	50.9

System Bias - Results (Percent)		
Zero (pre)	$SB_{i (zero)}$	0.0
Zero (post)	$SB_{final (zero)}$	0.9
Upscale (pre)	$SB_{i (upscale)}$	0.0
Upscale (post)	$SB_{final (upscale)}$	0.1
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	0.9
Upscale	$D_{upscale}$	0.1
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	66.70
Bias Average - Zero	$C_0$	N/A
Bias Average - Upscale	$C_M$	N/A
Corrected Run Average	$C_{Gas}$	66.7

Enviva - Wiggins  
Run #5

Date: 11-Oct  
Run Time: 1000-1100

Parameter	Symbol	Dryer 1
		THC (as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, zero}$	0.0
Low-Level Gas	$C_{v, low}$	28.0
Mid-Level Gas	$C_{v, mid}$	50.0
High-Level Gas	$C_{v, high}$	86.1
Calibration Span	CS	100.0

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.0
Low-Level Gas	$ACE_{low}$	0.4
Mid-Level Gas	$ACE_{mid}$	2.2
High-Level Gas	$ACE_{high}$	0.0
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.85
Final Zero	$C_{s, zero (post)}$	0.15
Upscale Gas Standard	$C_{MA}$	50.0
Initial Upscale	$C_{v, up (pre)}$	50.9
Final Upscale	$C_{v, up (post)}$	50.5

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.8
Zero (post)	$SB_{final} (zero)$	0.1
Upscale (pre)	$SB_i (upscale)$	-0.2
Upscale (post)	$SB_{final} (upscale)$	-0.6
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	-0.7
Upscale	$D_{upscale}$	-0.4
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	61.92
Bias Average - Zero	$C_0$	N/A
Bias Average - Upscale	$C_M$	N/A
Corrected Run Average	$C_{Gas}$	<b>61.9</b>

Enviva - Wiggins  
Run #6

Date: 11-Oct  
Run Time: 1137-1237

Parameter	Symbol	Dryer 1
		THC (as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.0
Low-Level Gas	$ACE_{low}$	0.4
Mid-Level Gas	$ACE_{mid}$	2.2
High-Level Gas	$ACE_{high}$	0.0
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.15
Final Zero	$C_{s, zero (post)}$	0.1
Upscale Gas Standard	$C_{MA}$	50.0
Initial Upscale	$C_{v, up (pre)}$	50.5
Final Upscale	$C_{v, up (post)}$	50.14

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.1
Zero (post)	$SB_{final} (zero)$	0.1
Upscale (pre)	$SB_i (upscale)$	-0.6
Upscale (post)	$SB_{final} (upscale)$	-1.0
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	-0.1
Upscale	$D_{upscale}$	-0.4
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	57.17
Bias Average - Zero	$C_0$	N/A
Bias Average - Upscale	$C_M$	N/A
Corrected Run Average	$C_{Gas}$	<b>57.2</b>

Parameter	Symbol	Hammermill 2
		THC (as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, zero}$	0.0
Low-Level Gas	$C_{v, low}$	27.99
Mid-Level Gas	$C_{v, mid}$	50
High-Level Gas	$C_{v, high}$	86.13
Calibration Span	CS	100

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.15

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.0
Low-Level Gas	$ACE_{low}$	0.4
Mid-Level Gas	$ACE_{mid}$	2.2
High-Level Gas	$ACE_{high}$	0.0
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.2
Final Zero	$C_{s, zero (post)}$	0.08
Upscale Gas Standard	$C_{MA}$	50.0
Initial Upscale	$C_{v, up (pre)}$	49.8
Final Upscale	$C_{v, up (post)}$	50

System Bias - Results (Percent)		
Zero (pre)	$SB_{i (zero)}$	0.2
Zero (post)	$SB_{final (zero)}$	0.0
Upscale (pre)	$SB_{i (upscale)}$	-1.3
Upscale (post)	$SB_{final (upscale)}$	-1.1
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	-0.1
Upscale	$D_{upscale}$	0.2
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	25.19
Bias Average - Zero	$C_0$	N/A
Bias Average - Upscale	$C_M$	N/A
Corrected Run Average	$C_{Gas}$	25.2

Enviva - Wiggins  
Run 11

Date: 11-Oct  
Run Time: 1935-2035

Parameter	Symbol	Hammermill 2
		THC (as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.0
Low-Level Gas	$ACE_{low}$	0.4
Mid-Level Gas	$ACE_{mid}$	2.2
High-Level Gas	$ACE_{high}$	0.0
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.08
Final Zero	$C_{s, zero (post)}$	0.21
Upscale Gas Standard	$C_{MA}$	50.0
Initial Upscale	$C_{v, up (pre)}$	50
Final Upscale	$C_{v, up (post)}$	49.85

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.0
Zero (post)	$SB_{final} (zero)$	0.2
Upscale (pre)	$SB_i (upscale)$	-1.1
Upscale (post)	$SB_{final} (upscale)$	-1.3
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	0.1
Upscale	$D_{upscale}$	-0.1
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	29.72
Bias Average - Zero	$C_0$	N/A
Bias Average - Upscale	$C_M$	N/A
Corrected Run Average	$C_{Gas}$	<b>29.7</b>

Enviva - Wiggins  
Run 12

Date: 10/11/2013  
Run Time: 2048-2148

Parameter	Symbol	Hammermill 2
		THC (as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.0
Low-Level Gas	$ACE_{low}$	0.4
Mid-Level Gas	$ACE_{mid}$	2.2
High-Level Gas	$ACE_{high}$	0.0
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.21
Final Zero	$C_{s, zero (post)}$	0.23
Upscale Gas Standard	$C_{MA}$	50.0
Initial Upscale	$C_{v, up (pre)}$	49.85
Final Upscale	$C_{v, up (post)}$	49.9

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.2
Zero (post)	$SB_{final} (zero)$	0.2
Upscale (pre)	$SB_i (upscale)$	-1.3
Upscale (post)	$SB_{final} (upscale)$	-1.2
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	0.0
Upscale	$D_{upscale}$	0.0
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	24.43
Bias Average - Zero	$C_0$	N/A
Bias Average - Upscale	$C_M$	N/A
Corrected Run Average	$C_{Gas}$	<b>24.4</b>

Parameter	Symbol	Pellet Cooler 1
		THC (as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, zero}$	0.0
Low-Level Gas	$C_{v, low}$	27.99
Mid-Level Gas	$C_{v, mid}$	50
High-Level Gas	$C_{v, high}$	86.13
Calibration Span	CS	100

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.1
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	50.4
High-Level Gas	$C_{Dir, high}$	86.15

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.1
Low-Level Gas	$ACE_{low}$	0.4
Mid-Level Gas	$ACE_{mid}$	0.8
High-Level Gas	$ACE_{high}$	0.0
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.1
Final Zero	$C_{s, zero (post)}$	0.35
Upscale Gas Standard	$C_{MA}$	50.0
Initial Upscale	$C_{v, up (pre)}$	50.4
Final Upscale	$C_{v, up (post)}$	50.3

System Bias - Results (Percent)		
Zero (pre)	$SB_{i (zero)}$	0.0
Zero (post)	$SB_{final (zero)}$	0.3
Upscale (pre)	$SB_{i (upscale)}$	0.0
Upscale (post)	$SB_{final (upscale)}$	-0.1
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	0.3
Upscale	$D_{upscale}$	-0.1
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	39.05
Bias Average - Zero	$C_0$	N/A
Bias Average - Upscale	$C_M$	N/A
Corrected Run Average	$C_{Gas}$	39.1

Enviva - Wiggins  
Run 14

Date: 12-Oct  
Run Time: 1022-1122

Parameter	Symbol	Pellet Cooler 1
		THC (as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.1
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	50.4
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.1
Low-Level Gas	$ACE_{low}$	0.4
Mid-Level Gas	$ACE_{mid}$	0.8
High-Level Gas	$ACE_{high}$	0.0
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.35
Final Zero	$C_{s, zero (post)}$	0.24
Upscale Gas Standard	$C_{MA}$	50.0
Initial Upscale	$C_{v, up (pre)}$	50.3
Final Upscale	$C_{v, up (post)}$	50.25

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.3
Zero (post)	$SB_{final} (zero)$	
Upscale (pre)	$SB_i (upscale)$	-0.1
Upscale (post)	$SB_{final} (upscale)$	
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	-0.1
Upscale	$D_{upscale}$	0.0
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	33.29
Bias Average - Zero	$C_0$	N/A
Bias Average - Upscale	$C_M$	N/A
Corrected Run Average	$C_{Gas}$	<b>33.3</b>

Enviva - Wiggins  
Run 15

Date: 12-Oct  
Run Time: 1141-124

Parameter	Symbol	Pellet Cooler 1
		THC (as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.1
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	50.4
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.1
Low-Level Gas	$ACE_{low}$	0.4
Mid-Level Gas	$ACE_{mid}$	0.8
High-Level Gas	$ACE_{high}$	0.0
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.24
Final Zero	$C_{s, zero (post)}$	0.33
Upscale Gas Standard	$C_{MA}$	50.0
Initial Upscale	$C_{v, up (pre)}$	50.25
Final Upscale	$C_{v, up (post)}$	50.1

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.2
Zero (post)	$SB_{final} (zero)$	0.3
Upscale (pre)	$SB_i (upscale)$	-0.1
Upscale (post)	$SB_{final} (upscale)$	-0.3
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	0.1
Upscale	$D_{upscale}$	-0.1
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	35.65
Bias Average - Zero	$C_0$	N/A
Bias Average - Upscale	$C_M$	N/A
Corrected Run Average	$C_{Gas}$	<b>35.7</b>

Parameter	Symbol	Aspirator
		THC (as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, zero}$	0.0
Low-Level Gas	$C_{v, low}$	258.1
Mid-Level Gas	$C_{v, mid}$	507.1
High-Level Gas	$C_{v, high}$	836.9
Calibration Span	CS	1000

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	1.1
Low-Level Gas	$C_{Dir, low}$	260
Mid-Level Gas	$C_{Dir, mid}$	507
High-Level Gas	$C_{Dir, high}$	838.3

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.1
Low-Level Gas	$ACE_{low}$	0.7
Mid-Level Gas	$ACE_{mid}$	0.0
High-Level Gas	$ACE_{high}$	0.1
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	1.1
Final Zero	$C_{s, zero (post)}$	2.4
Upscale Gas Standard	$C_{MA}$	836.9
Initial Upscale	$C_{v, up (pre)}$	838.3
Final Upscale	$C_{v, up (post)}$	837

System Bias - Results (Percent)		
Zero (pre)	$SB_{i (zero)}$	0.0
Zero (post)	$SB_{final (zero)}$	0.1
Upscale (pre)	$SB_{i (upscale)}$	0.0
Upscale (post)	$SB_{final (upscale)}$	-0.1
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	0.1
Upscale	$D_{upscale}$	-0.1
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	1074.70
Bias Average - Zero	$C_0$	N/A
Bias Average - Upscale	$C_M$	N/A
Corrected Run Average	$C_{Gas}$	1074.7

Parameter	Symbol	Aspirator
		THC (as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, zero}$	0.0
Low-Level Gas	$C_{v, low}$	258.1
Mid-Level Gas	$C_{v, mid}$	507.1
High-Level Gas	$C_{v, high}$	836.9
Calibration Span	CS	1000.0

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	1.1
Low-Level Gas	$C_{Dir, low}$	260.0
Mid-Level Gas	$C_{Dir, mid}$	507.0
High-Level Gas	$C_{Dir, high}$	838.3

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.1
Low-Level Gas	$ACE_{low}$	0.7
Mid-Level Gas	$ACE_{mid}$	0.0
High-Level Gas	$ACE_{high}$	0.1
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	2.40
Final Zero	$C_{s, zero (post)}$	1.4
Upscale Gas Standard	$C_{MA}$	836.9
Initial Upscale	$C_{v, up (pre)}$	837
Final Upscale	$C_{v, up (post)}$	837.5

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.1
Zero (post)	$SB_{final} (zero)$	0.0
Upscale (pre)	$SB_i (upscale)$	-0.1
Upscale (post)	$SB_{final} (upscale)$	-0.1
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	-0.1
Upscale	$D_{upscale}$	0.1
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	957.00
Bias Average - Zero	$C_0$	N/A
Bias Average - Upscale	$C_M$	N/A
Corrected Run Average	$C_{Gas}$	<b>957.0</b>

Enviva - Wiggins  
Run 18

Date: 12-Oct  
Run Time: 1800-1900

Parameter	Symbol	Aspirator
		THC (as C <sub>3</sub> H <sub>8</sub> )
		ppm <sub>w</sub>

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	1.1
Low-Level Gas	$C_{Dir, low}$	260.0
Mid-Level Gas	$C_{Dir, mid}$	507.0
High-Level Gas	$C_{Dir, high}$	838.3

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	$ACE_{zero}$	0.1
Low-Level Gas	$ACE_{low}$	0.7
Mid-Level Gas	$ACE_{mid}$	0.0
High-Level Gas	$ACE_{high}$	0.1
Specification	$ACE_{spec}$	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	1.40
Final Zero	$C_{s, zero (post)}$	2
Upscale Gas Standard	$C_{MA}$	836.9
Initial Upscale	$C_{v, up (pre)}$	837.5
Final Upscale	$C_{v, up (post)}$	835

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.0
Zero (post)	$SB_{final} (zero)$	0.1
Upscale (pre)	$SB_i (upscale)$	-0.1
Upscale (post)	$SB_{final} (upscale)$	-0.3
Specification	$SB_{spec}$	NA

System Drift - Results (Percent)		
Zero	$D_{zero}$	0.1
Upscale	$D_{upscale}$	-0.3
Specification	$D_{spec}$	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	$C_{ave}$	1200.00
Bias Average - Zero	$C_0$	N/A
Bias Average - Upscale	$C_M$	N/A
Corrected Run Average	$C_{Gas}$	<b>1200.0</b>

Parameter	Symbol	Dryer 2	
		THC (as C <sub>3</sub> H <sub>8</sub> )	
		ppm <sub>w</sub>	

**Analyzer Calibration Error - Calibration Standards**

Zero Gas	$C_{v, zero}$	0.0	0.0
Low-Level Gas	$C_{v, low}$	258.1	27.99
Mid-Level Gas	$C_{v, mid}$	507.1	50
High-Level Gas	$C_{v, high}$	836.9	86.13
Calibration Span	CS	1000	100

**Analyzer Calibration Error - Instrument Response**

Zero Gas	$C_{Dir, zero}$	1.0	1.0
Low-Level Gas	$C_{Dir, low}$	259	28.4
Mid-Level Gas	$C_{Dir, mid}$	506.8	50.34
High-Level Gas	$C_{Dir, high}$	837.3	86.24

**Analyzer Calibration Error - Results (Percent of Span)**

Zero Gas	$ACE_{zero}$	0.1	1.0
Low-Level Gas	$ACE_{low}$	0.3	1.5
Mid-Level Gas	$ACE_{mid}$	-0.1	0.7
High-Level Gas	$ACE_{high}$	0.0	0.1
Specification	$ACE_{spec}$	±5	±8

**System Calibrations - Instrument Response**

Initial Zero	$C_{s, zero (pre)}$	1.0	1.0
Final Zero	$C_{s, zero (post)}$	1.6	1.6
Upscale Gas Standard	$C_{MA}$	507.1	50.0
Initial Upscale	$C_{v, up (pre)}$	506.8	50.34
Final Upscale	$C_{v, up (post)}$	504	50.6

**System Bias - Results (Percent)**

Zero (pre)	$SB_i (zero)$	0.0	0.0
Zero (post)	$SB_{final} (zero)$	0.1	0.6
Upscale (pre)	$SB_i (upscale)$	0.0	0.0
Upscale (post)	$SB_{final} (upscale)$	-0.3	0.3
Specification	$SB_{spec}$	NA	NA

**System Drift - Results (Percent)**

Zero	$D_{zero}$	0.1	0.6
Upscale	$D_{upscale}$	-0.3	0.3
Specification	$D_{spec}$	±3	±6

**Response Test - Results (seconds)**

Upscale Test		NA	NA
Zero Test		NA	NA
Response Time		28	28

**Calibration Correction**

Raw Average	$C_{ave}$	91.8	91.8
Bias Average - Zero	$C_o$	N/A	N/A
Bias Average - Upscale	$C_M$	N/A	N/A
Corrected Run Average	$C_{Gas}$	91.8	91.8

Enviva - Wiggins  
Run 20

Date: 13-Oct  
Run Time: 1104-1204

Parameter	Symbol	Dryer 2	
		THC (as C <sub>3</sub> H <sub>8</sub> )	
		ppm <sub>w</sub>	

**Analyzer Calibration Error - Calibration Standards**

Zero Gas	$C_{v, zero}$	0.0	0.0
Low-Level Gas	$C_{v, low}$	258.1	28.0
Mid-Level Gas	$C_{v, mid}$	507.1	50.0
High-Level Gas	$C_{v, high}$	836.9	86.1
Calibration Span	CS	1000.0	100.0

**Analyzer Calibration Error - Instrument Response**

Zero Gas	$C_{Dir, zero}$	1.0	1.0
Low-Level Gas	$C_{Dir, low}$	259.0	28.4
Mid-Level Gas	$C_{Dir, mid}$	506.8	50.3
High-Level Gas	$C_{Dir, high}$	837.3	86.2

**Analyzer Calibration Error - Results (Percent of Span)**

Zero Gas	$ACE_{zero}$	0.1	1.0
Low-Level Gas	$ACE_{low}$	0.3	1.5
Mid-Level Gas	$ACE_{mid}$	-0.1	0.7
High-Level Gas	$ACE_{high}$	0.0	0.1
Specification	$ACE_{spec}$	±5	±8

**System Calibrations - Instrument Response**

Initial Zero	$C_{s, zero (pre)}$	1.60	1.60
Final Zero	$C_{s, zero (post)}$	0.42	0.42
Upscale Gas Standard	$C_{MA}$	507.1	50.0
Initial Upscale	$C_{v, up (pre)}$	504	50.6
Final Upscale	$C_{v, up (post)}$	503	50.4

**System Bias - Results (Percent)**

Zero (pre)	$SB_{i (zero)}$	0.1	0.6
Zero (post)	$SB_{final (zero)}$	-0.1	-0.6
Upscale (pre)	$SB_{i (upscale)}$	-0.3	0.3
Upscale (post)	$SB_{final (upscale)}$	-0.4	0.1
Specification	$SB_{spec}$	NA	NA

**System Drift - Results (Percent)**

Zero	$D_{zero}$	-0.1	-1.2
Upscale	$D_{upscale}$	-0.1	-0.2
Specification	$D_{spec}$	±3	±3

**Response Test - Results (seconds)**

Upscale Test		NA	NA
Zero Test		NA	NA
Response Time		28	28

**Calibration Correction**

Raw Average	$C_{ave}$	81.2	81.2
Bias Average - Zero	$C_o$	N/A	N/A
Bias Average - Upscale	$C_M$	N/A	N/A
Corrected Run Average	$C_{Gas}$	<b>81.2</b>	<b>81.2</b>

Enviva - Wiggins  
Run 21

Date: 13-Oct  
Run Time: 1231-1347  
Paused (1236-1252)

Parameter	Symbol	Dryer 2	
		THC (as C <sub>3</sub> H <sub>8</sub> )	
		ppm <sub>w</sub>	

Analyzer Calibration Error - Instrument Response			
Zero Gas	$C_{Dir, zero}$	1.0	1.00
Low-Level Gas	$C_{Dir, low}$	259.0	28.40
Mid-Level Gas	$C_{Dir, mid}$	506.8	50.34
High-Level Gas	$C_{Dir, high}$	837.3	86.24

Analyzer Calibration Error - Results (Percent of Span)			
Zero Gas	$ACE_{zero}$	0.1	1.0
Low-Level Gas	$ACE_{low}$	0.3	1.5
Mid-Level Gas	$ACE_{mid}$	-0.1	0.7
High-Level Gas	$ACE_{high}$	0.0	0.1
Specification	$ACE_{spec}$	±5	±8

System Calibrations - Instrument Response			
Initial Zero	$C_{s, zero (pre)}$	0.42	0.42
Final Zero	$C_{s, zero (post)}$	0.3	0.3
Upscale Gas Standard	$C_{MA}$	507.1	50.0
Initial Upscale	$C_{v, up (pre)}$	503	50.4
Final Upscale	$C_{v, up (post)}$	503.5	50.2

System Bias - Results (Percent)			
Zero (pre)	$SB_i (zero)$	-0.1	-0.6
Zero (post)	$SB_{final} (zero)$	-0.1	-0.7
Upscale (pre)	$SB_i (upscale)$	-0.4	0.1
Upscale (post)	$SB_{final} (upscale)$	-0.3	-0.1
Specification	$SB_{spec}$	NA	NA

System Drift - Results (Percent)			
Zero	$D_{zero}$	0.0	-0.1
Upscale	$D_{upscale}$	0.1	-0.2
Specification	$D_{spec}$	±3	±6

Response Test - Results (seconds)			
Upscale Test		NA	NA
Zero Test		NA	NA
Response Time		28	31

Calibration Correction			
Raw Average	$C_{ave}$	97.2	97.2
Bias Average - Zero	$C_0$	N/A	N/A
Bias Average - Upscale	$C_M$	N/A	N/A
Corrected Run Average	$C_{Gas}$	<b>97.2</b>	<b>97.2</b>

## **APPENDIX C**

### **Method 320 Data**

Company ACT  
 Analyst Initials CJT  
 Parameters EPA Method 320  
 # Samples 21 Runs

Client # 1911  
 Job # 0913-111  
 PO # 3134 1911  
 Report Date V0.62 13.10.18.12.58

Compound	Sample ID / Concentration (ppmv wet)					
	<b>Data Runs</b>					
	<b>GMH Run 1</b>	<b>GMH Run 2</b>	<b>GMH Run 3</b>	<b>Dryer 1 Run 1</b>	<b>Dryer 1 Run 2</b>	<b>Dryer 1 Run 3</b>
Acrolein	1.13 J	1.20 J	1.15 J	1.79 J	1.72 ND	1.72 ND
Formaldehyde	0.742	0.629	0.561	3.32	1.60	1.78
Methanol	0.508	0.460	0.376	2.52	1.70	1.59
Phenol	0.88 ND	0.88 ND	0.88 ND	2.04 ND	2.04 ND	2.04 ND
Propionaldehyde	0.234 ND	0.234 ND	0.251 J	0.644 J	0.714 J	0.505 J
acetaldehyde	0.756 J	0.721 J	0.723 J	1.27 ND	1.27 ND	1.27 ND
	<b>Data Runs</b>					
	<b>Pellet Cooler 2 Run 1</b>	<b>Pellet Cooler 2 Run 2</b>	<b>Pellet Cooler 2 Run 3</b>	<b>Hammermill 2 Run 1</b>	<b>Hammermill 2 Run 2</b>	<b>Hammermill 2 Run 3</b>
Acrolein	1.29 J	1.21 J	1.33 J	0.980 J	0.975 J	0.965 ND
Formaldehyde	1.07	0.663	1.84	1.04	1.14	1.11
Methanol	0.797	0.680 J	0.844	0.189 J	0.211 J	0.204 J
Phenol	1.08 ND	1.08 ND	1.08 ND	1.08 ND	1.08 ND	1.08 ND
Propionaldehyde	0.246 J	0.246 ND	0.359 J	0.233 J	0.243 J	0.263 J
acetaldehyde	0.864 J	0.825 J	0.786 J	0.715 J	0.710 J	0.707 ND
	<b>Data Runs</b>					
	<b>Pellet Cooler 1 Run 1</b>	<b>Pellet Cooler 1 Run 2</b>	<b>Pellet Cooler 1 Run 3</b>	<b>Aspirator Run 1</b>	<b>Aspirator Run 2</b>	<b>Aspirator Run 3</b>
Acrolein	0.976 J	1.02 J	1.35 J	3.16	3.12	2.25 J
Formaldehyde	1.44	1.25	1.26	1.05 ND	1.58 J	1.06 J
Methanol	0.537	0.327	0.351	8.30	8.90	8.16
Phenol	1.00 J	0.98 ND	0.98 ND	2.73 ND	2.73 ND	2.73 ND
Propionaldehyde	0.381 J	0.290 J	0.236 ND	3.00 ND	3.00 ND	3.00 ND
acetaldehyde	0.691 J	0.695 J	0.759 J	4.65	3.92 J	3.75
	<b>Data Runs</b>					
	<b>Dryer 2 Run 1</b>	<b>Dryer 2 Run 2</b>	<b>Dryer 2 Run 3</b>			
Acrolein	1.90 J	2.59	2.49			
Formaldehyde	6.40	6.58	6.76			
Methanol	18.8	10.2	10.8			
Phenol	2.78 ND	2.78 ND	2.78 ND			
Propionaldehyde	2.37	1.38	1.70			
acetaldehyde	0.967 J	3.28	1.02 J			

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	V0.62 13.10.18.12.58

**Minimum Detectable Concentration - Default**

	GMH	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
Run 1		1.13	0.502	0.742	0.0719	0.51	0.0912	0.88	0.44	0.234	0.120	0.756	0.371
Run 2		1.20	0.474	0.629	0.0684	0.46	0.0935	0.88	0.44	0.234	0.118	0.721	0.351
Run 3		1.15	0.480	0.561	0.0677	0.38	0.0913	0.88	0.45	0.251	0.113	0.723	0.355
Average SEC(ppm):		0.485		0.0693		0.0920		0.44		0.117		0.359	
MDC(ppm):		<b>0.971</b>		<b>0.139</b>		<b>0.184</b>		<b>0.88</b>		<b>0.234</b>		<b>0.718</b>	
<b>Dryer 1</b>													
Run 1		1.79	0.917	3.32	0.131	2.52	0.296	2.04	1.00	0.644	0.239	1.270	0.679
Run 2		1.72	0.850	1.60	0.126	1.70	0.293	2.04	1.07	0.714	0.227	1.270	0.628
Run 3		1.72	0.812	1.78	0.120	1.59	0.287	2.04	0.99	0.505	0.213	1.270	0.598
Average SEC(ppm):		0.859		0.126		0.292		1.02		0.226		0.635	
MDC(ppm):		<b>1.72</b>		<b>0.252</b>		<b>0.584</b>		<b>2.04</b>		<b>0.452</b>		<b>1.27</b>	
<b>Pellet Cooler 2</b>													
Run 1		1.29	0.496	1.07	0.0711	0.80	0.0813	1.08	0.54	0.246	0.125	0.864	0.370
Run 2		1.21	0.497	0.663	0.0704	0.68	0.0823	1.08	0.54	0.246	0.120	0.825	0.370
Run 3		1.33	0.507	1.84	0.0732	0.84	0.0844	1.09	0.55	0.359	0.124	0.786	0.378
Average SEC(ppm):		0.500		0.0716		0.0826		0.54		0.123		0.373	
MDC(ppm):		<b>1.00</b>		<b>0.143</b>		<b>0.165</b>		<b>1.08</b>		<b>0.246</b>		<b>0.745</b>	
<b>Hammermill 2</b>													
Run 1		0.98	0.480	1.04	0.0677	0.19	0.0809	1.08	0.54	0.233	0.113	0.715	0.353
Run 2		0.97	0.480	1.14	0.0682	0.21	0.0832	1.08	0.54	0.243	0.122	0.710	0.352
Run 3		0.97	0.488	1.11	0.0675	0.20	0.0839	1.08	0.55	0.263	0.113	0.707	0.356
Average SEC(ppm):		0.483		0.0678		0.0826		0.54		0.116		0.354	
MDC(ppm):		<b>0.965</b>		<b>0.136</b>		<b>0.165</b>		<b>1.08</b>		<b>0.232</b>		<b>0.707</b>	
<b>Pellet Cooler 1</b>													
Run 1		0.98	0.467	1.44	0.0646	0.54	0.0738	1.00	0.50	0.381	0.118	0.691	0.344
Run 2		1.02	0.463	1.25	0.0635	0.33	0.0723	0.98	0.50	0.290	0.119	0.695	0.341
Run 3		1.35	0.467	1.26	0.0647	0.35	0.0690	0.98	0.48	0.236	0.118	0.759	0.345
Average SEC(ppm):		0.466		0.0642		0.0717		0.49		0.118		0.343	
MDC(ppm):		<b>0.931</b>		<b>0.128</b>		<b>0.143</b>		<b>0.98</b>		<b>0.236</b>		<b>0.686</b>	
<b>Aspirator</b>													
Run 1		3.16	0.827	1.055	0.535	8.30	0.244	2.73	1.15	3.00	1.53	4.65	0.616
Run 2		3.12	0.808	1.58	0.467	8.90	0.256	2.73	1.60	3.00	1.35	3.92	0.602
Run 3		2.25	0.916	1.063	0.580	8.16	0.265	2.73	1.34	3.00	1.62	3.75	0.681
Average SEC(ppm):		0.850		0.527		0.255		1.36		1.50		0.633	
MDC(ppm):		<b>1.70</b>		<b>1.05</b>		<b>0.510</b>		<b>2.73</b>		<b>3.00</b>		<b>1.27</b>	
<b>Dryer 2</b>													
Run 1		1.90	0.631	6.40	0.108	18.8	0.539	2.78	1.29	2.37	0.222	0.967	0.472
Run 2		2.59	0.617	6.58	0.105	10.2	0.549	2.78	1.55	1.38	0.260	3.28	0.457
Run 3		2.49	0.633	6.76	0.112	10.8	0.531	2.78	1.33	1.70	0.263	1.02	0.473
Average SEC(ppm):		0.627		0.108		0.540		1.39		0.248		0.467	
MDC(ppm):		<b>1.25</b>		<b>0.217</b>		<b>1.08</b>		<b>2.78</b>		<b>0.497</b>		<b>0.934</b>	

Company ACT  
 Analyst Initials CUT  
 Parameters EPA Method 320  
 # Samples 21 Runs

Client # 1911  
 Job # 0913-111  
 PO # 3134 1911  
 Report Date V0.62 13.10.18.12.58

GMH Run 1																
Date	Method	Filename	DF	Acrotrin (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/10/2013 9:17	0913-111.A	13.10.10.0917_37_936	1	1.58	0.517	0.846	0.0700	0.434	0.0900	0.88	0.43	0.234	0.114	0.718	0.383	
10/10/2013 9:18	0913-111.A	13.10.10.0918_38_786	1	0.971	0.472	0.708	0.0680	0.457	0.0890	0.88	0.43	0.234	0.112	0.718	0.346	
10/10/2013 9:19	0913-111.A	13.10.10.0919_39_506	1	0.971	0.504	0.778	0.0720	0.443	0.0920	0.88	0.43	0.234	0.115	0.718	0.373	
10/10/2013 9:20	0913-111.A	13.10.10.0920_40_336	1	0.971	0.464	0.696	0.0690	0.467	0.0890	0.88	0.44	0.234	0.111	0.718	0.345	
10/10/2013 9:21	0913-111.A	13.10.10.0921_41_006	1	1.59	0.483	0.633	0.0700	0.454	0.0920	0.88	0.43	0.234	0.114	0.793	0.365	
10/10/2013 9:22	0913-111.A	13.10.10.0922_41_806	1	0.971	0.493	0.708	0.0680	0.457	0.0880	0.88	0.44	0.234	0.114	0.718	0.360	
10/10/2013 9:23	0913-111.A	13.10.10.0923_42_538	1	0.971	0.464	0.614	0.0660	0.469	0.0890	0.88	0.44	0.234	0.111	0.718	0.341	
10/10/2013 9:24	0913-111.A	13.10.10.0924_43_348	1	1.15	0.462	0.696	0.0630	0.481	0.0900	0.88	0.44	0.234	0.111	0.718	0.336	
10/10/2013 9:25	0913-111.A	13.10.10.0925_44_128	1	0.971	0.465	0.696	0.0680	0.477	0.0900	0.88	0.43	0.234	0.110	0.718	0.347	
10/10/2013 9:26	0913-111.A	13.10.10.0926_44_818	1	0.971	0.498	0.782	0.0660	0.407	0.0870	0.88	0.44	0.234	0.115	0.750	0.375	
10/10/2013 9:27	0913-111.A	13.10.10.0927_45_818	1	0.971	0.459	0.759	0.0660	0.491	0.0870	0.88	0.44	0.234	0.108	0.718	0.335	
10/10/2013 9:28	0913-111.A	13.10.10.0928_46_429	1	1.16	0.499	0.620	0.0690	0.383	0.0890	0.88	0.44	0.234	0.116	0.718	0.370	
10/10/2013 9:29	0913-111.A	13.10.10.0929_47_159	1	1.61	0.471	0.784	0.0680	0.445	0.0870	0.88	0.43	0.234	0.113	0.718	0.348	
10/10/2013 9:30	0913-111.A	13.10.10.0930_47_959	1	0.971	0.454	0.803	0.0660	0.537	0.0880	0.88	0.44	0.234	0.111	0.718	0.332	
10/10/2013 9:31	0913-111.A	13.10.10.0931_48_709	1	0.971	0.477	0.775	0.0700	0.442	0.0910	0.88	0.44	0.234	0.118	0.718	0.353	
10/10/2013 9:32	0913-111.A	13.10.10.0932_49_519	1	0.971	0.460	0.746	0.0660	0.477	0.0910	0.88	0.44	0.234	0.113	0.718	0.348	
10/10/2013 9:33	0913-111.A	13.10.10.0933_50_289	1	0.971	0.491	0.723	0.0730	0.473	0.0890	0.88	0.44	0.234	0.118	0.718	0.357	
10/10/2013 9:34	0913-111.A	13.10.10.0934_50_859	1	0.971	0.491	0.731	0.0680	0.456	0.0910	0.88	0.44	0.234	0.117	0.718	0.360	
10/10/2013 9:35	0913-111.A	13.10.10.0935_51_689	1	0.971	0.469	0.739	0.0680	0.477	0.0870	0.88	0.44	0.234	0.112	0.718	0.349	
10/10/2013 9:36	0913-111.A	13.10.10.0936_52_439	1	0.971	0.483	0.650	0.0710	0.446	0.0890	0.88	0.44	0.234	0.117	0.718	0.359	
10/10/2013 9:37	0913-111.A	13.10.10.0937_53_149	1	1.32	0.467	0.751	0.0700	0.448	0.0910	0.88	0.44	0.234	0.116	0.718	0.373	
10/10/2013 9:38	0913-111.A	13.10.10.0938_53_929	1	0.971	0.467	0.668	0.0680	0.467	0.0890	0.88	0.44	0.234	0.115	0.718	0.345	
10/10/2013 9:39	0913-111.A	13.10.10.0939_54_720	1	0.971	0.483	0.800	0.0720	0.416	0.0930	0.88	0.44	0.234	0.118	0.718	0.354	
10/10/2013 9:40	0913-111.A	13.10.10.0940_55_430	1	0.971	0.487	0.703	0.0680	0.393	0.0910	0.88	0.44	0.234	0.117	0.718	0.357	
10/10/2013 9:41	0913-111.A	13.10.10.0941_56_230	1	0.971	0.504	0.745	0.0710	0.435	0.0870	0.88	0.44	0.234	0.118	0.718	0.370	
10/10/2013 9:42	0913-111.A	13.10.10.0942_57_010	1	1.00	0.613	0.813	0.0700	0.410	0.0910	0.88	0.44	0.234	0.117	0.718	0.387	
10/10/2013 9:43	0913-111.A	13.10.10.0943_57_650	1	0.971	0.473	0.697	0.0690	0.415	0.0910	0.88	0.44	0.234	0.112	0.718	0.347	
10/10/2013 9:44	0913-111.A	13.10.10.0944_58_440	1	0.971	0.477	0.736	0.0670	0.393	0.0910	0.88	0.44	0.234	0.114	0.718	0.349	
10/10/2013 9:45	0913-111.A	13.10.10.0945_59_220	1	0.971	0.482	0.634	0.0670	0.388	0.0910	0.88	0.44	0.234	0.109	0.718	0.355	
10/10/2013 9:47	0913-111.A	13.10.10.0947_60_000	1	1.48	0.477	0.644	0.0690	0.448	0.0890	0.88	0.44	0.234	0.116	0.742	0.355	
10/10/2013 9:48	0913-111.A	13.10.10.0948_60_730	1	0.971	0.461	0.774	0.0660	0.420	0.0880	0.88	0.44	0.234	0.112	0.718	0.337	
10/10/2013 9:49	0913-111.A	13.10.10.0949_61_480	1	1.29	0.487	0.773	0.0640	0.501	0.0910	0.88	0.44	0.234	0.112	0.718	0.359	
10/10/2013 9:50	0913-111.A	13.10.10.0950_62_280	1	0.971	0.483	0.721	0.0680	0.464	0.0910	0.88	0.44	0.234	0.115	0.718	0.353	
10/10/2013 9:51	0913-111.A	13.10.10.0951_63_020	1	0.971	0.476	0.710	0.0700	0.457	0.0870	0.88	0.44	0.234	0.117	0.718	0.360	
10/10/2013 9:52	0913-111.A	13.10.10.0952_63_761	1	0.971	0.489	0.663	0.0700	0.453	0.0900	0.88	0.44	0.234	0.119	0.754	0.364	
10/10/2013 9:53	0913-111.A	13.10.10.0953_64_581	1	0.971	0.500	0.789	0.0690	0.523	0.0880	0.88	0.44	0.234	0.118	0.718	0.368	
10/10/2013 9:54	0913-111.A	13.10.10.0954_65_281	1	0.971	0.455	0.660	0.0670	0.400	0.0900	0.88	0.44	0.234	0.114	0.740	0.339	
10/10/2013 9:55	0913-111.A	13.10.10.0955_66_091	1	1.41	0.469	0.869	0.0710	0.647	0.0950	0.88	0.44	0.234	0.118	0.718	0.351	
10/10/2013 9:56	0913-111.A	13.10.10.0956_66_849	1	0.971	0.480	0.740	0.0690	0.448	0.0910	0.88	0.44	0.234	0.118	0.718	0.362	
10/10/2013 9:57	0913-111.A	13.10.10.0957_67_611	1	1.30	0.482	0.870	0.0720	0.667	0.0960	0.88	0.44	0.234	0.122	0.990	0.356	
10/10/2013 9:58	0913-111.A	13.10.10.0958_68_331	1	0.971	0.488	0.920	0.0700	0.688	0.0950	0.88	0.44	0.234	0.117	0.947	0.366	
10/10/2013 9:59	0913-111.A	13.10.10.0959_69_071	1	1.42	0.496	0.677	0.0700	0.649	0.0930	0.88	0.44	0.234	0.119	0.872	0.364	
10/10/2013 10:00	0913-111.A	13.10.10.1000_69_811	1	0.971	0.482	0.821	0.0700	0.564	0.0920	0.88	0.44	0.234	0.117	0.747	0.360	
10/10/2013 10:01	0913-111.A	13.10.10.1001_70_551	1	1.12	0.489	0.624	0.0690	0.459	0.0900	0.88	0.44	0.234	0.119	0.718	0.376	
10/10/2013 10:02	0913-111.A	13.10.10.1002_71_391	1	0.971	0.487	0.650	0.0680	0.580	0.0920	0.88	0.44	0.234	0.114	0.866	0.363	
10/10/2013 10:03	0913-111.A	13.10.10.1003_72_111	1	1.80	0.503	0.846	0.0710	0.577	0.0930	0.88	0.44	0.234	0.118	0.718	0.368	
10/10/2013 10:04	0913-111.A	13.10.10.1004_73_832	1	0.978	0.474	0.794	0.0690	0.664	0.0920	0.88	0.44	0.234	0.118	0.718	0.356	
10/10/2013 10:05	0913-111.A	13.10.10.1005_74_595	1	1.21	0.489	0.769	0.0700	0.593	0.0890	0.88	0.44	0.234	0.124	0.864	0.364	
10/10/2013 10:06	0913-111.A	13.10.10.1006_74_372	1	0.971	0.476	0.718	0.0710	0.644	0.0930	0.88	0.44	0.234	0.118	0.718	0.353	
10/10/2013 10:07	0913-111.A	13.10.10.1007_75_182	1	1.07	0.497	0.720	0.0720	0.618	0.0910	0.88	0.44	0.234	0.125	0.718	0.367	
10/10/2013 10:08	0913-111.A	13.10.10.1008_75_892	1	1.28	0.512	0.804	0.0750	0.660	0.0950	0.88	0.44	0.234	0.124	0.718	0.383	
10/10/2013 10:09	0913-111.A	13.10.10.1009_76_712	1	1.61	0.551	0.828	0.0820	0.582	0.0910	0.88	0.44	0.234	0.123	0.718	0.406	
10/10/2013 10:10	0913-111.A	13.10.10.1010_77_422	1	0.986	0.569	0.796	0.0790	0.620	0.0940	0.88	0.44	0.234	0.123	0.718	0.413	
10/10/2013 10:11	0913-111.A	13.10.10.1011_78_172	1	1.39	0.537	0.667	0.0780	0.631	0.0920	0.88	0.44	0.234	0.134	0.900	0.395	
10/10/2013 10:12	0913-111.A	13.10.10.1012_78_922	1	0.971	0.535	0.703	0.0700	0.435	0.0950	0.88	0.43	0.234	0.130	1.28	0.393	
10/10/2013 10:13	0913-111.A	13.10.10.1013_79_722	1	1.48	0.582	0.825	0.0840	0.497	0.0970	0.88	0.43	0.234	0.139	1.05	0.429	
10/10/2013 10:14	0913-111.A	13.10.10.1014_80_472	1	0.999	0.582	0.694	0.0830	0.533	0.0940	0.88	0.43	0.234	0.135	0.718	0.395	
10/10/2013 10:15	0913-111.A	13.10.10.1015_81_272	1	1.71	0.651	0.963	0.0820	0.501	0.0970	0.88	0.43	0.234	0.150	0.718	0.477	
10/10/2013 10:16	0913-111.A	13.10.10.1016_81_893	1	0.971	0.705	0.431	0.0960	0.400	0.102	0.88	0.43	0.234	0.158	0.718	0.515	
10/10/2013 10:17	0913-111.A	13.10.10.1017_82_633	1	1.15	0.698	0.729	0.100	0.361	0.100	0.88	0.44	0.234	0.162	0.718	0.514	
Average Conc. (ppm):				1	1.13	0.502	0.742	0.0719	0.508	0.0912	0.88	0.44	0.234	0.120	0.756	0.371

GMH Run 2															
Date	Method	Filename	DF	Acrotrin (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/10/2013 10:36	0913-111.A	13.10.10.1036_37_174	1	1.30	0.438	0.788	0.0660	0.421	0.0890	0.88	0.43	0.234	0.115	0.718	0.324

Company ACT  
 Analyst Initials CWT  
 Parameters EPA Method 320  
 # Samples 21 Runs

Client # 1911  
 Job # 0913-111  
 PO # 1314 1911  
 Report Date VO.62 13.10.18.12.58

GMH Run 3																
Date	Method	Filename	DF	Acrotein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/10/2013 11:50	0913-111_A	13_10_10_1150_33_060	1	0.971	0.466	0.541	0.0650	0.432	0.0970	0.88	0.44	0.234	0.109	0.718	0.348	
10/10/2013 11:51	0913-111_A	13_10_10_1151_33_861	1	0.987	0.510	0.328	0.0700	0.457	0.0930	0.88	0.44	0.234	0.113	0.904	0.373	
10/10/2013 11:52	0913-111_A	13_10_10_1152_34_581	1	0.971	0.513	0.468	0.0710	0.466	0.0940	0.88	0.44	0.234	0.116	0.718	0.374	
10/10/2013 11:53	0913-111_A	13_10_10_1153_35_331	1	0.971	0.499	0.475	0.0650	0.418	0.0970	0.88	0.44	0.234	0.110	0.718	0.368	
10/10/2013 11:54	0913-111_A	13_10_10_1154_36_151	1	1.30	0.467	0.511	0.0670	0.387	0.0950	0.88	0.45	0.234	0.112	0.718	0.348	
10/10/2013 11:55	0913-111_A	13_10_10_1155_36_951	1	1.20	0.499	0.554	0.0710	0.435	0.0940	0.88	0.45	0.234	0.117	0.718	0.365	
10/10/2013 11:56	0913-111_A	13_10_10_1156_37_691	1	0.971	0.481	0.425	0.0680	0.378	0.0910	0.88	0.45	0.234	0.112	0.718	0.355	
10/10/2013 11:57	0913-111_A	13_10_10_1157_38_401	1	1.41	0.466	0.527	0.0690	0.458	0.0940	0.88	0.45	0.234	0.114	0.718	0.346	
10/10/2013 11:58	0913-111_A	13_10_10_1158_39_211	1	1.13	0.468	0.472	0.0710	0.432	0.0940	0.88	0.45	0.234	0.113	0.718	0.351	
10/10/2013 11:59	0913-111_A	13_10_10_1159_40_021	1	1.58	0.479	0.524	0.0680	0.324	0.0900	0.88	0.44	0.234	0.113	0.718	0.357	
10/10/2013 12:00	0913-111_A	13_10_10_1200_40_731	1	0.971	0.485	0.472	0.0670	0.389	0.0950	0.88	0.45	0.234	0.112	0.718	0.359	
10/10/2013 12:01	0913-111_A	13_10_10_1201_41_561	1	1.28	0.472	0.636	0.0700	0.357	0.0910	0.88	0.44	0.234	0.113	0.718	0.355	
10/10/2013 12:02	0913-111_A	13_10_10_1202_42_302	1	0.971	0.473	0.612	0.0670	0.404	0.0910	0.88	0.44	0.234	0.114	0.718	0.349	
10/10/2013 12:03	0913-111_A	13_10_10_1203_43_022	1	0.971	0.449	0.609	0.0630	0.398	0.0900	0.88	0.44	0.234	0.105	0.718	0.328	
10/10/2013 12:04	0913-111_A	13_10_10_1204_43_872	1	1.01	0.489	0.509	0.0700	0.361	0.0930	0.88	0.45	0.234	0.116	0.718	0.364	
10/10/2013 12:05	0913-111_A	13_10_10_1205_44_582	1	0.971	0.505	0.520	0.0700	0.401	0.0910	0.88	0.45	0.234	0.116	0.718	0.376	
10/10/2013 12:06	0913-111_A	13_10_10_1206_45_332	1	1.66	0.479	0.582	0.0680	0.354	0.0930	0.88	0.44	0.234	0.112	0.718	0.358	
10/10/2013 12:07	0913-111_A	13_10_10_1207_46_182	1	0.971	0.478	0.498	0.0640	0.379	0.0910	0.88	0.45	0.234	0.112	0.718	0.358	
10/10/2013 12:08	0913-111_A	13_10_10_1208_46_912	1	1.00	0.500	0.622	0.0670	0.438	0.0910	0.88	0.45	0.234	0.114	0.718	0.373	
10/10/2013 12:09	0913-111_A	13_10_10_1209_47_682	1	1.35	0.456	0.588	0.0670	0.406	0.0910	0.88	0.45	0.234	0.112	0.718	0.346	
10/10/2013 12:10	0913-111_A	13_10_10_1210_48_432	1	0.971	0.533	0.475	0.0710	0.361	0.0910	0.88	0.44	0.234	0.117	0.718	0.391	
10/10/2013 12:11	0913-111_A	13_10_10_1211_49_202	1	0.971	0.444	0.555	0.0650	0.383	0.0930	0.88	0.44	0.234	0.109	0.718	0.338	
10/10/2013 12:12	0913-111_A	13_10_10_1212_50_012	1	0.971	0.500	0.555	0.0700	0.363	0.0910	0.88	0.44	0.234	0.114	0.718	0.372	
10/10/2013 12:13	0913-111_A	13_10_10_1213_50_712	1	0.971	0.466	0.624	0.0650	0.410	0.0940	0.88	0.44	0.234	0.109	0.718	0.347	
10/10/2013 12:14	0913-111_A	13_10_10_1214_51_513	1	1.36	0.450	0.604	0.0660	0.355	0.0920	0.88	0.45	0.234	0.108	0.718	0.334	
10/10/2013 12:15	0913-111_A	13_10_10_1215_52_273	1	0.971	0.448	0.543	0.0640	0.420	0.0890	0.88	0.44	0.234	0.110	0.718	0.364	
10/10/2013 12:16	0913-111_A	13_10_10_1216_53_003	1	1.00	0.465	0.562	0.0660	0.302	0.0900	0.88	0.44	0.234	0.110	0.838	0.341	
10/10/2013 12:17	0913-111_A	13_10_10_1217_53_803	1	1.42	0.480	0.562	0.0670	0.311	0.0910	0.88	0.44	0.234	0.113	0.718	0.352	
10/10/2013 12:18	0913-111_A	13_10_10_1218_54_503	1	0.980	0.474	0.507	0.0690	0.363	0.0890	0.88	0.44	0.234	0.113	0.718	0.356	
10/10/2013 12:19	0913-111_A	13_10_10_1219_55_313	1	1.41	0.480	0.565	0.0650	0.409	0.0910	0.88	0.44	0.234	0.110	0.718	0.359	
10/10/2013 12:20	0913-111_A	13_10_10_1220_55_913	1	0.971	0.469	0.563	0.0690	0.363	0.0910	0.88	0.44	0.234	0.110	0.718	0.343	
10/10/2013 12:21	0913-111_A	13_10_10_1221_56_773	1	1.09	0.439	0.556	0.0650	0.413	0.0920	0.88	0.45	0.234	0.109	0.718	0.319	
10/10/2013 12:22	0913-111_A	13_10_10_1222_57_533	1	1.29	0.501	0.511	0.0680	0.345	0.0930	0.88	0.45	0.234	0.117	0.718	0.368	
10/10/2013 12:23	0913-111_A	13_10_10_1223_58_253	1	0.89	0.489	0.614	0.0690	0.276	0.0900	0.88	0.45	0.234	0.115	0.718	0.365	
10/10/2013 12:24	0913-111_A	13_10_10_1224_59_013	1	0.971	0.467	0.561	0.0670	0.377	0.0900	0.88	0.45	0.234	0.109	0.718	0.348	
10/10/2013 12:25	0913-111_A	13_10_10_1225_59_763	1	0.971	0.465	0.501	0.0670	0.404	0.0910	0.88	0.45	0.234	0.111	0.718	0.345	
10/10/2013 12:27	0913-111_A	13_10_10_1227_00_544	1	0.971	0.493	0.590	0.0700	0.331	0.0920	0.88	0.45	0.234	0.114	0.718	0.359	
10/10/2013 12:28	0913-111_A	13_10_10_1228_01_284	1	0.971	0.488	0.598	0.0680	0.349	0.0910	0.88	0.45	0.235	0.114	0.718	0.357	
10/10/2013 12:29	0913-111_A	13_10_10_1229_02_134	1	1.27	0.486	0.559	0.0650	0.346	0.0890	0.88	0.45	0.234	0.112	0.718	0.359	
10/10/2013 12:30	0913-111_A	13_10_10_1230_02_884	1	0.971	0.483	0.477	0.0670	0.323	0.0910	0.88	0.45	0.234	0.113	0.718	0.356	
10/10/2013 12:31	0913-111_A	13_10_10_1231_03_584	1	0.971	0.457	0.589	0.0630	0.393	0.0920	0.88	0.45	0.234	0.107	0.718	0.336	
10/10/2013 12:32	0913-111_A	13_10_10_1232_04_304	1	0.971	0.485	0.687	0.0690	0.350	0.0890	0.88	0.45	0.234	0.113	0.718	0.359	
10/10/2013 12:33	0913-111_A	13_10_10_1233_05_164	1	1.56	0.461	0.551	0.0680	0.337	0.0900	0.88	0.45	0.234	0.119	0.718	0.368	
10/10/2013 12:34	0913-111_A	13_10_10_1234_05_924	1	0.971	0.480	0.648	0.0680	0.334	0.0910	0.88	0.45	0.234	0.116	0.718	0.356	
10/10/2013 12:35	0913-111_A	13_10_10_1235_06_674	1	0.971	0.462	0.608	0.0660	0.357	0.0900	0.88	0.45	0.234	0.111	0.718	0.343	
10/10/2013 12:36	0913-111_A	13_10_10_1236_07_474	1	0.971	0.467	0.567	0.0660	0.366	0.0900	0.88	0.45	0.263	0.113	0.718	0.345	
10/10/2013 12:37	0913-111_A	13_10_10_1237_08_174	1	0.971	0.473	0.642	0.0650	0.403	0.0910	0.88	0.45	0.234	0.112	0.718	0.343	
10/10/2013 12:38	0913-111_A	13_10_10_1238_09_024	1	0.971	0.489	0.620	0.0690	0.346	0.0900	0.88	0.45	0.234	0.117	0.718	0.355	
10/10/2013 12:40	0913-111_A	13_10_10_1240_22_660	1	1.54	0.467	0.615	0.0670	0.370	0.0890	0.88	0.45	0.340	0.116	0.718	0.346	
10/10/2013 12:41	0913-111_A	13_10_10_1241_23_370	1	1.50	0.503	0.599	0.0700	0.393	0.0920	0.88	0.45	0.347	0.117	0.718	0.374	
10/10/2013 12:42	0913-111_A	13_10_10_1242_24_140	1	1.83	0.489	0.510	0.0690	0.329	0.0910	0.88	0.44	0.279	0.120	0.718	0.364	
10/10/2013 12:43	0913-111_A	13_10_10_1243_24_950	1	1.61	0.487	0.520	0.0680	0.338	0.0910	0.88	0.44	0.354	0.119	0.718	0.358	
10/10/2013 12:44	0913-111_A	13_10_10_1244_25_670	1	1.08	0.480	0.560	0.0680	0.372	0.0910	0.88	0.45	0.358	0.119	0.718	0.359	
10/10/2013 12:45	0913-111_A	13_10_10_1245_26_440	1	1.33	0.461	0.596	0.0680	0.332	0.0880	0.88	0.45	0.340	0.117	0.718	0.343	
10/10/2013 12:46	0913-111_A	13_10_10_1246_27_150	1	0.971	0.479	0.592	0.0700	0.330	0.0900	0.88	0.44	0.234	0.113	0.718	0.354	
10/10/2013 12:47	0913-111_A	13_10_10_1247_27_970	1	1.06	0.483	0.718	0.0640	0.390	0.0880	0.88	0.45	0.291	0.111	0.718	0.354	
10/10/2013 12:48	0913-111_A	13_10_10_1248_28_730	1	0.971	0.459	0.700	0.0650	0.385	0.0920	0.88	0.45	0.234	0.119	0.718	0.368	
10/10/2013 12:49	0913-111_A	13_10_10_1249_29_530	1	0.971	0.522	0.687	0.0710	0.345	0.0900	0.88	0.44	0.368	0.121	0.718	0.388	
10/10/2013 12:50	0913-111_A	13_10_10_1250_30_250	1	1.09	0.475	0.612	0.0670	0.353	0.0880	0.88	0.45	0.234	0.114	0.718	0.360	
Average Conc. (ppm):				1	1.15	0.480	0.561	0.0677	0.376	0.0913	0.88	0.45	0.251	0.113	0.723	0.355

Dryer 1 Run 1															
Date	Method	Filename	DF	Acrotein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/10/2013 17:38	0913-111_A	13_10_10_1738_19_855	1	1.87	0.963	5.41	0.145	0.145	0.311	2.04	0.94	1.36	2.04	0.253	0.711
10/10/2013 17:39	0913-111_A	13_10_10_1739_20_675	1	2.01	0.979	5.39	0.142	0.311	0.309	2.04	0.92	1.36</			

Company ACT  
 Analyst Initials CUT  
 Parameters EPA Method 320  
 # Samples 21 Runs

Client # 1911  
 Job # 0913-111  
 PO # 3134 1911  
 Report Date VO.62 13.10.18.12.58

Date	Method	Filename	DF	Acroline (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/11/2013 10:00	0913-111	A 13.10.11.1000_40_402	1	1.72	0.860	1.57	0.121	1.50	0.297	2.04	1.20	0.672	0.219	1.27	0.636
10/11/2013 10:01	0913-111	A 13.10.11.1001_41_122	1	1.72	0.811	1.50	0.116	1.53	0.301	2.04	1.18	0.500	0.215	1.27	0.591
10/11/2013 10:02	0913-111	A 13.10.11.1002_41_912	1	1.72	0.841	1.40	0.126	1.50	0.297	2.04	1.16	0.684	0.224	1.27	0.624
10/11/2013 10:03	0913-111	A 13.10.11.1003_42_642	1	1.72	0.846	1.51	0.128	1.64	0.306	2.04	1.13	0.624	0.224	1.27	0.623
10/11/2013 10:04	0913-111	A 13.10.11.1004_43_352	1	1.72	0.863	1.56	0.129	1.59	0.301	2.04	1.12	0.550	0.227	1.27	0.633
10/11/2013 10:05	0913-111	A 13.10.11.1005_44_132	1	1.72	0.825	1.53	0.122	1.52	0.297	2.04	1.10	0.513	0.219	1.27	0.603
10/11/2013 10:06	0913-111	A 13.10.11.1006_44_842	1	1.72	0.870	1.47	0.127	1.59	0.298	2.04	1.10	0.547	0.226	1.27	0.640
10/11/2013 10:07	0913-111	A 13.10.11.1007_45_652	1	1.72	0.847	1.43	0.123	1.58	0.300	2.04	1.10	0.452	0.223	1.27	0.624
10/11/2013 10:08	0913-111	A 13.10.11.1008_46_362	1	1.72	0.863	1.51	0.125	1.63	0.299	2.04	1.09	0.698	0.225	1.27	0.635
10/11/2013 10:09	0913-111	A 13.10.11.1009_47_132	1	1.72	0.883	1.42	0.127	1.63	0.292	2.04	1.08	0.688	0.225	1.27	0.646
10/11/2013 10:10	0913-111	A 13.10.11.1010_47_862	1	1.72	0.846	1.33	0.128	1.58	0.291	2.04	1.08	0.609	0.227	1.27	0.623
10/11/2013 10:11	0913-111	A 13.10.11.1011_48_603	1	1.72	0.850	1.50	0.124	1.66	0.290	2.04	1.06	0.644	0.224	1.27	0.631
10/11/2013 10:12	0913-111	A 13.10.11.1012_49_403	1	1.72	0.856	1.43	0.125	1.59	0.283	2.04	1.08	0.489	0.222	1.27	0.629
10/11/2013 10:13	0913-111	A 13.10.11.1013_50_133	1	1.72	0.854	1.48	0.128	1.61	0.291	2.04	1.09	0.613	0.226	1.27	0.632
10/11/2013 10:14	0913-111	A 13.10.11.1014_50_843	1	1.72	0.860	1.46	0.122	1.60	0.290	2.04	1.09	0.546	0.221	1.27	0.643
10/11/2013 10:15	0913-111	A 13.10.11.1015_51_633	1	1.72	0.869	1.44	0.126	1.61	0.285	2.04	1.09	0.576	0.228	1.27	0.642
10/11/2013 10:16	0913-111	A 13.10.11.1016_52_393	1	1.72	0.847	1.46	0.123	1.70	0.286	2.04	1.08	0.639	0.222	1.27	0.629
10/11/2013 10:17	0913-111	A 13.10.11.1017_53_133	1	1.72	0.852	1.52	0.127	1.64	0.282	2.04	1.08	0.710	0.226	1.27	0.631
10/11/2013 10:18	0913-111	A 13.10.11.1018_53_883	1	1.72	0.862	1.24	0.129	1.62	0.282	2.04	1.09	0.649	0.227	1.27	0.639
10/11/2013 10:19	0913-111	A 13.10.11.1019_54_693	1	1.72	0.862	1.44	0.125	1.61	0.290	2.04	1.07	0.667	0.222	1.27	0.606
10/11/2013 10:20	0913-111	A 13.10.11.1020_55_363	1	1.72	0.861	1.26	0.123	1.58	0.281	2.04	1.07	0.452	0.222	1.27	0.636
10/11/2013 10:21	0913-111	A 13.10.11.1021_56_083	1	1.72	0.843	1.35	0.128	1.56	0.281	2.04	1.07	0.537	0.227	1.27	0.627
10/11/2013 10:22	0913-111	A 13.10.11.1022_56_793	1	1.72	0.826	1.47	0.123	1.54	0.282	2.04	1.07	0.517	0.217	1.27	0.606
10/11/2013 10:23	0913-111	A 13.10.11.1023_57_534	1	1.72	0.867	1.48	0.126	1.57	0.293	2.04	1.08	0.561	0.223	1.27	0.640
10/11/2013 10:24	0913-111	A 13.10.11.1024_58_284	1	1.72	0.851	1.40	0.128	1.60	0.292	2.04	1.07	0.623	0.224	1.27	0.636
10/11/2013 10:25	0913-111	A 13.10.11.1025_58_974	1	1.72	0.867	1.50	0.122	1.61	0.286	2.04	1.05	0.599	0.226	1.27	0.635
10/11/2013 10:26	0913-111	A 13.10.11.1026_59_734	1	1.72	0.829	1.63	0.122	1.56	0.292	2.04	1.06	0.692	0.219	1.27	0.601
10/11/2013 10:28	0913-111	A 13.10.11.1028_60_474	1	1.72	0.844	1.58	0.129	1.69	0.289	2.04	1.05	0.636	0.222	1.27	0.631
10/11/2013 10:29	0913-111	A 13.10.11.1029_61_274	1	1.72	0.862	1.52	0.127	1.71	0.295	2.04	1.07	0.704	0.226	1.27	0.633
10/11/2013 10:30	0913-111	A 13.10.11.1030_61_984	1	1.72	0.829	1.44	0.123	1.64	0.288	2.04	1.07	0.523	0.220	1.27	0.610
10/11/2013 10:31	0913-111	A 13.10.11.1031_62_734	1	1.72	0.822	1.46	0.124	1.61	0.282	2.04	1.08	0.749	0.219	1.27	0.611
10/11/2013 10:32	0913-111	A 13.10.11.1032_63_544	1	1.72	0.860	1.47	0.125	1.58	0.284	2.04	1.08	0.701	0.225	1.27	0.638
10/11/2013 10:33	0913-111	A 13.10.11.1033_64_204	1	1.72	0.853	1.42	0.126	1.61	0.286	2.04	1.06	0.721	0.224	1.27	0.639
10/11/2013 10:34	0913-111	A 13.10.11.1034_65_094	1	1.72	0.865	1.48	0.125	1.58	0.282	2.04	1.07	0.542	0.227	1.27	0.631
10/11/2013 10:35	0913-111	A 13.10.11.1035_65_724	1	1.72	0.859	1.62	0.130	1.69	0.289	2.04	1.06	0.719	0.231	1.27	0.633
10/11/2013 10:36	0913-111	A 13.10.11.1036_66_535	1	1.72	0.865	1.55	0.128	1.66	0.290	2.04	1.06	0.686	0.230	1.27	0.631
10/11/2013 10:37	0913-111	A 13.10.11.1037_67_285	1	1.72	0.851	1.47	0.127	1.57	0.295	2.04	1.06	0.740	0.227	1.27	0.631
10/11/2013 10:38	0913-111	A 13.10.11.1038_67_995	1	1.72	0.833	1.52	0.127	1.71	0.293	2.04	1.05	0.687	0.229	1.27	0.613
10/11/2013 10:39	0913-111	A 13.10.11.1039_68_675	1	1.72	0.842	1.59	0.127	1.67	0.294	2.04	1.05	0.712	0.226	1.27	0.624
10/11/2013 10:40	0913-111	A 13.10.11.1040_69_475	1	1.72	0.836	1.56	0.129	1.75	0.292	2.04	1.06	0.752	0.231	1.27	0.620
10/11/2013 10:41	0913-111	A 13.10.11.1041_70_245	1	1.72	0.861	1.58	0.129	1.70	0.294	2.04	1.05	0.773	0.225	1.27	0.631
10/11/2013 10:42	0913-111	A 13.10.11.1042_71_005	1	1.72	0.846	1.59	0.125	1.74	0.293	2.04	1.05	0.693	0.227	1.27	0.630
10/11/2013 10:43	0913-111	A 13.10.11.1043_71_755	1	1.72	0.870	1.69	0.127	1.80	0.297	2.04	1.06	0.726	0.228	1.27	0.632
10/11/2013 10:44	0913-111	A 13.10.11.1044_72_415	1	1.72	0.843	1.52	0.123	1.63	0.287	2.04	1.08	0.744	0.225	1.27	0.617
10/11/2013 10:45	0913-111	A 13.10.11.1045_73_215	1	1.72	0.831	1.49	0.127	1.65	0.288	2.04	1.07	0.754	0.224	1.27	0.614
10/11/2013 10:46	0913-111	A 13.10.11.1046_73_925	1	1.72	0.838	1.57	0.126	1.69	0.291	2.04	1.05	0.694	0.223	1.27	0.627
10/11/2013 10:47	0913-111	A 13.10.11.1047_74_685	1	1.72	0.849	1.54	0.127	1.70	0.292	2.04	1.06	0.706	0.227	1.27	0.624
10/11/2013 10:48	0913-111	A 13.10.11.1048_75_466	1	1.72	0.838	1.62	0.124	1.88	0.298	2.04	1.03	0.851	0.231	1.27	0.621
10/11/2013 10:49	0913-111	A 13.10.11.1049_76_246	1	1.72	0.878	1.69	0.128	1.78	0.291	2.04	1.01	0.949	0.237	1.27	0.650
10/11/2013 10:50	0913-111	A 13.10.11.1050_76_906	1	1.72	0.890	2.24	0.131	2.08	0.319	2.04	0.98	0.875	0.231	1.27	0.668
10/11/2013 10:51	0913-111	A 13.10.11.1051_77_706	1	1.72	0.900	2.70	0.131	2.33	0.320	2.04	0.97	1.12	0.241	1.27	0.686
10/11/2013 10:52	0913-111	A 13.10.11.1052_78_486	1	1.72	0.861	2.71	0.131	2.03	0.318	2.04	0.97	1.28	0.245	1.27	0.695
10/11/2013 10:53	0913-111	A 13.10.11.1053_79_216	1	1.72	0.863	2.31	0.132	2.16	0.310	2.04	0.99	1.13	0.241	1.27	0.637
10/11/2013 10:54	0913-111	A 13.10.11.1054_79_966	1	1.72	0.855	2.12	0.129	2.04	0.310	2.04	1.01	1.17	0.237	1.27	0.634
10/11/2013 10:55	0913-111	A 13.10.11.1055_80_716	1	1.72	0.871	1.93	0.127	2.00	0.299	2.04	1.03	1.10	0.235	1.27	0.641
10/11/2013 10:56	0913-111	A 13.10.11.1056_81_466	1	1.72	0.856	1.83	0.126	1.96	0.296	2.04	1.02	1.032	0.232	1.27	0.637
10/11/2013 10:57	0913-111	A 13.10.11.1057_82_216	1	1.72	0.846	1.81	0.131	1.87	0.299	2.04	1.03	0.795	0.238	1.27	0.624
10/11/2013 10:58	0913-111	A 13.10.11.1058_82_936	1	1.72	0.846	1.87	0.128	1.87	0.304	2.04	1.04	0.971	0.228	1.27	0.623
10/11/2013 10:59	0913-111	A 13.10.11.1059_83_757	1	1.72	0.840	1.71	0.124	1.85	0.294	2.04	1.04	1.01	0.228	1.27	0.616
10/11/2013 11:00	0913-111	A 13.10.11.1100_84_457	1	1.72	0.739	1.36	0.113	1.64	0.240	2.04	1.23	0.562	0.230	1.27	0.551
<b>Average Conc. (ppm): 1 1.72 0.850 1.60 0.126 1.70 0.293 2.04 1.07 0.914 0.227 1.27 0.628</b>															

Date	Method	Filename	DF	Acroline (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/11/2013 11:37	0913-111	A 13.10.11.1137_48_670	1	1.72	0.785	1.48	0.117	1.23	0.285	2.04	1.07	0.452	0.217	1.27	0.580
10/11/2013 11:38	0913-111	A 13.10.11.1138_49_370	1	1.72	0.778	1.61	0.119	1.23	0.285	2.04	1.06	0.452	0.211	1.27	0.572
10/11/2013 11:39	0913-111	A 13.10.11.1139_50_160	1	1.72	0.799	1.54	0.121	1.32	0.284	2.04	1.05	0.452	0.217	1.27	0.577
10/11/2013 11:40	0913-111														

Company ACT  
 Analyst Initials CUT  
 Parameters EPA Method 320  
 # Samples 21 Runs

Client # 1911  
 Job # 0913-111  
 PO # 1314 1911  
 Report Date V0.62 13.10.18.12.58

Pellet Cooler 2 Run 1

Date	Method	Filename	DF	Acroline (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/11/2013 13:44	0913-111	13.10.11.1344_00_484	1	1.00	0.514	1.46	0.0740	0.972	0.0810	1.08	0.54	0.246	0.127	1.07	0.386	
10/11/2013 13:45	0913-111	13.10.11.1345_01_204	1	1.21	0.477	1.41	0.0700	0.959	0.0810	1.08	0.53	0.246	0.126	1.10	0.362	
10/11/2013 13:46	0913-111	13.10.11.1346_02_004	1	1.38	0.509	1.09	0.0710	0.876	0.0810	1.08	0.54	0.246	0.124	1.10	0.384	
10/11/2013 13:47	0913-111	13.10.11.1347_02_754	1	1.00	0.492	1.15	0.0710	0.801	0.0790	1.08	0.53	0.246	0.122	0.812	0.367	
10/11/2013 13:48	0913-111	13.10.11.1348_03_454	1	1.39	0.518	1.03	0.0690	0.829	0.0820	1.08	0.53	0.246	0.123	0.874	0.381	
10/11/2013 13:49	0913-111	13.10.11.1349_04_244	1	1.06	0.463	1.02	0.0690	0.798	0.0790	1.08	0.54	0.246	0.117	0.878	0.338	
10/11/2013 13:50	0913-111	13.10.11.1350_05_064	1	1.47	0.480	1.00	0.0700	0.818	0.0820	1.08	0.54	0.246	0.119	0.745	0.355	
10/11/2013 13:51	0913-111	13.10.11.1351_05_795	1	1.69	0.503	1.05	0.0750	0.826	0.0830	1.08	0.54	0.246	0.126	0.745	0.381	
10/11/2013 13:52	0913-111	13.10.11.1352_06_545	1	2.23	0.464	0.964	0.0750	0.730	0.0800	1.08	0.53	0.246	0.124	1.12	0.353	
10/11/2013 13:53	0913-111	13.10.11.1353_07_335	1	1.00	0.521	1.10	0.0740	0.859	0.0800	1.08	0.53	0.246	0.128	0.819	0.386	
10/11/2013 13:54	0913-111	13.10.11.1354_08_045	1	1.00	0.498	1.02	0.0680	0.823	0.0830	1.08	0.54	0.246	0.121	0.884	0.388	
10/11/2013 13:55	0913-111	13.10.11.1355_09_815	1	2.04	0.513	1.06	0.0750	0.829	0.0800	1.08	0.54	0.246	0.128	0.937	0.392	
10/11/2013 13:56	0913-111	13.10.11.1356_09_515	1	1.85	0.514	1.06	0.0750	0.861	0.0800	1.08	0.53	0.246	0.127	0.874	0.384	
10/11/2013 13:57	0913-111	13.10.11.1357_10_335	1	1.12	0.488	1.15	0.0660	0.904	0.0840	1.08	0.54	0.246	0.116	0.784	0.360	
10/11/2013 13:58	0913-111	13.10.11.1358_11_105	1	1.00	0.487	1.12	0.0700	0.817	0.0820	1.08	0.54	0.246	0.122	1.02	0.360	
10/11/2013 13:59	0913-111	13.10.11.1359_11_825	1	1.00	0.480	1.11	0.0730	0.851	0.0830	1.08	0.53	0.246	0.124	1.23	0.358	
10/11/2013 14:00	0913-111	13.10.11.1400_12_475	1	1.18	0.488	1.01	0.0700	0.854	0.0830	1.08	0.54	0.246	0.124	1.19	0.363	
10/11/2013 14:01	0913-111	13.10.11.1401_13_185	1	1.00	0.514	1.08	0.0720	0.822	0.0770	1.08	0.53	0.246	0.124	0.745	0.381	
10/11/2013 14:02	0913-111	13.10.11.1402_13_945	1	1.42	0.493	1.05	0.0730	0.833	0.0800	1.08	0.53	0.246	0.122	0.862	0.368	
10/11/2013 14:03	0913-111	13.10.11.1403_14_706	1	1.36	0.505	1.03	0.0690	0.804	0.0790	1.08	0.53	0.246	0.122	0.745	0.377	
10/11/2013 14:04	0913-111	13.10.11.1404_15_456	1	1.18	0.464	1.18	0.0690	0.787	0.0810	1.08	0.54	0.246	0.124	0.869	0.384	
10/11/2013 14:05	0913-111	13.10.11.1405_16_186	1	1.00	0.489	1.11	0.0680	0.832	0.0810	1.08	0.54	0.246	0.121	0.745	0.368	
10/11/2013 14:06	0913-111	13.10.11.1406_16_946	1	1.11	0.527	1.01	0.0670	0.828	0.0800	1.08	0.54	0.246	0.124	0.765	0.390	
10/11/2013 14:07	0913-111	13.10.11.1407_17_746	1	1.00	0.486	1.11	0.0690	0.796	0.0810	1.08	0.53	0.246	0.121	0.917	0.367	
10/11/2013 14:08	0913-111	13.10.11.1408_18_506	1	1.28	0.461	1.10	0.0700	0.797	0.0790	1.08	0.53	0.246	0.122	0.875	0.365	
10/11/2013 14:09	0913-111	13.10.11.1409_19_206	1	1.00	0.486	1.06	0.0710	0.820	0.0790	1.08	0.54	0.246	0.123	0.745	0.384	
10/11/2013 14:10	0913-111	13.10.11.1410_20_016	1	1.06	0.496	1.05	0.0680	0.853	0.0790	1.08	0.53	0.246	0.122	1.05	0.377	
10/11/2013 14:11	0913-111	13.10.11.1411_20_696	1	1.24	0.504	1.04	0.0710	0.818	0.0790	1.08	0.53	0.246	0.125	1.25	0.376	
10/11/2013 14:12	0913-111	13.10.11.1412_21_506	1	1.11	0.489	1.10	0.0680	0.905	0.0770	1.08	0.53	0.246	0.123	1.06	0.363	
10/11/2013 14:13	0913-111	13.10.11.1413_22_276	1	1.23	0.469	1.06	0.0720	0.779	0.0790	1.08	0.54	0.246	0.121	0.959	0.367	
10/11/2013 14:14	0913-111	13.10.11.1414_22_977	1	1.14	0.476	1.17	0.0730	0.810	0.0810	1.08	0.54	0.246	0.123	0.745	0.361	
10/11/2013 14:15	0913-111	13.10.11.1415_23_697	1	1.13	0.488	0.926	0.0730	0.808	0.0800	1.08	0.54	0.246	0.125	0.745	0.367	
10/11/2013 14:16	0913-111	13.10.11.1416_24_517	1	1.50	0.503	1.06	0.0710	0.831	0.0830	1.08	0.54	0.246	0.122	0.947	0.370	
10/11/2013 14:17	0913-111	13.10.11.1417_25_267	1	1.00	0.504	1.14	0.0700	0.791	0.0790	1.08	0.54	0.246	0.127	0.875	0.371	
10/11/2013 14:18	0913-111	13.10.11.1418_25_967	1	1.27	0.514	1.07	0.0710	0.810	0.0810	1.08	0.54	0.246	0.125	0.840	0.380	
10/11/2013 14:19	0913-111	13.10.11.1419_26_687	1	1.72	0.503	1.07	0.0700	0.766	0.0810	1.08	0.54	0.246	0.125	0.745	0.371	
10/11/2013 14:20	0913-111	13.10.11.1420_27_457	1	1.45	0.468	1.11	0.0720	0.820	0.0820	1.08	0.54	0.246	0.125	1.13	0.350	
10/11/2013 14:21	0913-111	13.10.11.1421_28_207	1	1.09	0.495	1.04	0.0710	0.744	0.0800	1.08	0.54	0.246	0.124	0.745	0.363	
10/11/2013 14:22	0913-111	13.10.11.1422_29_967	1	1.40	0.499	1.06	0.0710	0.849	0.0840	1.08	0.54	0.246	0.125	0.745	0.369	
10/11/2013 14:23	0913-111	13.10.11.1423_29_697	1	1.80	0.513	1.12	0.0710	0.798	0.0820	1.08	0.54	0.246	0.125	0.905	0.382	
10/11/2013 14:24	0913-111	13.10.11.1424_30_467	1	1.46	0.492	1.11	0.0700	0.785	0.0820	1.08	0.54	0.246	0.124	0.928	0.369	
10/11/2013 14:25	0913-111	13.10.11.1425_31_177	1	1.00	0.488	1.09	0.0680	0.824	0.0830	1.08	0.54	0.246	0.124	0.901	0.361	
10/11/2013 14:26	0913-111	13.10.11.1426_31_988	1	1.62	0.517	1.12	0.0740	0.781	0.0820	1.08	0.54	0.246	0.129	0.946	0.380	
10/11/2013 14:27	0913-111	13.10.11.1427_32_727	1	1.00	0.462	1.07	0.0700	0.752	0.0810	1.08	0.54	0.246	0.124	0.745	0.369	
10/11/2013 14:28	0913-111	13.10.11.1428_33_468	1	1.94	0.493	1.07	0.0700	0.752	0.0810	1.08	0.54	0.246	0.128	0.745	0.366	
10/11/2013 14:29	0913-111	13.10.11.1429_34_178	1	1.00	0.513	1.00	0.0720	0.778	0.0840	1.08	0.54	0.246	0.127	0.745	0.380	
10/11/2013 14:30	0913-111	13.10.11.1430_35_028	1	1.00	0.518	0.998	0.0750	0.794	0.0830	1.08	0.54	0.246	0.129	0.996	0.380	
10/11/2013 14:31	0913-111	13.10.11.1431_35_798	1	1.56	0.489	1.04	0.0720	0.789	0.0840	1.08	0.54	0.246	0.126	0.745	0.376	
10/11/2013 14:32	0913-111	13.10.11.1432_36_488	1	1.19	0.506	1.04	0.0730	0.760	0.0820	1.08	0.54	0.246	0.128	0.745	0.379	
10/11/2013 14:33	0913-111	13.10.11.1433_37_208	1	1.00	0.487	1.06	0.0740	0.774	0.0830	1.08	0.54	0.246	0.127	0.760	0.368	
10/11/2013 14:34	0913-111	13.10.11.1434_37_918	1	1.06	0.496	1.14	0.0700	0.750	0.0830	1.08	0.54	0.246	0.126	0.784	0.374	
10/11/2013 14:35	0913-111	13.10.11.1435_38_748	1	1.00	0.467	1.06	0.0670	0.796	0.0840	1.08	0.55	0.246	0.122	0.745	0.349	
10/11/2013 14:36	0913-111	13.10.11.1436_39_468	1	1.00	0.463	0.969	0.0690	0.726	0.0840	1.08	0.55	0.246	0.124	0.960	0.360	
10/11/2013 14:37	0913-111	13.10.11.1437_40_168	1	1.85	0.508	1.00	0.0730	0.722	0.0850	1.08	0.55	0.246	0.128	0.745	0.374	
10/11/2013 14:38	0913-111	13.10.11.1438_40_969	1	1.55	0.494	0.950	0.0740	0.789	0.0840	1.08	0.55	0.246	0.128	0.784	0.374	
10/11/2013 14:39	0913-111	13.10.11.1439_41_669	1	1.00	0.513	1.05	0.0750	0.750	0.0860	1.08	0.55	0.246	0.131	0.745	0.379	
10/11/2013 14:40	0913-111	13.10.11.1440_42_369	1	1.56	0.487	1.12	0.0720	0.710	0.0890	1.08	0.55	0.246	0.126	0.745	0.362	
10/11/2013 14:41	0913-111	13.10.11.1441_43_159	1	1.17	0.522	1.12	0.0730	0.768	0.0860	1.08	0.55	0.246	0.125	0.745	0.386	
10/11/2013 14:42	0913-111	13.10.11.1442_43_779	1	1.00	0.517	0.993	0.0710	0.760	0.0860	1.08	0.55	0.246	0.127	0.745	0.381	
10/11/2013 14:43	0913-111	13.10.11.1443_44_609	1	1.44	0.475	0.993	0.0680	0.833	0.0580	1.08	0.39	0.246	0.153	0.745	0.359	
Average Conc. (ppm):				1	1.29	0.496	1.07	0.0711	0.797	0.0813	1.08	0.54	0.246	0.125	0.864	0.370

Pellet Cooler 2 Run 2

Date	Method	Filename	DF	Acroline (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/11/2013 15:08	0913-111	13.10.11.1508_02_515	1	1.00	0.480	0.460	0.0650	0.602	0.0840	1.08	0.55	0.246	0.115	1.06	0.354
10/11/2013 15:09	0913-111	13.10.11.1509_03_295	1												

Company | ACT  
 Analyst Initials | CUT  
 Parameters | EPA Method 320  
 # Samples | 21 Runs

Client # | 1911  
 Job # | 0913-111  
 PO # | 1314 1911  
 Report Date | V0.62 13.10.18.12.58

**Pellet Cooler 2 Run 3**

Date	Method	Filename	DF	Acroline (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/11/2013 16:29	0913-111	13.10.11.1629_02_222	1	1.41	0.500	1.27	0.0750	0.793	0.0840	1.08	0.55	0.246	0.125	0.989	0.379
10/11/2013 16:30	0913-111	13.10.11.1630_02_972	1	1.08	0.520	1.12	0.0740	0.741	0.0840	1.08	0.55	0.246	0.125	0.787	0.385
10/11/2013 16:31	0913-111	13.10.11.1631_03_632	1	1.13	0.505	0.925	0.0710	0.715	0.0850	1.08	0.55	0.246	0.119	1.25	0.372
10/11/2013 16:32	0913-111	13.10.11.1632_04_442	1	1.00	0.521	1.10	0.0720	0.688	0.0820	1.08	0.55	0.246	0.123	1.18	0.385
10/11/2013 16:33	0913-111	13.10.11.1633_05_202	1	1.11	0.507	1.07	0.0730	0.780	0.0840	1.08	0.55	0.246	0.118	0.745	0.384
10/11/2013 16:34	0913-111	13.10.11.1634_05_962	1	1.25	0.512	1.11	0.0690	0.837	0.0870	1.08	0.55	0.246	0.117	1.02	0.379
10/11/2013 16:35	0913-111	13.10.11.1635_06_772	1	1.27	0.525	1.12	0.0730	0.837	0.0880	1.08	0.55	0.246	0.125	0.991	0.388
10/11/2013 16:36	0913-111	13.10.11.1636_07_512	1	1.00	0.524	1.20	0.0760	0.931	0.0840	1.08	0.55	0.246	0.124	0.745	0.395
10/11/2013 16:37	0913-111	13.10.11.1637_08_223	1	1.00	0.528	1.19	0.0760	0.867	0.0880	1.08	0.55	0.246	0.127	0.745	0.393
10/11/2013 16:38	0913-111	13.10.11.1638_08_953	1	1.67	0.504	1.20	0.0780	0.906	0.0860	1.08	0.56	0.246	0.129	1.16	0.377
10/11/2013 16:39	0913-111	13.10.11.1639_09_743	1	1.00	0.532	1.28	0.0740	0.932	0.0870	1.08	0.56	0.246	0.125	0.745	0.390
10/11/2013 16:40	0913-111	13.10.11.1640_10_493	1	1.00	0.536	1.34	0.0770	0.956	0.0870	1.08	0.56	0.246	0.129	0.745	0.394
10/11/2013 16:41	0913-111	13.10.11.1641_11_243	1	1.10	0.505	1.31	0.0720	0.940	0.0880	1.08	0.56	0.246	0.122	0.745	0.372
10/11/2013 16:42	0913-111	13.10.11.1642_12_003	1	1.05	0.482	1.31	0.0690	0.921	0.0880	1.08	0.56	0.246	0.121	0.922	0.362
10/11/2013 16:43	0913-111	13.10.11.1643_12_743	1	1.49	0.519	1.42	0.0730	0.948	0.0870	1.08	0.56	0.246	0.129	0.746	0.387
10/11/2013 16:44	0913-111	13.10.11.1644_13_493	1	1.52	0.519	1.30	0.0740	0.951	0.0850	1.08	0.56	0.246	0.129	0.745	0.388
10/11/2013 16:45	0913-111	13.10.11.1645_14_293	1	2.25	0.539	3.47	0.0800	1.675	0.0870	1.49	0.57	1.49	0.443	0.745	0.403
10/11/2013 16:46	0913-111	13.10.11.1646_15_003	1	2.60	0.502	3.49	0.0810	1.271	0.0870	1.14	0.56	1.16	0.439	0.745	0.372
10/11/2013 16:47	0913-111	13.10.11.1647_15_783	1	2.07	0.525	2.98	0.0800	1.030	0.0880	1.08	0.56	0.670	0.136	0.745	0.390
10/11/2013 16:48	0913-111	13.10.11.1648_16_503	1	1.17	0.504	2.40	0.0760	0.875	0.0860	1.08	0.56	0.621	0.131	0.745	0.371
10/11/2013 16:49	0913-111	13.10.11.1649_17_254	1	1.44	0.509	2.21	0.0760	0.739	0.0830	1.08	0.55	0.485	0.129	0.745	0.378
10/11/2013 16:50	0913-111	13.10.11.1650_17_954	1	1.22	0.521	2.09	0.0720	0.746	0.0850	1.08	0.56	0.404	0.124	0.745	0.384
10/11/2013 16:51	0913-111	13.10.11.1651_18_704	1	1.05	0.503	2.16	0.0770	0.833	0.0860	1.08	0.56	0.347	0.126	0.745	0.379
10/11/2013 16:52	0913-111	13.10.11.1652_19_514	1	1.67	0.515	2.13	0.0750	0.842	0.0880	1.08	0.56	0.424	0.125	0.745	0.389
10/11/2013 16:53	0913-111	13.10.11.1653_20_254	1	1.18	0.528	2.14	0.0770	0.888	0.0860	1.08	0.56	0.259	0.129	0.745	0.385
10/11/2013 16:54	0913-111	13.10.11.1654_20_974	1	1.42	0.509	2.22	0.0760	0.753	0.0840	1.08	0.55	0.309	0.130	0.745	0.380
10/11/2013 16:55	0913-111	13.10.11.1655_21_734	1	1.00	0.521	2.23	0.0750	0.784	0.0880	1.08	0.56	0.338	0.127	0.745	0.390
10/11/2013 16:56	0913-111	13.10.11.1656_22_484	1	1.79	0.517	2.23	0.0730	0.820	0.0840	1.08	0.55	0.618	0.128	0.745	0.385
10/11/2013 16:57	0913-111	13.10.11.1657_23_244	1	1.00	0.521	2.01	0.0750	0.967	0.0830	1.08	0.55	0.447	0.127	0.745	0.382
10/11/2013 16:58	0913-111	13.10.11.1658_24_014	1	1.43	0.494	2.02	0.0720	0.753	0.0840	1.08	0.55	0.465	0.129	0.745	0.374
10/11/2013 16:59	0913-111	13.10.11.1659_24_714	1	1.44	0.527	2.01	0.0720	0.783	0.0840	1.08	0.55	0.434	0.127	0.745	0.388
10/11/2013 17:00	0913-111	13.10.11.1700_25_504	1	1.00	0.521	2.05	0.0760	0.806	0.0840	1.08	0.55	0.460	0.128	0.745	0.393
10/11/2013 17:01	0913-111	13.10.11.1701_26_275	1	1.46	0.530	1.98	0.0740	0.722	0.0830	1.08	0.55	0.463	0.125	0.745	0.392
10/11/2013 17:02	0913-111	13.10.11.1702_27_015	1	1.52	0.486	1.94	0.0690	0.790	0.0840	1.08	0.55	0.344	0.120	0.745	0.371
10/11/2013 17:03	0913-111	13.10.11.1703_27_725	1	1.80	0.524	1.91	0.0750	0.840	0.0840	1.08	0.55	0.268	0.125	0.745	0.375
10/11/2013 17:04	0913-111	13.10.11.1704_28_495	1	1.37	0.488	1.78	0.0730	0.737	0.0850	1.08	0.55	0.380	0.122	0.745	0.364
10/11/2013 17:05	0913-111	13.10.11.1705_29_235	1	1.64	0.497	1.88	0.0720	0.809	0.0820	1.08	0.55	0.246	0.121	0.745	0.369
10/11/2013 17:06	0913-111	13.10.11.1706_30_015	1	1.24	0.491	1.92	0.0710	0.776	0.0820	1.08	0.55	0.313	0.119	0.745	0.370
10/11/2013 17:07	0913-111	13.10.11.1707_30_725	1	1.00	0.504	1.92	0.0730	0.840	0.0840	1.08	0.55	0.323	0.119	0.745	0.375
10/11/2013 17:08	0913-111	13.10.11.1708_31_445	1	1.00	0.502	1.92	0.0710	0.728	0.0830	1.08	0.55	0.391	0.116	0.745	0.376
10/11/2013 17:09	0913-111	13.10.11.1709_32_195	1	1.23	0.512	1.90	0.0720	0.804	0.0800	1.08	0.55	0.386	0.122	0.745	0.381
10/11/2013 17:10	0913-111	13.10.11.1710_33_005	1	2.31	0.486	1.97	0.0720	0.773	0.0840	1.08	0.54	0.413	0.120	0.745	0.367
10/11/2013 17:11	0913-111	13.10.11.1711_33_755	1	1.00	0.506	1.88	0.0710	0.831	0.0820	1.08	0.55	0.424	0.119	0.745	0.376
10/11/2013 17:12	0913-111	13.10.11.1712_34_507	1	1.00	0.505	1.80	0.0780	0.784	0.0840	1.08	0.55	0.378	0.120	0.745	0.382
10/11/2013 17:13	0913-111	13.10.11.1713_35_276	1	1.00	0.500	2.00	0.0710	0.907	0.0810	1.08	0.55	0.293	0.123	0.745	0.379
10/11/2013 17:14	0913-111	13.10.11.1714_35_986	1	1.38	0.473	1.83	0.0720	0.748	0.0850	1.08	0.55	0.246	0.121	0.745	0.353
10/11/2013 17:15	0913-111	13.10.11.1715_36_786	1	1.31	0.511	1.91	0.0710	0.731	0.0840	1.08	0.55	0.343	0.121	0.745	0.374
10/11/2013 17:16	0913-111	13.10.11.1716_37_536	1	1.56	0.489	1.88	0.0690	0.776	0.0840	1.08	0.55	0.246	0.122	0.745	0.359
10/11/2013 17:17	0913-111	13.10.11.1717_38_286	1	1.29	0.469	1.87	0.0680	0.840	0.0850	1.08	0.55	0.323	0.121	0.745	0.349
10/11/2013 17:18	0913-111	13.10.11.1718_38_976	1	1.51	0.474	1.78	0.0710	0.800	0.0820	1.08	0.55	0.246	0.123	0.745	0.351
10/11/2013 17:19	0913-111	13.10.11.1719_39_786	1	1.22	0.511	1.79	0.0700	0.870	0.0840	1.08	0.55	0.285	0.120	0.745	0.369
10/11/2013 17:20	0913-111	13.10.11.1720_40_566	1	1.17	0.487	1.92	0.0710	0.727	0.0820	1.08	0.55	0.291	0.120	0.745	0.378
10/11/2013 17:21	0913-111	13.10.11.1721_41_276	1	1.00	0.507	1.97	0.0690	0.785	0.0820	1.08	0.55	0.257	0.119	0.745	0.379
10/11/2013 17:22	0913-111	13.10.11.1722_41_986	1	1.00	0.519	1.95	0.0720	0.778	0.0810	1.08	0.54	0.246	0.127	0.745	0.381
10/11/2013 17:23	0913-111	13.10.11.1723_42_806	1	1.00	0.487	1.85	0.0710	0.879	0.0840	1.08	0.54	0.326	0.122	0.745	0.367
10/11/2013 17:24	0913-111	13.10.11.1724_43_527	1	1.00	0.492	1.96	0.0720	0.858	0.0840	1.08	0.55	0.246	0.123	0.745	0.367
10/11/2013 17:25	0913-111	13.10.11.1725_44_287	1	1.00	0.503	1.93	0.0690	0.840	0.0840	1.08	0.55	0.403	0.123	0.745	0.376
10/11/2013 17:26	0913-111	13.10.11.1726_44_997	1	2.21	0.497	2.04	0.0710	0.849	0.0830	1.08	0.55	0.283	0.124	0.745	0.375
10/11/2013 17:27	0913-111	13.10.11.1727_45_747	1	1.92	0.492	1.89	0.0720	0.869	0.0830	1.08	0.55	0.246	0.121	0.745	0.367
10/11/2013 17:28	0913-111	13.10.11.1728_46_477	1	1.20	0.490	1.80	0.0750	0.814	0.0820	1.08	0.55	0.246	0.122	0.745	0.367
10/11/2013 17:29	0913-111	13.10.11.1729_47_307	1	1.25	0.504	1.95	0.0720	0.843	0.0820	1.08	0.55	0.302	0.124	0.745	0.380
Average Conc. (ppm):			1	1.33	0.507	1.84	0.0732	0.844	0.0844	1.09	0.55	0.359	0.124	0.786	0.378

**Hammermill 2 Run 1**

Date	Method	Filename	DF	Acroline (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/11/2013 18:10	0913-111	13.10.11													

Company: ACT  
 Analyst Initials: CTT  
 Parameters: EPA Method 320  
 # Samples: 21  
 Runs: 21

Client # 1911  
 Job # 0913-111  
 PO # 1134 1911  
 Report Date: V0.62 13.10.18.12.58

**Hammermill 2 Run 2**

Date	Method	Filename	DF	Acroetin (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/11/2013 19:35	0913-111	13_10_11_1935_01_714	1	1.03	0.455	0.387	0.0660	0.165	0.0760	1.08	0.52	0.232	0.107	0.707	0.335	
10/11/2013 19:36	0913-111	13_10_11_1936_02_534	1	0.965	0.465	0.476	0.0620	0.184	0.0770	1.08	0.52	0.232	0.104	0.707	0.343	
10/11/2013 19:37	0913-111	13_10_11_1937_03_234	1	0.965	0.466	0.584	0.0660	0.165	0.0770	1.08	0.52	0.232	0.107	0.707	0.343	
10/11/2013 19:38	0913-111	13_10_11_1938_03_964	1	0.965	0.470	0.688	0.0660	0.165	0.0800	1.08	0.53	0.232	0.110	0.707	0.348	
10/11/2013 19:39	0913-111	13_10_11_1939_04_744	1	0.965	0.468	0.608	0.0660	0.165	0.0810	1.08	0.53	0.232	0.108	0.731	0.346	
10/11/2013 19:40	0913-111	13_10_11_1940_05_514	1	0.965	0.483	0.569	0.0660	0.203	0.0800	1.08	0.54	0.232	0.109	0.707	0.360	
10/11/2013 19:41	0913-111	13_10_11_1941_06_114	1	0.965	0.470	0.705	0.0620	0.168	0.0850	1.08	0.55	0.232	0.105	0.707	0.343	
10/11/2013 19:42	0913-111	13_10_11_1942_06_924	1	0.965	0.504	0.659	0.0670	0.169	0.0830	1.08	0.55	0.232	0.114	0.707	0.369	
10/11/2013 19:43	0913-111	13_10_11_1943_07_674	1	0.965	0.502	0.739	0.0700	0.180	0.0860	1.08	0.55	0.232	0.117	0.707	0.369	
10/11/2013 19:44	0913-111	13_10_11_1944_08_385	1	0.965	0.467	0.816	0.0680	0.184	0.0850	1.08	0.55	0.232	0.114	0.707	0.355	
10/11/2013 19:45	0913-111	13_10_11_1945_09_195	1	0.965	0.496	0.955	0.0730	0.189	0.0880	1.08	0.56	0.232	0.123	0.707	0.366	
10/11/2013 19:46	0913-111	13_10_11_1946_09_915	1	0.965	0.512	1.22	0.0740	0.179	0.0880	1.08	0.57	0.232	0.127	0.707	0.375	
10/11/2013 19:47	0913-111	13_10_11_1947_10_665	1	0.965	0.505	1.29	0.0720	0.175	0.0860	1.08	0.56	0.232	0.122	0.707	0.372	
10/11/2013 19:48	0913-111	13_10_11_1948_11_485	1	0.965	0.487	1.11	0.0670	0.165	0.0830	1.08	0.55	0.232	0.113	0.707	0.357	
10/11/2013 19:49	0913-111	13_10_11_1949_12_195	1	0.965	0.492	1.06	0.0700	0.165	0.0840	1.08	0.55	0.292	0.114	0.707	0.359	
10/11/2013 19:51	0913-111	13_10_11_1951_13_755	1	0.965	0.462	1.17	0.0650	0.165	0.0830	1.08	0.55	0.271	0.106	0.707	0.339	
10/11/2013 19:52	0913-111	13_10_11_1952_14_475	1	0.965	0.501	1.09	0.0680	0.165	0.0840	1.08	0.55	0.232	0.114	0.707	0.363	
10/11/2013 19:53	0913-111	13_10_11_1953_15_195	1	0.965	0.453	0.918	0.0660	0.165	0.0820	1.08	0.55	0.238	0.109	0.707	0.338	
10/11/2013 19:54	0913-111	13_10_11_1954_16_015	1	1.16	0.466	0.745	0.0620	0.165	0.0840	1.08	0.55	0.236	0.110	0.707	0.342	
10/11/2013 19:55	0913-111	13_10_11_1955_16_735	1	0.965	0.464	0.645	0.0670	0.186	0.0830	1.08	0.56	0.232	0.109	0.707	0.364	
10/11/2013 19:56	0913-111	13_10_11_1956_17_546	1	0.965	0.477	0.739	0.0700	0.167	0.0870	1.08	0.55	0.232	0.114	0.707	0.351	
10/11/2013 19:57	0913-111	13_10_11_1957_18_266	1	0.965	0.484	0.834	0.0700	0.165	0.0830	1.08	0.55	0.232	0.114	0.707	0.355	
10/11/2013 19:58	0913-111	13_10_11_1958_18_986	1	0.965	0.497	0.781	0.0660	0.197	0.0890	1.08	0.56	0.303	0.114	0.707	0.361	
10/11/2013 19:59	0913-111	13_10_11_1959_19_796	1	0.965	0.465	0.968	0.0700	0.165	0.0870	1.08	0.56	0.232	0.116	0.707	0.364	
10/11/2013 20:00	0913-111	13_10_11_2000_20_526	1	0.965	0.485	1.18	0.0670	0.165	0.0840	1.08	0.55	0.232	0.115	0.707	0.355	
10/11/2013 20:01	0913-111	13_10_11_2001_21_306	1	0.965	0.486	0.996	0.0660	0.282	0.0820	1.08	0.55	0.232	0.114	0.707	0.365	
10/11/2013 20:02	0913-111	13_10_11_2002_22_056	1	0.965	0.470	1.20	0.0710	0.297	0.0770	1.08	0.56	0.232	0.117	0.707	0.366	
10/11/2013 20:03	0913-111	13_10_11_2003_22_766	1	0.965	0.503	1.15	0.0730	0.266	0.0870	1.08	0.56	0.232	0.120	0.707	0.362	
10/11/2013 20:04	0913-111	13_10_11_2004_23_566	1	0.965	0.490	1.52	0.0720	0.287	0.0860	1.08	0.56	0.232	0.120	0.707	0.362	
10/11/2013 20:05	0913-111	13_10_11_2005_24_316	1	0.965	0.499	1.31	0.0720	0.247	0.0900	1.08	0.56	0.232	0.121	0.707	0.366	
10/11/2013 20:06	0913-111	13_10_11_2006_25_026	1	0.965	0.479	1.24	0.0670	0.289	0.0850	1.08	0.55	0.232	0.116	0.707	0.351	
10/11/2013 20:07	0913-111	13_10_11_2007_25_847	1	0.965	0.471	1.50	0.0680	0.281	0.0840	1.08	0.55	0.290	0.113	0.707	0.340	
10/11/2013 20:08	0913-111	13_10_11_2008_26_547	1	1.29	0.496	0.966	0.0710	0.381	0.0840	1.08	0.55	0.232	0.121	0.707	0.363	
10/11/2013 20:09	0913-111	13_10_11_2009_27_297	1	0.965	0.485	0.779	0.0680	0.323	0.0890	1.08	0.56	0.232	0.117	0.707	0.355	
10/11/2013 20:10	0913-111	13_10_11_2010_28_067	1	0.965	0.515	2.01	0.0720	0.308	0.0860	1.08	0.56	0.232	0.127	0.846	0.373	
10/11/2013 20:11	0913-111	13_10_11_2011_28_787	1	0.965	0.467	2.07	0.0680	0.318	0.0880	1.08	0.55	0.383	0.118	0.707	0.342	
10/11/2013 20:12	0913-111	13_10_11_2012_29_547	1	0.965	0.517	1.95	0.0710	0.254	0.0860	1.08	0.55	0.371	0.121	0.707	0.378	
10/11/2013 20:13	0913-111	13_10_11_2013_30_317	1	0.965	0.479	1.47	0.0700	0.287	0.0860	1.08	0.55	0.274	0.119	0.707	0.352	
10/11/2013 20:14	0913-111	13_10_11_2014_31_027	1	0.965	0.486	1.48	0.0700	0.165	0.0830	1.08	0.55	0.341	0.117	0.707	0.352	
10/11/2013 20:15	0913-111	13_10_11_2015_31_827	1	0.965	0.502	1.42	0.0710	0.200	0.0840	1.08	0.55	0.232	0.117	0.707	0.366	
10/11/2013 20:16	0913-111	13_10_11_2016_32_537	1	0.965	0.474	1.60	0.0660	0.218	0.0860	1.08	0.55	0.232	0.115	0.707	0.349	
10/11/2013 20:17	0913-111	13_10_11_2017_33_257	1	0.965	0.473	1.84	0.0690	0.244	0.0860	1.08	0.56	0.232	0.120	0.707	0.345	
10/11/2013 20:18	0913-111	13_10_11_2018_34_028	1	0.965	0.481	1.79	0.0720	0.283	0.0860	1.08	0.55	0.232	0.118	0.707	0.353	
10/11/2013 20:19	0913-111	13_10_11_2019_34_828	1	0.965	0.441	1.32	0.0570	0.231	0.0810	1.08	0.54	0.232	0.103	0.707	0.319	
10/11/2013 20:20	0913-111	13_10_11_2020_35_678	1	0.965	0.409	0.893	0.0620	0.237	0.0790	1.08	0.53	0.232	0.100	0.707	0.303	
10/11/2013 20:21	0913-111	13_10_11_2021_36_418	1	0.965	0.433	0.987	0.0620	0.202	0.0750	1.08	0.53	0.232	0.103	0.707	0.318	
10/11/2013 20:22	0913-111	13_10_11_2022_37_128	1	0.965	0.461	1.19	0.0620	0.237	0.0830	1.08	0.54	0.232	0.114	0.707	0.338	
10/11/2013 20:23	0913-111	13_10_11_2023_37_728	1	0.965	0.479	1.36	0.0660	0.198	0.0870	1.08	0.56	0.232	0.119	0.707	0.351	
10/11/2013 20:24	0913-111	13_10_11_2024_38_578	1	0.965	0.483	1.45	0.0680	0.184	0.0860	1.08	0.56	0.232	0.124	0.707	0.352	
10/11/2013 20:25	0913-111	13_10_11_2025_39_308	1	0.965	0.491	1.36	0.0700	0.239	0.0850	1.08	0.56	0.232	0.121	0.707	0.361	
10/11/2013 20:26	0913-111	13_10_11_2026_40_038	1	0.965	0.466	1.27	0.0680	0.182	0.0850	1.08	0.56	0.232	0.116	0.707	0.340	
10/11/2013 20:27	0913-111	13_10_11_2027_40_768	1	0.965	0.584	1.15	0.0670	0.191	0.0860	1.08	0.55	0.232	0.115	0.707	0.356	
10/11/2013 20:28	0913-111	13_10_11_2028_41_548	1	0.965	0.493	1.23	0.0660	0.243	0.0850	1.08	0.55	0.232	0.114	0.707	0.359	
10/11/2013 20:29	0913-111	13_10_11_2029_42_348	1	0.965	0.477	0.973	0.0670	0.171	0.0860	1.08	0.55	0.232	0.113	0.707	0.350	
10/11/2013 20:30	0913-111	13_10_11_2030_43_068	1	0.965	0.474	0.997	0.0660	0.165	0.0850	1.08	0.55	0.232	0.111	0.707	0.344	
10/11/2013 20:31	0913-111	13_10_11_2031_43_818	1	0.965	0.465	0.840	0.0660	0.185	0.0840	1.08	0.55	0.232	0.114	0.707	0.345	
10/11/2013 20:32	0913-111	13_10_11_2032_44_619	1	0.965	0.493	1.57	0.0710	0.253	0.0850	1.08	0.56	0.232	0.122	0.707	0.360	
10/11/2013 20:33	0913-111	13_10_11_2033_45_359	1	0.965	0.463	1.44	0.0670	0.165	0.0840	1.08	0.55	0.232	0.111	0.707	0.342	
10/11/2013 20:34	0913-111	13_10_11_2034_46_079	1	0.965	0.450	0.598	0.0670	0.165	0.0680	1.08	0.46	0.232	0.112	0.707	0.331	
10/11/2013 20:35	0913-111	13_10_11_2035_46_799	1	0.965	0.515	0.136	0.100	0.165	0.0420	1.08	0.128	0.232	0.504	0.707	0.391	
Average Conc. (ppm):				1	0.975	0.480	1.14	0.0682	0.211	0.0832	1.08	0.54	0.243	0.122	0.710	0.352

**Hammermill 2 Run 3**

Date	Method	Filename	DF	Acroetin (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/11/2013 20:48	0913-111	13_10_11_2048_56_780	1	0.965	0.501	0.733	0.0690	0.224	0.0890						

Company ACT  
 Analyst Initials CWT  
 Parameters EPA Method 320  
 # Samples 21  
 Runs

Client # 1911  
 Job # 0913-111  
 PO # 3134 1911  
 Report Date V0.62 13.10.18.12.58

Pellet Cooler 1 Run 1

Date	Method	Filename	DF	AcroIn (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/12/2013 8:58	0913-111	13_10_12_0858_54_250	1	0.931	0.473	1.38	0.0630	0.373	0.0710	0.98	0.49	0.236	0.114	0.686	0.343	
10/12/2013 8:59	0913-111	13_10_12_0859_55_060	1	0.931	0.451	1.43	0.0630	0.416	0.0730	0.98	0.49	0.297	0.113	0.686	0.332	
10/12/2013 9:00	0913-111	13_10_12_0900_55_760	1	0.931	0.473	1.46	0.0650	0.440	0.0700	0.98	0.49	0.291	0.120	0.686	0.353	
10/12/2013 9:01	0913-111	13_10_12_0901_56_540	1	0.931	0.443	1.56	0.0630	0.413	0.0710	0.98	0.49	0.337	0.114	0.686	0.327	
10/12/2013 9:02	0913-111	13_10_12_0902_57_240	1	1.05	0.458	1.42	0.0670	0.487	0.0710	0.98	0.49	0.293	0.115	0.686	0.344	
10/12/2013 9:03	0913-111	13_10_12_0903_58_000	1	0.931	0.447	1.38	0.0610	0.431	0.0700	0.98	0.49	0.236	0.109	0.686	0.328	
10/12/2013 9:04	0913-111	13_10_12_0904_58_810	1	0.931	0.487	1.32	0.0660	0.495	0.0740	0.98	0.49	0.337	0.116	0.686	0.352	
10/12/2013 9:05	0913-111	13_10_12_0905_59_520	1	1.20	0.480	1.26	0.0650	0.456	0.0700	0.98	0.49	0.236	0.116	0.686	0.351	
10/12/2013 9:07	0913-111	13_10_12_0907_00_280	1	0.931	0.462	1.41	0.0670	0.543	0.0710	0.98	0.49	0.236	0.119	0.686	0.339	
10/12/2013 9:08	0913-111	13_10_12_0908_01_061	1	0.931	0.477	1.50	0.0680	0.496	0.0700	0.98	0.50	0.340	0.116	0.686	0.350	
10/12/2013 9:09	0913-111	13_10_12_0909_01_771	1	0.931	0.449	1.53	0.0590	0.483	0.0700	0.98	0.50	0.373	0.112	0.686	0.332	
10/12/2013 9:10	0913-111	13_10_12_0910_02_601	1	0.931	0.449	1.50	0.0610	0.450	0.0720	0.98	0.50	0.236	0.114	0.686	0.330	
10/12/2013 9:11	0913-111	13_10_12_0911_03_351	1	0.931	0.460	1.49	0.0630	0.502	0.0740	0.98	0.50	0.236	0.111	0.686	0.335	
10/12/2013 9:12	0913-111	13_10_12_0912_04_061	1	0.931	0.461	1.45	0.0640	0.553	0.0740	0.98	0.50	0.236	0.115	0.686	0.337	
10/12/2013 9:13	0913-111	13_10_12_0913_04_821	1	0.931	0.456	1.51	0.0650	0.543	0.0740	0.98	0.50	0.344	0.115	0.686	0.338	
10/12/2013 9:14	0913-111	13_10_12_0914_05_631	1	1.19	0.466	1.48	0.0630	0.513	0.0750	0.98	0.50	0.306	0.115	0.686	0.344	
10/12/2013 9:15	0913-111	13_10_12_0915_06_381	1	0.931	0.477	1.43	0.0640	0.522	0.0720	0.98	0.50	0.442	0.115	0.686	0.353	
10/12/2013 9:16	0913-111	13_10_12_0916_06_991	1	0.931	0.459	1.47	0.0640	0.464	0.0710	0.98	0.50	0.425	0.114	0.686	0.337	
10/12/2013 9:17	0913-111	13_10_12_0917_07_721	1	0.931	0.443	1.52	0.0700	0.624	0.0720	0.98	0.50	0.242	0.122	0.686	0.322	
10/12/2013 9:18	0913-111	13_10_12_0918_08_531	1	0.931	0.470	1.47	0.0660	0.615	0.0720	0.98	0.51	0.257	0.117	0.686	0.345	
10/12/2013 9:19	0913-111	13_10_12_0919_09_292	1	0.931	0.465	1.69	0.0640	0.591	0.0740	0.98	0.51	0.527	0.119	0.686	0.352	
10/12/2013 9:20	0913-111	13_10_12_0920_09_962	1	0.931	0.473	1.50	0.0650	0.545	0.0740	0.98	0.51	0.342	0.122	0.686	0.343	
10/12/2013 9:21	0913-111	13_10_12_0921_10_712	1	0.931	0.490	1.63	0.0620	0.634	0.0770	0.98	0.51	0.497	0.117	0.686	0.354	
10/12/2013 9:22	0913-111	13_10_12_0922_11_562	1	0.931	0.487	1.54	0.0700	0.574	0.0750	0.98	0.51	0.356	0.123	0.686	0.368	
10/12/2013 9:23	0913-111	13_10_12_0923_12_282	1	0.931	0.461	1.52	0.0610	0.620	0.0750	0.98	0.51	0.525	0.114	0.686	0.340	
10/12/2013 9:24	0913-111	13_10_12_0924_13_092	1	1.31	0.472	1.51	0.0640	0.620	0.0730	0.98	0.51	0.620	0.124	0.686	0.344	
10/12/2013 9:25	0913-111	13_10_12_0925_13_802	1	0.931	0.471	1.50	0.0700	0.601	0.0760	0.98	0.51	0.292	0.118	0.938	0.348	
10/12/2013 9:26	0913-111	13_10_12_0926_14_512	1	1.14	0.468	1.44	0.0680	0.691	0.0760	0.98	0.51	0.291	0.121	0.686	0.340	
10/12/2013 9:27	0913-111	13_10_12_0927_15_282	1	0.931	0.471	1.41	0.0640	0.516	0.0740	0.98	0.51	0.320	0.113	0.686	0.345	
10/12/2013 9:28	0913-111	13_10_12_0928_16_092	1	0.931	0.465	1.51	0.0630	0.549	0.0750	0.98	0.51	0.356	0.117	0.686	0.352	
10/12/2013 9:29	0913-111	13_10_12_0929_16_802	1	0.931	0.486	1.43	0.0660	0.505	0.0760	0.98	0.51	0.391	0.117	0.686	0.353	
10/12/2013 9:30	0913-111	13_10_12_0930_17_552	1	0.931	0.475	1.50	0.0670	0.505	0.0750	0.98	0.51	0.236	0.122	0.686	0.355	
10/12/2013 9:31	0913-111	13_10_12_0931_18_263	1	0.931	0.487	1.54	0.0660	0.600	0.0740	0.98	0.51	0.412	0.124	0.686	0.358	
10/12/2013 9:32	0913-111	13_10_12_0932_19_013	1	0.931	0.471	1.39	0.0660	0.511	0.0750	0.98	0.51	0.358	0.124	0.686	0.351	
10/12/2013 9:33	0913-111	13_10_12_0933_19_773	1	0.931	0.483	1.61	0.0650	0.620	0.0760	0.98	0.51	0.350	0.124	0.686	0.350	
10/12/2013 9:34	0913-111	13_10_12_0934_20_553	1	0.931	0.465	1.61	0.0660	0.585	0.0770	0.98	0.52	0.476	0.123	0.686	0.340	
10/12/2013 9:35	0913-111	13_10_12_0935_21_313	1	1.44	0.491	1.53	0.0690	0.690	0.0760	0.98	0.52	0.475	0.131	0.686	0.358	
10/12/2013 9:36	0913-111	13_10_12_0936_22_033	1	1.06	0.466	1.49	0.0620	0.596	0.0800	0.98	0.51	0.642	0.122	0.686	0.342	
10/12/2013 9:37	0913-111	13_10_12_0937_22_823	1	0.931	0.481	1.42	0.0670	0.567	0.0760	0.98	0.51	0.370	0.121	0.686	0.352	
10/12/2013 9:38	0913-111	13_10_12_0938_23_533	1	0.931	0.478	1.39	0.0630	0.543	0.0780	0.99	0.51	0.519	0.118	0.686	0.346	
10/12/2013 9:39	0913-111	13_10_12_0939_24_263	1	0.931	0.469	1.38	0.0640	0.609	0.0770	1.02	0.51	0.450	0.115	0.686	0.348	
10/12/2013 9:40	0913-111	13_10_12_0940_25_023	1	1.13	0.476	1.39	0.0620	0.507	0.0740	1.03	0.51	0.558	0.118	0.686	0.346	
10/12/2013 9:41	0913-111	13_10_12_0941_25_743	1	0.931	0.468	1.27	0.0630	0.612	0.0720	0.98	0.51	0.236	0.114	0.686	0.344	
10/12/2013 9:42	0913-111	13_10_12_0942_26_523	1	0.931	0.482	1.32	0.0640	0.516	0.0730	0.98	0.51	0.351	0.118	0.686	0.351	
10/12/2013 9:43	0913-111	13_10_12_0943_27_234	1	0.931	0.448	1.37	0.0660	0.502	0.0720	1.00	0.50	0.439	0.114	0.686	0.328	
10/12/2013 9:44	0913-111	13_10_12_0944_27_984	1	0.931	0.464	1.48	0.0660	0.512	0.0740	0.98	0.51	0.486	0.118	0.686	0.343	
10/12/2013 9:45	0913-111	13_10_12_0945_28_744	1	0.931	0.428	1.37	0.0610	0.502	0.0740	0.99	0.50	0.423	0.110	0.686	0.324	
10/12/2013 9:46	0913-111	13_10_12_0946_29_534	1	0.931	0.467	1.30	0.0680	0.516	0.0760	1.01	0.51	0.352	0.121	0.686	0.358	
10/12/2013 9:47	0913-111	13_10_12_0947_30_304	1	0.931	0.472	1.32	0.0640	0.497	0.0750	1.05	0.51	0.241	0.116	0.686	0.344	
10/12/2013 9:48	0913-111	13_10_12_0948_30_974	1	1.12	0.487	1.27	0.0610	0.527	0.0750	1.03	0.51	0.405	0.117	0.686	0.359	
10/12/2013 9:49	0913-111	13_10_12_0949_31_774	1	1.09	0.461	1.47	0.0600	0.528	0.0730	1.08	0.51	0.525	0.113	0.686	0.335	
10/12/2013 9:50	0913-111	13_10_12_0950_32_484	1	0.931	0.453	1.26	0.0650	0.505	0.0750	1.06	0.51	0.348	0.117	0.686	0.329	
10/12/2013 9:51	0913-111	13_10_12_0951_33_294	1	0.931	0.471	1.34	0.0680	0.571	0.0760	1.09	0.51	0.369	0.117	0.704	0.351	
10/12/2013 9:52	0913-111	13_10_12_0952_34_074	1	1.20	0.470	1.30	0.0610	0.563	0.0730	1.09	0.51	0.402	0.120	0.686	0.346	
10/12/2013 9:53	0913-111	13_10_12_0953_34_794	1	0.931	0.463	1.37	0.0630	0.527	0.0740	1.02	0.51	0.565	0.118	0.686	0.343	
10/12/2013 9:54	0913-111	13_10_12_0954_35_514	1	0.931	0.477	1.37	0.0690	0.563	0.0720	1.03	0.51	0.236	0.123	0.686	0.352	
10/12/2013 9:55	0913-111	13_10_12_0955_36_294	1	0.931	0.459	1.41	0.0630	0.533	0.0730	1.07	0.51	0.465	0.125	0.686	0.337	
10/12/2013 9:56	0913-111	13_10_12_0956_36_955	1	0.931	0.446	1.33	0.0620	0.538	0.0760	1.09	0.51	0.573	0.121	0.686	0.328	
10/12/2013 9:57	0913-111	13_10_12_0957_37_745	1	0.931	0.464	1.46	0.0640	0.523	0.0750	1.08	0.51	0.516	0.119	0.686	0.345	
10/12/2013 9:58	0913-111	13_10_12_0958_38_355	1	0.931	0.450	1.36	0.0650	0.534	0.0750	1.10	0.51	0.448	0.121	0.686	0.330	
Average Conc. (ppm):				1	0.976	0.467	1.44	0.0646	0.537	0.0738	1.00	0.50	0.381	0.118	0.691	0.344

Pellet Cooler 1 Run 2

Date	Method	Filename	DF	AcroIn (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/12/2013 10:22	0913-111	13_10_12_1022_56_297	1	0.931	0.480	1.36	0.0680	0.307	0.0760	0.98	0.51	0.236	0.126	0.686	0.354
10/12/2013 10:23	0913-111	13_10_12_1023_57													

Company: ACT  
 Analyst Initials: CWT  
 Parameters: EPA Method 320  
 # Samples: 21  
 # Runs: 21

Client # 1911  
 Job # 0913-111  
 PO # 3134 1911  
 Report Date: V0.62 13.10.18.12.58

**Pellet Cooler 1 Run 3**

Date	Method	Filename	DF	Acroline (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/12/2013 11:41	0913-111	13_10_12_1141_54_484	1	0.967	0.465	1.43	0.0640	0.316	0.0690	0.98	0.48	0.236	0.118	0.686	0.340
10/12/2013 11:42	0913-111	13_10_12_1142_55_194	1	0.931	0.471	1.18	0.0630	0.282	0.0710	0.98	0.48	0.236	0.114	0.905	0.345
10/12/2013 11:43	0913-111	13_10_12_1143_55_574	1	1.57	0.480	1.15	0.0600	0.327	0.0680	0.98	0.47	0.236	0.119	0.844	0.354
10/12/2013 11:44	0913-111	13_10_12_1144_56_674	1	1.69	0.446	1.19	0.0670	0.311	0.0700	0.98	0.48	0.236	0.120	0.686	0.337
10/12/2013 11:45	0913-111	13_10_12_1145_57_474	1	1.18	0.455	1.29	0.0630	0.402	0.0710	0.98	0.48	0.236	0.117	0.686	0.337
10/12/2013 11:46	0913-111	13_10_12_1146_58_174	1	1.31	0.467	1.15	0.0650	0.472	0.0720	0.98	0.48	0.236	0.119	0.686	0.348
10/12/2013 11:47	0913-111	13_10_12_1147_58_354	1	1.52	0.453	1.23	0.0630	0.368	0.0690	0.98	0.48	0.236	0.119	0.686	0.336
10/12/2013 11:48	0913-111	13_10_12_1148_59_814	1	1.10	0.447	1.38	0.0650	0.333	0.0710	0.98	0.48	0.236	0.118	0.686	0.333
10/12/2013 11:50	0913-111	13_10_12_1150_00_524	1	1.41	0.478	1.43	0.0620	0.400	0.0690	0.98	0.48	0.236	0.121	1.13	0.351
10/12/2013 11:51	0913-111	13_10_12_1151_01_374	1	1.64	0.467	1.33	0.0670	0.385	0.0670	0.98	0.48	0.236	0.118	0.686	0.347
10/12/2013 11:52	0913-111	13_10_12_1152_02_144	1	1.21	0.466	1.35	0.0650	0.361	0.0680	0.98	0.48	0.236	0.119	0.686	0.344
10/12/2013 11:53	0913-111	13_10_12_1153_03_904	1	1.13	0.475	1.40	0.0680	0.294	0.0700	0.98	0.48	0.236	0.127	0.686	0.353
10/12/2013 11:54	0913-111	13_10_12_1154_03_615	1	1.22	0.476	1.53	0.0680	0.449	0.0710	0.98	0.49	0.236	0.129	0.978	0.348
10/12/2013 11:55	0913-111	13_10_12_1155_04_415	1	1.43	0.472	1.51	0.0690	0.366	0.0730	0.98	0.48	0.236	0.126	0.686	0.341
10/12/2013 11:56	0913-111	13_10_12_1156_05_115	1	1.14	0.462	1.36	0.0670	0.419	0.0700	0.98	0.48	0.236	0.122	0.686	0.345
10/12/2013 11:57	0913-111	13_10_12_1157_05_325	1	0.932	0.444	1.41	0.0650	0.344	0.0700	0.98	0.48	0.236	0.119	0.686	0.330
10/12/2013 11:58	0913-111	13_10_12_1158_06_635	1	1.06	0.481	1.36	0.0620	0.274	0.0680	0.98	0.48	0.236	0.123	0.898	0.351
10/12/2013 11:59	0913-111	13_10_12_1159_07_345	1	0.931	0.461	1.32	0.0650	0.336	0.0690	0.98	0.48	0.236	0.126	0.857	0.343
10/12/2013 12:00	0913-111	13_10_12_1200_08_135	1	2.15	0.484	1.38	0.0680	0.316	0.0680	0.98	0.48	0.236	0.124	0.686	0.358
10/12/2013 12:01	0913-111	13_10_12_1201_08_905	1	1.29	0.452	1.45	0.0640	0.327	0.0730	0.98	0.48	0.236	0.118	0.686	0.335
10/12/2013 12:02	0913-111	13_10_12_1202_09_625	1	1.70	0.444	1.33	0.0670	0.304	0.0690	0.98	0.48	0.236	0.117	0.686	0.327
10/12/2013 12:03	0913-111	13_10_12_1203_10_385	1	1.24	0.434	1.22	0.0600	0.353	0.0680	0.98	0.48	0.236	0.114	0.686	0.323
10/12/2013 12:04	0913-111	13_10_12_1204_11_135	1	0.931	0.458	1.37	0.0650	0.304	0.0700	0.98	0.48	0.236	0.117	0.709	0.335
10/12/2013 12:05	0913-111	13_10_12_1205_11_785	1	2.02	0.471	1.33	0.0650	0.375	0.0710	0.98	0.48	0.236	0.123	1.10	0.345
10/12/2013 12:06	0913-111	13_10_12_1206_12_506	1	1.21	0.456	1.30	0.0620	0.389	0.0690	0.98	0.48	0.236	0.114	0.686	0.321
10/12/2013 12:07	0913-111	13_10_12_1207_13_246	1	0.931	0.485	1.44	0.0650	0.369	0.0680	0.98	0.48	0.236	0.118	0.686	0.346
10/12/2013 12:08	0913-111	13_10_12_1208_13_996	1	0.969	0.470	1.26	0.0600	0.316	0.0680	0.98	0.48	0.236	0.118	0.686	0.343
10/12/2013 12:09	0913-111	13_10_12_1209_14_786	1	1.21	0.447	1.21	0.0570	0.308	0.0680	0.98	0.48	0.236	0.114	0.780	0.331
10/12/2013 12:10	0913-111	13_10_12_1210_15_476	1	1.17	0.465	1.12	0.0630	0.315	0.0690	0.98	0.47	0.236	0.116	0.686	0.353
10/12/2013 12:11	0913-111	13_10_12_1211_16_216	1	1.08	0.471	1.15	0.0660	0.340	0.0670	0.98	0.47	0.236	0.115	0.686	0.350
10/12/2013 12:12	0913-111	13_10_12_1212_16_976	1	0.931	0.437	1.05	0.0620	0.356	0.0700	0.98	0.47	0.236	0.110	0.882	0.317
10/12/2013 12:13	0913-111	13_10_12_1213_17_736	1	0.931	0.447	1.12	0.0680	0.289	0.0670	0.98	0.47	0.236	0.116	0.874	0.331
10/12/2013 12:14	0913-111	13_10_12_1214_18_466	1	2.48	0.475	1.17	0.0660	0.253	0.0690	0.98	0.47	0.236	0.117	0.686	0.357
10/12/2013 12:15	0913-111	13_10_12_1215_19_276	1	1.74	0.455	1.13	0.0650	0.351	0.0670	0.98	0.47	0.236	0.116	0.686	0.334
10/12/2013 12:16	0913-111	13_10_12_1216_20_026	1	1.12	0.469	1.21	0.0670	0.297	0.0700	0.98	0.47	0.236	0.119	0.686	0.342
10/12/2013 12:17	0913-111	13_10_12_1217_20_746	1	1.29	0.468	1.19	0.0650	0.286	0.0700	0.98	0.47	0.236	0.118	1.06	0.349
10/12/2013 12:18	0913-111	13_10_12_1218_21_457	1	0.931	0.483	1.29	0.0630	0.375	0.0700	0.98	0.48	0.236	0.117	0.11	0.351
10/12/2013 12:19	0913-111	13_10_12_1219_22_227	1	1.31	0.491	1.24	0.0630	0.368	0.0670	0.98	0.47	0.236	0.116	0.686	0.363
10/12/2013 12:20	0913-111	13_10_12_1220_23_037	1	1.56	0.461	1.15	0.0650	0.408	0.0690	0.98	0.47	0.236	0.116	0.753	0.342
10/12/2013 12:21	0913-111	13_10_12_1221_23_767	1	0.931	0.478	1.32	0.0620	0.342	0.0670	0.98	0.47	0.236	0.114	0.775	0.350
10/12/2013 12:22	0913-111	13_10_12_1222_24_527	1	1.59	0.481	1.24	0.0680	0.333	0.0690	0.98	0.47	0.236	0.120	0.686	0.366
10/12/2013 12:23	0913-111	13_10_12_1223_25_227	1	0.931	0.477	1.07	0.0650	0.409	0.0650	0.98	0.47	0.236	0.119	0.743	0.346
10/12/2013 12:24	0913-111	13_10_12_1224_25_967	1	1.50	0.467	1.21	0.0630	0.453	0.0670	0.98	0.47	0.236	0.117	0.734	0.355
10/12/2013 12:25	0913-111	13_10_12_1225_26_707	1	0.969	0.482	1.10	0.0650	0.347	0.0670	0.98	0.47	0.236	0.115	0.686	0.341
10/12/2013 12:26	0913-111	13_10_12_1226_27_507	1	1.14	0.478	1.23	0.0680	0.390	0.0690	0.98	0.47	0.236	0.119	0.686	0.355
10/12/2013 12:27	0913-111	13_10_12_1227_28_287	1	1.80	0.477	1.11	0.0640	0.418	0.0680	0.98	0.47	0.236	0.116	0.759	0.350
10/12/2013 12:28	0913-111	13_10_12_1228_29_047	1	1.83	0.475	1.18	0.0650	0.456	0.0680	0.98	0.47	0.236	0.118	0.686	0.348
10/12/2013 12:29	0913-111	13_10_12_1229_29_787	1	1.30	0.479	1.20	0.0670	0.417	0.0690	0.98	0.47	0.236	0.115	0.790	0.350
10/12/2013 12:30	0913-111	13_10_12_1230_30_476	1	1.42	0.468	1.22	0.0640	0.308	0.0700	0.98	0.47	0.236	0.113	0.686	0.344
10/12/2013 12:31	0913-111	13_10_12_1231_31_266	1	1.20	0.471	1.20	0.0690	0.362	0.0680	0.98	0.47	0.236	0.119	0.755	0.355
10/12/2013 12:32	0913-111	13_10_12_1232_31_986	1	1.31	0.464	1.17	0.0620	0.328	0.0680	0.98	0.47	0.236	0.115	0.718	0.348
10/12/2013 12:33	0913-111	13_10_12_1233_32_746	1	1.21	0.464	1.26	0.0600	0.339	0.0680	0.98	0.47	0.236	0.113	0.686	0.338
10/12/2013 12:34	0913-111	13_10_12_1234_33_486	1	1.11	0.469	1.22	0.0670	0.327	0.0670	0.98	0.47	0.236	0.118	0.686	0.344
10/12/2013 12:35	0913-111	13_10_12_1235_34_246	1	1.26	0.462	1.22	0.0630	0.414	0.0700	0.98	0.47	0.236	0.117	1.07	0.344
10/12/2013 12:36	0913-111	13_10_12_1236_35_006	1	1.59	0.482	1.26	0.0650	0.370	0.0700	0.98	0.47	0.236	0.116	0.777	0.351
10/12/2013 12:38	0913-111	13_10_12_1238_36_630	1	2.01	0.489	1.29	0.0650	0.306	0.0660	0.98	0.47	0.236	0.118	0.686	0.366
10/12/2013 12:39	0913-111	13_10_12_1239_37_370	1	2.18	0.485	1.10	0.0640	0.347	0.0700	0.98	0.47	0.236	0.115	0.686	0.360
10/12/2013 12:40	0913-111	13_10_12_1240_38_120	1	0.931	0.461	1.18	0.0630	0.289	0.0680	0.98	0.47	0.236	0.116	0.686	0.345
10/12/2013 12:41	0913-111	13_10_12_1241_38_930	1	1.45	0.482	1.03	0.0670	0.350	0.0740	0.98	0.47	0.236	0.118	0.832	0.351
<b>Average Conc. (ppm):</b>	<b>1</b>	<b>1.35</b>	<b>0.467</b>	<b>1.26</b>	<b>0.647</b>	<b>0.647</b>	<b>0.351</b>	<b>0.0690</b>	<b>0.98</b>	<b>0.48</b>	<b>0.236</b>	<b>0.118</b>	<b>0.759</b>	<b>0.345</b>	

**Aspirator Run 1**

Date	Method	Filename	DF	Acroline (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/12/2013 15:09	0913-111	13_10_12_1509_17_938	1	1.75	0.778	1.05	0.388	8.75	0.236	2.73	1.44	3.00	1.44	4.85	0.583
10/12/2013 15:10	0913-111	13_10_12_1510_18_588	1	3.53	0.815	1.05	0.498	8.61	0.233	2.73	1.02	3.00	1.43		

Company ACT  
 Analyst Initials CUT  
 Parameters EPA Method 320  
 # Samples 21 Runs

Client # 1911  
 Job # 0913-111  
 PO # 3134 1911  
 Report Date VO.62.13.10.18.12.58

**Aspirator Run 2**

Date	Method	Filename	DF	Acrotein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/12/2013 16:36	0913-111	A 13.10.12.1636_22_016	1	2.99	0.831	1.26	0.505	8.21	0.237	2.73	1.31	3.00	1.47	4.99	0.621	
10/12/2013 16:37	0913-111	A 13.10.12.1637_22_786	1	3.74	0.820	1.54	0.511	8.34	0.282	2.73	1.64	3.00	1.45	4.01	0.614	
10/12/2013 16:38	0913-111	A 13.10.12.1638_23_596	1	2.83	0.843	1.44	0.553	8.97	0.299	2.73	1.43	3.00	1.56	4.72	0.630	
10/12/2013 16:39	0913-111	A 13.10.12.1639_24_356	1	3.46	0.860	1.49	0.557	8.84	0.303	2.73	1.50	3.00	1.57	4.59	0.635	
10/12/2013 16:40	0913-111	A 13.10.12.1640_25_056	1	3.59	0.838	1.41	0.559	8.50	0.256	2.73	1.31	3.00	1.60	5.02	0.617	
10/12/2013 16:41	0913-111	A 13.10.12.1641_25_866	1	3.44	0.843	1.29	0.538	8.45	0.250	2.73	1.31	3.00	1.55	5.06	0.632	
10/12/2013 16:42	0913-111	A 13.10.12.1642_26_526	1	2.96	0.785	1.36	0.502	8.81	0.287	2.73	1.38	3.00	1.44	4.99	0.587	
10/12/2013 16:43	0913-111	A 13.10.12.1643_27_336	1	2.73	0.797	1.45	0.494	8.65	0.270	2.73	1.81	3.00	1.38	4.46	0.597	
10/12/2013 16:44	0913-111	A 13.10.12.1644_28_086	1	3.31	0.817	1.50	0.478	8.56	0.271	2.73	1.78	3.00	1.36	3.99	0.612	
10/12/2013 16:45	0913-111	A 13.10.12.1645_28_826	1	2.82	0.785	1.69	0.469	8.67	0.272	2.73	1.69	3.00	1.35	4.60	0.582	
10/12/2013 16:46	0913-111	A 13.10.12.1646_29_536	1	2.91	0.795	1.55	0.479	8.99	0.292	2.73	1.60	3.00	1.37	4.65	0.587	
10/12/2013 16:47	0913-111	A 13.10.12.1647_30_356	1	3.94	0.795	1.64	0.471	8.91	0.265	2.73	1.54	3.00	1.34	4.90	0.595	
10/12/2013 16:48	0913-111	A 13.10.12.1648_31_017	1	4.04	0.764	1.47	0.467	8.86	0.267	2.73	1.46	3.00	1.33	4.72	0.569	
10/12/2013 16:49	0913-111	A 13.10.12.1649_31_837	1	2.86	0.770	1.43	0.465	8.94	0.262	2.73	1.47	3.00	1.30	3.40	0.567	
10/12/2013 16:50	0913-111	A 13.10.12.1650_32_607	1	3.01	0.803	1.46	0.466	9.04	0.262	2.73	1.55	3.00	1.33	3.86	0.594	
10/12/2013 16:51	0913-111	A 13.10.12.1651_33_377	1	2.63	0.782	1.61	0.458	8.96	0.250	2.73	2.12	3.00	1.31	3.90	0.591	
10/12/2013 16:52	0913-111	A 13.10.12.1652_33_977	1	3.25	0.810	1.63	0.462	9.03	0.254	2.73	1.93	3.00	1.33	3.87	0.598	
10/12/2013 16:53	0913-111	A 13.10.12.1653_34_767	1	3.79	0.798	1.59	0.468	9.20	0.266	2.73	1.83	3.00	1.33	4.16	0.591	
10/12/2013 16:54	0913-111	A 13.10.12.1654_35_477	1	3.78	0.797	1.52	0.797	9.20	0.263	2.73	1.92	3.00	1.35	3.91	0.594	
10/12/2013 16:55	0913-111	A 13.10.12.1655_36_207	1	3.31	0.775	1.67	0.458	8.96	0.254	2.73	1.62	3.00	1.30	3.30	0.577	
10/12/2013 16:56	0913-111	A 13.10.12.1656_36_947	1	3.44	0.780	1.50	0.458	8.67	0.256	2.73	1.64	3.00	1.28	3.96	0.582	
10/12/2013 16:57	0913-111	A 13.10.12.1657_37_757	1	3.00	0.766	1.39	0.447	9.14	0.261	2.73	1.42	3.00	1.28	4.10	0.571	
10/12/2013 16:58	0913-111	A 13.10.12.1658_38_477	1	4.04	0.786	1.32	0.450	9.13	0.261	2.73	1.35	3.00	1.28	3.88	0.585	
10/12/2013 16:59	0913-111	A 13.10.12.1659_39_217	1	3.22	0.792	1.32	0.441	9.08	0.270	2.73	1.28	3.00	1.28	4.55	0.595	
10/12/2013 17:00	0913-111	A 13.10.12.1700_40_018	1	2.87	0.787	1.37	0.448	8.89	0.215	2.73	1.27	3.00	1.32	4.41	0.579	
10/12/2013 17:01	0913-111	A 13.10.12.1701_40_728	1	3.47	0.821	1.42	0.451	8.94	0.259	2.73	1.49	3.00	1.29	4.14	0.614	
10/12/2013 17:02	0913-111	A 13.10.12.1702_41_438	1	2.87	0.779	1.65	0.451	9.18	0.252	2.73	1.67	3.00	1.28	3.90	0.578	
10/12/2013 17:03	0913-111	A 13.10.12.1703_42_208	1	3.09	0.814	1.71	0.459	9.05	0.257	2.73	1.69	3.00	1.31	3.50	0.602	
10/12/2013 17:04	0913-111	A 13.10.12.1704_42_928	1	3.58	0.811	1.46	0.464	8.45	0.221	2.73	1.33	3.00	1.36	4.19	0.607	
10/12/2013 17:05	0913-111	A 13.10.12.1705_43_758	1	2.79	0.817	1.54	0.471	8.13	0.268	2.73	1.37	3.00	1.35	3.67	0.606	
10/12/2013 17:06	0913-111	A 13.10.12.1706_44_458	1	3.01	0.782	1.63	0.477	8.01	0.269	2.73	1.41	3.00	1.36	4.20	0.589	
10/12/2013 17:07	0913-111	A 13.10.12.1707_45_208	1	3.91	0.800	1.57	0.489	8.57	0.230	2.73	1.46	3.00	1.40	4.20	0.595	
10/12/2013 17:08	0913-111	A 13.10.12.1708_46_018	1	3.00	0.803	1.52	0.481	8.99	0.265	2.73	1.48	3.00	1.36	4.01	0.604	
10/12/2013 17:09	0913-111	A 13.10.12.1709_46_738	1	2.61	0.787	1.66	0.461	8.09	0.257	2.73	1.73	3.00	1.33	4.40	0.586	
10/12/2013 17:10	0913-111	A 13.10.12.1710_47_448	1	2.63	0.783	1.97	0.442	8.13	0.247	2.73	1.63	3.00	1.32	3.63	0.593	
10/12/2013 17:11	0913-111	A 13.10.12.1711_48_248	1	3.22	0.776	1.67	0.441	9.04	0.255	2.73	1.67	3.00	1.27	3.31	0.580	
10/12/2013 17:12	0913-111	A 13.10.12.1712_48_989	1	3.03	0.828	1.75	0.447	9.29	0.263	2.73	1.58	3.00	1.29	3.28	0.612	
10/12/2013 17:13	0913-111	A 13.10.12.1713_49_799	1	3.28	0.802	1.76	0.455	9.21	0.259	2.73	1.50	3.00	1.30	3.77	0.597	
10/12/2013 17:14	0913-111	A 13.10.12.1714_50_509	1	3.39	0.772	1.72	0.450	8.54	0.253	2.73	1.46	3.00	1.31	3.64	0.576	
10/12/2013 17:15	0913-111	A 13.10.12.1715_51_279	1	2.99	0.774	1.68	0.464	8.90	0.265	2.73	1.47	3.00	1.33	4.39	0.587	
10/12/2013 17:16	0913-111	A 13.10.12.1716_51_999	1	3.88	0.820	1.52	0.472	8.83	0.267	2.73	1.44	3.00	1.34	4.59	0.605	
10/12/2013 17:17	0913-111	A 13.10.12.1717_52_749	1	2.71	0.839	1.78	0.490	8.04	0.270	2.73	1.59	3.00	1.38	4.40	0.621	
10/12/2013 17:18	0913-111	A 13.10.12.1718_53_549	1	3.25	0.828	1.78	0.481	8.89	0.247	2.73	2.10	3.00	1.37	3.25	0.617	
10/12/2013 17:19	0913-111	A 13.10.12.1719_54_299	1	2.67	0.804	1.84	0.455	8.04	0.255	2.73	2.41	3.00	1.32	3.82	0.604	
10/12/2013 17:20	0913-111	A 13.10.12.1720_55_079	1	3.67	0.829	2.03	0.454	8.09	0.265	2.73	1.99	3.00	1.29	3.07	0.620	
10/12/2013 17:21	0913-111	A 13.10.12.1721_55_909	1	2.49	0.800	1.80	0.427	9.19	0.257	2.73	1.60	3.00	1.23	3.85	0.594	
10/12/2013 17:22	0913-111	A 13.10.12.1722_56_659	1	2.88	0.787	1.57	0.433	9.28	0.258	2.73	1.45	3.00	1.26	3.74	0.582	
10/12/2013 17:23	0913-111	A 13.10.12.1723_57_409	1	2.15	0.763	1.67	0.417	9.15	0.261	2.73	1.38	3.00	1.21	3.44	0.567	
10/12/2013 17:24	0913-111	A 13.10.12.1724_58_220	1	3.23	0.784	1.53	0.445	9.46	0.257	2.73	1.41	3.00	1.27	3.15	0.583	
10/12/2013 17:25	0913-111	A 13.10.12.1725_58_940	1	2.76	0.795	1.71	0.444	9.36	0.251	2.73	1.54	3.00	1.27	3.27	0.587	
10/12/2013 17:26	0913-111	A 13.10.12.1726_59_780	1	3.25	0.778	1.79	0.448	8.94	0.236	2.73	1.92	3.00	1.24	3.22	0.578	
10/12/2013 17:27	0913-111	A 13.10.12.1728_00_500	1	2.96	0.759	2.03	0.414	8.98	0.225	2.73	2.41	3.00	1.18	2.94	0.570	
10/12/2013 17:29	0913-111	A 13.10.12.1729_01_300	1	3.24	0.822	1.64	0.434	9.08	0.244	2.73	1.61	3.00	1.24	3.30	0.584	
10/12/2013 17:30	0913-111	A 13.10.12.1730_02_020	1	1.92	0.796	1.45	0.447	9.16	0.257	2.73	1.30	3.00	1.30	3.78	0.592	
10/12/2013 17:31	0913-111	A 13.10.12.1731_02_780	1	2.36	0.812	1.29	0.455	8.71	0.213	2.73	1.29	3.00	1.33	4.55	0.597	
10/12/2013 17:32	0913-111	A 13.10.12.1732_03_490	1	3.07	0.798	1.43	0.462	9.13	0.259	2.73	1.44	3.00	1.32	3.79	0.599	
10/12/2013 17:33	0913-111	A 13.10.12.1733_04_240	1	2.74	0.788	1.48	0.459	8.96	0.256	2.73	1.42	3.00	1.32	3.98	0.580	
10/12/2013 17:34	0913-111	A 13.10.12.1734_04_920	1	3.29	0.835	1.53	0.457	8.92	0.254	2.73	1.62	3.00	1.31	3.72	0.615	
10/12/2013 17:35	0913-111	A 13.10.12.1735_05_660	1	2.95	0.815	1.88	0.448	8.75	0.232	2.73	2.24	3.00	1.25	2.83	0.606	
10/12/2013 17:36	0913-111	A 13.10.12.1736_06_381	1	3.24	1.19	1.05	0.523	6.25	0.213	2.73	1.31	3.00	1.27	1.27	0.602	
Average Conc. (ppm):				1	3.12	0.808	1.58	0.467	8.90	0.256	2.73	1.60	3.00	1.35	3.92	0.602

**Aspirator Run 3**

Date	Method	Filename	DF	Acrotein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/12/2013 18:00	0913-111	A 13.10.12.1800_36_741	1	2.53	0.845	1.05	0.520	9.94	0.225	2.73	1.17	3.00	1.48	3.73	0.627
10/12/2013 18:01	0913-111	A 13.10.12.1801_37_551	1	2.85	0.859	1.05	0.504	8.15	0.224	2.73	1.03	3.00	1.45	3.52	0.631
10/12/2013 18:02	0913-111	A 13.10.12.1802_38_261	1	2.74	0.806	1.05	0.500	8.25	0.223	2.73	1.04	3.00	1.43	3.76	0.

Company ACT  
 Analyst Initials CUT  
 Parameters EPA Method 320  
 # Samples 21 Runs

Client # 1911  
 Job # 0913-111  
 PO # 3134 1911  
 Report Date V0.62.13.10.18.12.58

Dryer 2 Run 1

Date	Method	Filename	DF	Acrotoin (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/13/2013 9:21	0913-111_A	13_10_13_0921_40_932	1	2.53	0.630	5.62	0.101	17.3	0.524	2.78	0.07	1.37	0.203	1.48	0.474	
10/13/2013 9:22	0913-111_A	13_10_13_0922_41_872	1	1.61	0.616	6.08	0.103	18.4	0.551	2.78	0.08	1.70	0.199	0.985	0.455	
10/13/2013 9:23	0913-111_A	13_10_13_0923_41_392	1	2.03	0.641	6.63	0.108	18.8	0.561	2.78	0.08	1.69	0.207	1.39	0.480	
10/13/2013 9:24	0913-111_A	13_10_13_0924_42_103	1	1.25	0.634	6.81	0.106	18.9	0.556	2.78	0.07	1.88	0.213	1.17	0.472	
10/13/2013 9:25	0913-111_A	13_10_13_0925_42_893	1	1.84	0.630	7.02	0.104	19.1	0.559	2.78	0.08	1.97	0.210	0.934	0.466	
10/13/2013 9:26	0913-111_A	13_10_13_0926_43_853	1	2.09	0.648	7.27	0.109	19.3	0.565	2.78	0.07	2.02	0.216	1.24	0.486	
10/13/2013 9:27	0913-111_A	13_10_13_0927_44_353	1	1.59	0.652	7.16	0.111	19.5	0.556	2.78	0.08	2.34	0.216	0.934	0.484	
10/13/2013 9:28	0913-111_A	13_10_13_0928_45_093	1	1.92	0.648	7.07	0.108	19.8	0.550	2.78	0.08	2.23	0.214	0.934	0.485	
10/13/2013 9:29	0913-111_A	13_10_13_0929_45_913	1	2.06	0.610	6.71	0.104	19.9	0.545	2.78	0.07	2.22	0.208	1.13	0.453	
10/13/2013 9:30	0913-111_A	13_10_13_0930_46_663	1	1.25	0.620	6.81	0.108	20.0	0.544	2.78	0.08	2.28	0.210	0.934	0.481	
10/13/2013 9:31	0913-111_A	13_10_13_0931_47_433	1	1.25	0.652	6.61	0.107	20.2	0.542	2.78	0.08	2.27	0.213	0.934	0.466	
10/13/2013 9:32	0913-111_A	13_10_13_0932_48_143	1	1.54	0.631	6.32	0.105	20.2	0.544	2.78	1.97	1.92	0.211	0.945	0.472	
10/13/2013 9:33	0913-111_A	13_10_13_0933_48_863	1	1.93	0.639	6.25	0.106	20.2	0.539	2.78	1.93	2.33	0.212	0.934	0.478	
10/13/2013 9:34	0913-111_A	13_10_13_0934_49_573	1	1.25	0.625	5.96	0.109	20.5	0.547	2.78	1.81	2.36	0.215	0.934	0.465	
10/13/2013 9:35	0913-111_A	13_10_13_0935_50_263	1	1.95	0.617	5.68	0.104	20.3	0.529	2.78	1.72	2.12	0.207	0.934	0.457	
10/13/2013 9:36	0913-111_A	13_10_13_0936_51_104	1	2.84	0.624	5.68	0.107	19.9	0.523	2.78	1.71	2.23	0.211	0.934	0.467	
10/13/2013 9:37	0913-111_A	13_10_13_0937_51_824	1	1.88	0.617	5.55	0.101	19.3	0.509	2.78	1.60	2.16	0.207	0.934	0.460	
10/13/2013 9:38	0913-111_A	13_10_13_0938_52_634	1	1.86	0.614	5.38	0.104	18.8	0.513	2.78	1.62	2.11	0.206	0.934	0.457	
10/13/2013 9:39	0913-111_A	13_10_13_0939_53_384	1	1.45	0.624	5.46	0.101	19.1	0.516	2.78	1.59	2.26	0.209	0.934	0.462	
10/13/2013 9:40	0913-111_A	13_10_13_0940_54_084	1	1.63	0.644	5.40	0.104	19.9	0.517	2.78	1.49	2.30	0.216	0.934	0.479	
10/13/2013 9:41	0913-111_A	13_10_13_0941_54_884	1	2.02	0.611	5.47	0.108	20.4	0.517	2.78	1.58	2.20	0.216	0.934	0.455	
10/13/2013 9:42	0913-111_A	13_10_13_0942_55_604	1	1.97	0.624	5.40	0.107	20.9	0.511	2.78	1.61	2.26	0.213	0.934	0.465	
10/13/2013 9:43	0913-111_A	13_10_13_0943_56_414	1	2.27	0.601	5.23	0.104	21.1	0.513	2.78	1.57	2.09	0.213	0.934	0.449	
10/13/2013 9:44	0913-111_A	13_10_13_0944_57_124	1	1.69	0.614	5.28	0.111	21.2	0.507	2.78	1.65	2.02	0.219	0.934	0.464	
10/13/2013 9:45	0913-111_A	13_10_13_0945_57_864	1	1.67	0.627	5.10	0.105	21.1	0.509	2.78	1.53	2.13	0.213	0.934	0.466	
10/13/2013 9:46	0913-111_A	13_10_13_0946_58_664	1	1.91	0.627	5.13	0.106	21.4	0.514	2.78	1.46	2.32	0.215	0.934	0.462	
10/13/2013 9:47	0913-111_A	13_10_13_0947_59_355	1	1.42	0.595	5.45	0.108	21.7	0.521	2.78	1.53	2.19	0.216	0.934	0.448	
10/13/2013 9:49	0913-111_A	13_10_13_0949_00_105	1	1.86	0.641	5.46	0.110	21.5	0.510	2.78	1.51	2.23	0.220	0.934	0.479	
10/13/2013 9:50	0913-111_A	13_10_13_0950_00_875	1	1.25	0.630	5.66	0.107	21.4	0.517	2.78	1.54	2.22	0.218	0.934	0.465	
10/13/2013 9:51	0913-111_A	13_10_13_0951_01_625	1	1.89	0.645	5.83	0.116	21.8	0.536	2.78	1.39	2.24	0.224	0.934	0.465	
10/13/2013 9:52	0913-111_A	13_10_13_0952_02_335	1	1.62	0.635	6.10	0.109	21.9	0.541	2.78	1.51	2.48	0.225	0.934	0.472	
10/13/2013 9:53	0913-111_A	13_10_13_0953_03_175	1	1.66	0.625	5.99	0.109	21.6	0.539	2.78	1.51	2.37	0.220	0.934	0.466	
10/13/2013 9:54	0913-111_A	13_10_13_0954_03_855	1	1.93	0.623	5.89	0.110	21.9	0.541	2.78	1.54	2.49	0.224	0.934	0.464	
10/13/2013 9:55	0913-111_A	13_10_13_0955_04_565	1	2.47	0.633	6.09	0.110	21.8	0.540	2.78	1.64	2.52	0.222	0.934	0.474	
10/13/2013 9:56	0913-111_A	13_10_13_0956_05_265	1	1.92	0.622	6.19	0.111	21.9	0.539	2.78	1.59	2.68	0.221	0.934	0.467	
10/13/2013 9:57	0913-111_A	13_10_13_0957_06_075	1	1.81	0.614	6.23	0.112	21.9	0.543	2.78	1.58	2.57	0.226	0.934	0.460	
10/13/2013 9:58	0913-111_A	13_10_13_0958_06_845	1	1.40	0.650	6.62	0.113	22.1	0.556	2.78	1.64	2.70	0.229	0.934	0.483	
10/13/2013 9:59	0913-111_A	13_10_13_0959_07_685	1	1.79	0.616	6.83	0.113	22.1	0.565	2.78	1.65	2.62	0.230	0.934	0.467	
10/13/2013 10:00	0913-111_A	13_10_13_1000_08_486	1	1.25	0.640	6.83	0.109	22.1	0.561	2.78	1.64	2.62	0.224	0.934	0.482	
10/13/2013 10:01	0913-111_A	13_10_13_1001_09_226	1	1.28	0.649	7.05	0.110	21.8	0.555	2.78	1.67	2.78	0.234	0.934	0.481	
10/13/2013 10:02	0913-111_A	13_10_13_1002_09_906	1	2.18	0.629	6.90	0.114	21.5	0.548	2.78	1.63	2.82	0.232	0.934	0.473	
10/13/2013 10:03	0913-111_A	13_10_13_1003_10_696	1	2.08	0.678	6.91	0.118	21.2	0.543	2.78	1.54	2.87	0.239	0.934	0.507	
10/13/2013 10:04	0913-111_A	13_10_13_1004_11_436	1	2.56	0.639	6.24	0.114	20.9	0.528	2.78	1.49	2.62	0.231	0.934	0.482	
10/13/2013 10:05	0913-111_A	13_10_13_1005_12_176	1	1.61	0.623	6.19	0.107	20.7	0.525	2.78	1.52	2.66	0.228	0.934	0.464	
10/13/2013 10:06	0913-111_A	13_10_13_1006_12_966	1	2.39	0.625	6.04	0.109	19.6	0.533	2.78	1.54	2.66	0.233	0.934	0.468	
10/13/2013 10:07	0913-111_A	13_10_13_1007_13_776	1	1.78	0.625	6.36	0.111	18.8	0.542	2.78	1.62	2.53	0.228	0.934	0.472	
10/13/2013 10:08	0913-111_A	13_10_13_1008_14_516	1	2.53	0.642	6.62	0.106	17.6	0.550	2.78	1.55	2.58	0.229	0.934	0.480	
10/13/2013 10:09	0913-111_A	13_10_13_1009_15_276	1	2.39	0.634	7.03	0.111	16.5	0.550	2.78	1.51	2.61	0.227	0.934	0.478	
10/13/2013 10:10	0913-111_A	13_10_13_1010_15_986	1	1.44	0.650	7.05	0.111	15.3	0.549	2.78	1.57	2.40	0.228	0.934	0.494	
10/13/2013 10:11	0913-111_A	13_10_13_1011_16_786	1	2.51	0.631	7.36	0.109	14.0	0.549	2.78	1.55	2.54	0.228	0.934	0.476	
10/13/2013 10:12	0913-111_A	13_10_13_1012_17_487	1	1.46	0.650	7.48	0.107	12.8	0.543	2.78	1.51	2.63	0.225	0.934	0.483	
10/13/2013 10:13	0913-111_A	13_10_13_1013_18_287	1	2.24	0.660	7.75	0.108	11.6	0.536	2.78	1.49	2.72	0.225	0.934	0.490	
10/13/2013 10:14	0913-111_A	13_10_13_1014_19_017	1	2.42	0.677	8.54	0.110	11.0	0.555	2.78	1.38	2.71	0.227	0.934	0.512	
10/13/2013 10:15	0913-111_A	13_10_13_1015_19_817	1	2.16	0.619	7.71	0.106	11.0	0.543	2.78	1.24	2.71	0.225	0.934	0.470	
10/13/2013 10:16	0913-111_A	13_10_13_1016_20_417	1	2.13	0.618	7.44	0.109	11.7	0.549	2.78	1.34	2.42	0.233	0.934	0.466	
10/13/2013 10:17	0913-111_A	13_10_13_1017_21_227	1	1.37	0.621	7.70	0.113	12.8	0.556	2.78	1.46	2.61	0.242	0.939	0.470	
10/13/2013 10:18	0913-111_A	13_10_13_1018_21_987	1	2.79	0.636	7.44	0.110	13.2	0.560	2.78	1.49	2.75	0.255	1.03	0.479	
10/13/2013 10:19	0913-111_A	13_10_13_1019_22_707	1	1.95	0.634	6.71	0.107	12.9	0.550	2.78	1.53	2.64	0.256	0.934	0.471	
10/13/2013 10:20	0913-111_A	13_10_13_1020_23_387	1	2.11	0.594	6.66	0.110	12.8	0.547	2.78	1.51	2.54	0.258	0.934	0.447	
10/13/2013 10:21	0913-111_A	13_10_13_1021_23_197	1	3.00	0.628	6.73	0.113	12.7	0.548	2.78	1.51	2.53	0.273	0.988	0.468	
Average Conc. (ppm):				1	1.90	0.631	6.40	0.108	18.8	0.539	2.78	1.29	2.37	0.222	0.967	0.472

Dryer 2 Run 2

Date	Method	Filename	DF	Acrotoin (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/13/2013 11:04	0913-111_A	13_10_13_1104_56_401	1	2.45	0.615	6.06	0.106	10.4	0.532	2.78	1.31	1.47	0.260	3.09	0.457
10/13/2013 11:05	0913-111_A	13_10_13_1105_57_191	1	2.20	0.620	6.50	0.108	10.0	0.535	2.78	1.31	1.39	0.260	3.57	0.457
10/13/2013 11:06	0913-111_A	13_10_13_1106_57_991	1	2.54	0.621	7.03									

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	V0.62 13.10.18.12.58

## Path Length - Path

Date	Method	FileName	ethylene (ppm)	SEC (ppm)
10/10/2013 8:12	0913-111_CTS	13_10_10_0812_04_850	8.79	0.137
10/10/2013 8:12	0913-111_CTS	13_10_10_0812_23_390	8.77	0.136
10/10/2013 8:12	0913-111_CTS	13_10_10_0812_42_040	8.78	0.137
10/10/2013 8:13	0913-111_CTS	13_10_10_0813_00_420	8.80	0.136
10/10/2013 8:13	0913-111_CTS	13_10_10_0813_18_930	8.82	0.137
10/10/2013 8:13	0913-111_CTS	13_10_10_0813_37_540	8.81	0.138
10/10/2013 8:13	0913-111_CTS	13_10_10_0813_56_040	8.82	0.137
10/10/2013 8:14	0913-111_CTS	13_10_10_0814_14_670	8.80	0.138
<b>Average (m)</b>			<b>8.80</b>	<b>0.137</b>
10/10/2013 19:33	0913-111_CTS	13_10_10_1933_09_783	8.67	0.137
10/10/2013 19:33	0913-111_CTS	13_10_10_1933_28_313	8.69	0.137
10/10/2013 19:33	0913-111_CTS	13_10_10_1933_46_843	8.69	0.138
10/10/2013 19:34	0913-111_CTS	13_10_10_1934_05_353	8.71	0.137
10/10/2013 19:34	0913-111_CTS	13_10_10_1934_23_963	8.70	0.137
10/10/2013 19:34	0913-111_CTS	13_10_10_1934_42_473	8.71	0.138
10/10/2013 19:35	0913-111_CTS	13_10_10_1935_01_103	8.66	0.137
10/10/2013 19:35	0913-111_CTS	13_10_10_1935_19_513	8.67	0.139
<b>Average (m)</b>			<b>8.69</b>	<b>0.138</b>
<b>Average Pathlength (m)</b>			<b>8.74</b>	<b>0.137</b>
Max (m)			8.80	
Min (m)			8.69	
Max % Deviation			0.62%	

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	V0.62 13.10.18.12.58

## Path Length - Path

Date	Method	FileName	ethylene (ppm)	SEC (ppm)
10/11/2013 9:38	0913-111_CTS	13_10_11_0938_33_970	8.13	0.130
10/11/2013 9:38	0913-111_CTS	13_10_11_0938_52_580	8.16	0.129
10/11/2013 9:39	0913-111_CTS	13_10_11_0939_11_060	8.17	0.129
10/11/2013 9:39	0913-111_CTS	13_10_11_0939_29_540	8.18	0.129
10/11/2013 9:39	0913-111_CTS	13_10_11_0939_48_180	8.19	0.130
10/11/2013 9:40	0913-111_CTS	13_10_11_0940_06_710	8.18	0.129
10/11/2013 9:40	0913-111_CTS	13_10_11_0940_25_190	8.20	0.129
10/11/2013 9:40	0913-111_CTS	13_10_11_0940_43_760	8.18	0.130
<b>Average (m)</b>			<b>8.17</b>	<b>0.129</b>
10/11/2013 11:22	0913-111_CTS	13_10_11_1122_55_958	8.63	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_14_479	8.66	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_32_989	8.68	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_51_519	8.71	0.133
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_10_019	8.70	0.134
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_28_559	8.73	0.134
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_47_159	8.74	0.134
10/11/2013 11:25	0913-111_CTS	13_10_11_1125_05_659	8.74	0.134
<b>Average (m)</b>			<b>8.70</b>	<b>0.134</b>
<b>Average Pathlength (m)</b>			<b>8.44</b>	<b>0.131</b>
Max (m)			8.70	
Min (m)			8.17	
Max % Deviation			3.10%	

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	V0.62 13.10.18.12.58

## Path Length - Path

Date	Method	FileName	ethylene (ppm)	SEC (ppm)
10/11/2013 11:22	0913-111_CTS	13_10_11_1122_55_958	8.63	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_14_479	8.66	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_32_989	8.68	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_51_519	8.71	0.133
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_10_019	8.70	0.134
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_28_559	8.73	0.134
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_47_159	8.74	0.134
10/11/2013 11:25	0913-111_CTS	13_10_11_1125_05_659	8.74	0.134
<b>Average (m)</b>			<b>8.70</b>	<b>0.134</b>
10/11/2013 13:02	0913-111_CTS	13_10_11_1302_32_762	8.73	0.133
10/11/2013 13:02	0913-111_CTS	13_10_11_1302_51_282	8.77	0.134
10/11/2013 13:03	0913-111_CTS	13_10_11_1303_09_882	8.73	0.133
10/11/2013 13:03	0913-111_CTS	13_10_11_1303_28_382	8.71	0.133
10/11/2013 13:03	0913-111_CTS	13_10_11_1303_46_792	8.74	0.133
10/11/2013 13:04	0913-111_CTS	13_10_11_1304_05_402	8.75	0.133
10/11/2013 13:04	0913-111_CTS	13_10_11_1304_23_922	8.74	0.133
10/11/2013 13:04	0913-111_CTS	13_10_11_1304_42_382	8.73	0.133
<b>Average (m)</b>			<b>8.74</b>	<b>0.133</b>
10/11/2013 17:56	0913-111_CTS	13_10_11_1756_33_272	8.44	0.129
10/11/2013 17:56	0913-111_CTS	13_10_11_1756_51_882	8.57	0.130
10/11/2013 17:57	0913-111_CTS	13_10_11_1757_10_412	8.67	0.132
10/11/2013 17:57	0913-111_CTS	13_10_11_1757_29_032	8.71	0.132
10/11/2013 17:57	0913-111_CTS	13_10_11_1757_47_542	8.75	0.132
10/11/2013 17:58	0913-111_CTS	13_10_11_1758_06_042	8.76	0.132
10/11/2013 17:58	0913-111_CTS	13_10_11_1758_24_642	8.79	0.133
10/11/2013 17:58	0913-111_CTS	13_10_11_1758_43_102	8.75	0.133
<b>Average (m)</b>			<b>8.68</b>	<b>0.132</b>
10/12/2013 7:59	0913-111_CTS	13_10_12_0759_05_353	8.70	0.139
10/12/2013 7:59	0913-111_CTS	13_10_12_0759_23_963	8.74	0.139
10/12/2013 7:59	0913-111_CTS	13_10_12_0759_42_473	8.71	0.137
10/12/2013 8:00	0913-111_CTS	13_10_12_0800_01_103	8.70	0.136
10/12/2013 8:00	0913-111_CTS	13_10_12_0800_19_593	8.69	0.137
10/12/2013 8:00	0913-111_CTS	13_10_12_0800_38_103	8.75	0.136
10/12/2013 8:00	0913-111_CTS	13_10_12_0800_56_713	8.68	0.136
10/12/2013 8:01	0913-111_CTS	13_10_12_0801_15_143	8.68	0.136

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	V0.62 13.10.18.12.58

## Path Length - Path

Date	Method	FileName	ethylene (ppm)	SEC (ppm)
		<b>Average (m)</b>	<b>8.71</b>	<b>0.137</b>
10/12/2013 8:15	0913-111_CTS	13_10_12_0815_33_684	8.60	0.134
10/12/2013 8:15	0913-111_CTS	13_10_12_0815_52_184	8.59	0.134
10/12/2013 8:16	0913-111_CTS	13_10_12_0816_10_704	8.58	0.134
10/12/2013 8:16	0913-111_CTS	13_10_12_0816_29_314	8.60	0.133
10/12/2013 8:16	0913-111_CTS	13_10_12_0816_47_804	8.60	0.133
10/12/2013 8:17	0913-111_CTS	13_10_12_0817_06_244	8.61	0.134
10/12/2013 8:17	0913-111_CTS	13_10_12_0817_24_834	8.62	0.133
10/12/2013 8:17	0913-111_CTS	13_10_12_0817_43_344	8.59	0.134
		<b>Average (m)</b>	<b>8.60</b>	<b>0.134</b>
10/12/2013 13:02	0913-111_CTS	13_10_12_1302_33_472	8.74	0.137
10/12/2013 13:02	0913-111_CTS	13_10_12_1302_52_082	8.76	0.137
10/12/2013 13:03	0913-111_CTS	13_10_12_1303_10_582	8.79	0.137
10/12/2013 13:03	0913-111_CTS	13_10_12_1303_29_082	8.79	0.138
10/12/2013 13:03	0913-111_CTS	13_10_12_1303_47_602	8.78	0.137
10/12/2013 13:04	0913-111_CTS	13_10_12_1304_06_112	8.77	0.137
10/12/2013 13:04	0913-111_CTS	13_10_12_1304_24_752	8.78	0.137
10/12/2013 13:04	0913-111_CTS	13_10_12_1304_43_242	8.78	0.138
		<b>Average (m)</b>	<b>8.78</b>	<b>0.137</b>
10/12/2013 19:42	0913-111_CTS	13_10_12_1942_21_772	8.68	0.133
10/12/2013 19:42	0913-111_CTS	13_10_12_1942_40_362	8.71	0.132
10/12/2013 19:42	0913-111_CTS	13_10_12_1942_58_862	8.77	0.134
10/12/2013 19:43	0913-111_CTS	13_10_12_1943_17_462	8.77	0.134
10/12/2013 19:43	0913-111_CTS	13_10_12_1943_35_992	8.80	0.134
10/12/2013 19:43	0913-111_CTS	13_10_12_1943_54_432	8.79	0.133
10/12/2013 19:44	0913-111_CTS	13_10_12_1944_13_082	8.82	0.135
10/12/2013 19:44	0913-111_CTS	13_10_12_1944_31_502	8.78	0.134
		<b>Average (m)</b>	<b>8.76</b>	<b>0.134</b>
10/13/2013 7:58	0913-111_CTS	13_10_13_0758_40_845	8.55	0.130
10/13/2013 7:58	0913-111_CTS	13_10_13_0758_59_345	8.50	0.129
10/13/2013 7:59	0913-111_CTS	13_10_13_0759_17_835	8.49	0.129
10/13/2013 7:59	0913-111_CTS	13_10_13_0759_36_445	8.50	0.129
10/13/2013 7:59	0913-111_CTS	13_10_13_0759_54_925	8.49	0.129
10/13/2013 8:00	0913-111_CTS	13_10_13_0800_13_565	8.51	0.130
10/13/2013 8:00	0913-111_CTS	13_10_13_0800_31_995	8.47	0.130

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	V0.62 13.10.18.12.58

## Path Length - Path

Date	Method	FileName	ethylene (ppm)	SEC (ppm)
10/13/2013 8:00	0913-111_CTS	13_10_13_0800_50_506	8.52	0.130
<b>Average (m)</b>			<b>8.50</b>	<b>0.130</b>
10/13/2013 8:16	0913-111_CTS	13_10_13_0816_09_687	8.73	0.133
10/13/2013 8:16	0913-111_CTS	13_10_13_0816_28_197	8.69	0.133
10/13/2013 8:16	0913-111_CTS	13_10_13_0816_46_707	8.71	0.134
10/13/2013 8:17	0913-111_CTS	13_10_13_0817_05_247	8.72	0.133
10/13/2013 8:17	0913-111_CTS	13_10_13_0817_23_757	8.73	0.134
10/13/2013 8:17	0913-111_CTS	13_10_13_0817_42_347	8.77	0.134
10/13/2013 8:18	0913-111_CTS	13_10_13_0818_00_857	8.70	0.133
10/13/2013 8:18	0913-111_CTS	13_10_13_0818_19_377	8.74	0.134
<b>Average (m)</b>			<b>8.72</b>	<b>0.134</b>
10/13/2013 14:34	0913-111_CTS	13_10_13_1434_10_233	8.70	0.135
10/13/2013 14:34	0913-111_CTS	13_10_13_1434_28_743	8.73	0.135
10/13/2013 14:34	0913-111_CTS	13_10_13_1434_47_263	8.76	0.136
10/13/2013 14:35	0913-111_CTS	13_10_13_1435_05_884	8.75	0.135
10/13/2013 14:35	0913-111_CTS	13_10_13_1435_24_394	8.72	0.133
10/13/2013 14:35	0913-111_CTS	13_10_13_1435_42_804	8.74	0.135
10/13/2013 14:36	0913-111_CTS	13_10_13_1436_01_424	8.74	0.134
10/13/2013 14:36	0913-111_CTS	13_10_13_1436_19_934	8.72	0.134
<b>Average (m)</b>			<b>8.73</b>	<b>0.135</b>
<b>Average Pathlength (m)</b>			<b>8.69</b>	<b>0.134</b>
Max (m)			8.78	
Min (m)			8.50	
Max % Deviation			2.17%	

**APPENDIX D**

**Method 320 Log Sheet**

FTIR Log - Enviva Wiggins

Date	Time	Filename	Method	Pressure	Notes	Run ID	
10-Oct	754	13.10.10.0753.42.969	CTS	14.7	Background		
	806	13.10.10.0806.08.036	CTS	14.7	CTS (pathlength = 8.78 m)		
	855	13.10.10.0855.00.744	0913-177A	14.6	Background		
	914	<b>13.10.10.0914.12.674</b>	<b>0913-177A</b>	<b>13.5</b>	<b>Sampling GHM - Run 1 (0917-1017)</b>	<b>1</b>	
	1036	<b>13.10.10.0914.12.674</b>	<b>0913-177A</b>	<b>13.3</b>	<b>Sampling GHM - Run 2 (1036-1136)</b>	<b>2</b>	
	1150	<b>13.10.10.0914.12.674</b>	<b>0913-177A</b>	<b>13.5</b>	<b>Sampling GHM - Run 3 (1150-1250)</b>	<b>3</b>	
	1738	<b>13.10.10.1429.45.242</b>	<b>0913-177A</b>	<b>13.9</b>	<b>Sampling Dryer 1 - Run 1 (1738-1838)</b>	<b>4</b>	
	1915	13.10.10.1915.03.541	0913-177A	14.6	Background		
	1923	<b>13.10.10.1923.11.342</b>	CTS	<b>14.6</b>	Background		
	1926	<b>13.10.10.1926.54.274</b>	CTS	<b>14.7</b>	<b>CTS (pathlength = 8.78 m)</b>		
	2005	<b>13.10.10.2004.59.706</b>	0913-177A	<b>14.6</b>	<b>Water Spectra (Dryer 1 - Run 1)</b>		
	2035	<b>13.10.10.2034.59.394</b>	0913-177A	<b>14.6</b>	<b>Water Spectra (GHM)</b>		
11-Oct	933	13.10.11.0932.48.189	CTS	14.8	Background	Background interference	
	936	13.10.11.0936.57.524	CTS	14.8	CTS (pathlength = 8.18 m)		
	948	13.10.11.0948.41.630	0913-177A	14.8	Background		
	955	<b>13.10.11.0954.19.486</b>	<b>0913-177A</b>	<b>14.4</b>	<b>Sampling Dryer 1 - Run 2 (1000-1100)</b>		<b>5</b>
	1117	13.10.11.1117.32.588	CTS	14.8	Background		
	1121	13.10.11.1121.00.310	CTS	14.8	CTS (pathlength = 8.73 m)		
	1127	13.10.11.1127.34.199	0913-177A	14.7	Background		
	1137	<b>13.10.11.1134.41.951</b>	<b>0913-177A</b>	<b>14.2</b>	<b>Sampling Dryer 1 - Run 3 (1137-1237)</b>		<b>6</b>
	1257	13.10.11.1257.46.512	CTS	14.7	Background		
	1301	13.10.11.1301.14.338	CTS	14.7	CTS (pathlength = 8.73 m)		
	1308	13.10.11.1308.39.947	0913-177A	14.7	Background		
	1342	<b>13.10.11.1342.51.774</b>	<b>0913-177A</b>	<b>14.2</b>	<b>Sampling Pellet Cooler 2 - Run 1 (1343-1443)</b>		<b>7</b>
	1508	<b>13.10.11.1342.51.774</b>	<b>0913-177A</b>	<b>14.1</b>	<b>Sampling Pellet Cooler 2 - Run 2 (1508-1608)</b>		<b>8</b>
	1650	<b>13.10.11.1342.51.774</b>	<b>0913-177A</b>	<b>14.1</b>	<b>Sampling Pellet Cooler 2 - Run 3 (1629-1729)</b>		<b>9</b>
	1752	13.10.11.1752.08.661	CTS	14.6	Background		
	1755	13.10.11.1755.37.781	CTS	14.6	CTS (pathlength = 8.7165 m)		
	1802	13.10.11.1802.37.522	0913-177A	14.6	Background		
	1342	<b>13.10.11.1809.44.552</b>	<b>0913-177A</b>	<b>14.3</b>	<b>Sampling Hammermill 2 - Run 1 (1811-1911)</b>		<b>10</b>
	1935	<b>13.10.11.1809.44.552</b>	<b>0913-177A</b>	<b>14.4</b>	<b>Sampling Hammermill 2 - Run 2 (1935-2035)</b>		<b>11</b>
	2048	<b>13.10.11.1809.44.552</b>	<b>0913-177A</b>	<b>14.5</b>	<b>Sampling Hammermill 2 - Run 3 (2048-2148)</b>		<b>12</b>
2200	13.10.11.2200.54.734	CTS	14.7	Background			
2204	13.10.11.2204.32.940	CTS	14.8	CTS (pathlength = 8.75475 m)			
2213	13.10.11.2213.44.875	0913-177A	14.8	Background			
2224	<b>13.10.11.2224.53.772</b>	<b>0913-177A</b>	<b>14.7</b>	<b>Water Spectra (Dryer 1 - Run 2, 3)</b>			
2240	<b>13.10.11.2240.27.896</b>	<b>0913-177A</b>	<b>14.7</b>	<b>Water Spectra (Pellet Cooler 2, Hammermill 2)</b>			
12-Oct	0805	13.10.12.0805.29.253	CTS	14.9	Background		
	0809	13.10.12.0809.22.964	CTS	14.9	CTS (pathlength = 8.59 m)		
	0822	13.10.12.08.22.17.097	0913-177A	14.8	Background		
	858	<b>13.10.12.0857.28.740</b>	<b>0913-177A</b>	<b>14.4</b>	<b>Sampling Pellet Cooler 1- Run 1 (0858-0958)</b>	<b>13</b>	
	1022	<b>13.10.12.0857.28.740</b>	<b>0913-177A</b>	<b>14.3</b>	<b>Sampling Pellet Cooler 1- Run 2 (1022-1122)</b>	<b>14</b>	
	1141	<b>13.10.12.0857.28.740</b>	<b>0913-177A</b>	<b>14.2</b>	<b>Sampling Pellet Cooler 1- Run 1 (1141-1241)</b>	<b>15</b>	
	1257	13.10.12.1257.12.281	CTS	14.6	Background		
	1301	13.10.12.1300.55.794	CTS	14.6	CTS (pathlength = 8.77 m)		
	1308	13.10.12.1309.21.752	0913-177A	14.6	Background		
	1509	<b>13.10.12.1347.50.707</b>	<b>0913-177A</b>	<b>13.8</b>	<b>Sampling Aspirator- Run 1 (1509-1609)</b>	<b>16</b>	
	1636	<b>13.10.12.1347.50.707</b>	<b>0913-177A</b>	<b>13.8</b>	<b>Sampling Aspirator- Run 2 (1636-1736)</b>	<b>17</b>	
	1800	<b>13.10.12.1347.50.707</b>	<b>0913-177A</b>	<b>13.9</b>	<b>Sampling Aspirator- Run 3 (1800-1900)</b>	<b>18</b>	
	1936	13.10.12.1936.27.563	CTS	14.91	Background		
	1940	13.10.12.1940.26.868	CTS	14.72	CTS (pathlength = 8.78 m)		
	1951	13.10.12.1951.39.443	0913-177A	14.75	Background		
	2003	<b>13.10.12.2003.07.633</b>	0913-177A	<b>14.59</b>	<b>Water Spectra (Aspirator)</b>		
	2023	<b>13.10.12.2023.12.427</b>	0913-177A	<b>14.55</b>	<b>Water Spectra (Pellet Cooler 1)</b>		
	13-Oct	807	13.10.13.0807.16.306	0913-177A	14.77	Background	
0810		13.10.13.0810.33.996	CTS	14.78	Background		
0810		13.10.13.0813.37.211	CTS	14.85	CTS (pathlength = 8.71 m)		
0921		<b>13.10.13.0919.17.032</b>	<b>0913-177A</b>	<b>14.24</b>	<b>Sampling Dryer 2 - Run 1 (0921-1021)</b>	<b>19</b>	
1104		<b>13.10.13.0919.17.032</b>	<b>0913-177A</b>	<b>14.17</b>	<b>Sampling Dryer 2 - Run 2 (1104-1204)</b>	<b>20</b>	
1231		<b>13.10.13.0919.17.032</b>	<b>0913-177A</b>	<b>14.17</b>	<b>Sampling Dryer 2 - Run 3 (1231-1347); paused 1236-1252</b>	<b>21</b>	
1420		13.10.13.1419.54.342	CTS	14.91	Background		
1430		13.10.13.1425.31.173	CTS	14.85	CTS (pathlength = 8.73 m)		
1447		13.10.13.1447.35.695	0913-177A	14.8	Background		
1506		<b>13.10.13.1506.31.082</b>	0913-177A	<b>14.71</b>	<b>Water Spectra (Dryer 2)</b>		

## **APPENDIX E**

### **Example Calculations**

## EXAMPLE CALCULATIONS

Run Number: Dryer 1 – Run 1

### **Stack Gas Temperature, °R**

$$T_s = 460 + t_s$$

$$T_s = 460 + 146.3 = 606.3 \text{ °R}$$

### **Volume of Dry Gas Sampled at Standard Conditions, Dry Standard Cubic Feet**

$$V_{\text{mstd}} = [17.64] \gamma \left[ V_m \left[ \frac{\left( P_{\text{bar}} + \frac{\Delta H}{13.6} \right)}{T_m + 460} \right] \right]$$

$$V_{\text{mstd}} = [17.64] [0.9728] [33.201] \left[ \frac{\left( 29.90 + \frac{1.00}{13.6} \right)}{541.3} \right]$$

$$V_{\text{mstd}} = 31.564 \text{ ft}^3$$

### **Volume of Water Sampled, SCF**

$$V_{\text{wstd}} = 0.04715 \text{ [Weight of Condensed Moisture]}$$

$$V_{\text{wstd}} = 0.04715 [129.5]$$

$$V_{\text{wstd}} = 6.106 \text{ ft}^3$$

### **Fraction of Water Vapor in Sample Gas Stream**

$$\% \text{H}_2\text{O} = \left[ \frac{V_{\text{wstd}}}{V_{\text{mstd}} + V_{\text{wstd}}} \right] \times 100$$

$$\% \text{H}_2\text{O} = \left[ \frac{6.106}{31.564 + 6.106} \right] \times 100$$

$$\% \text{H}_2\text{O} = 16.21$$

### **Dry Mole Fraction of Flue Gas**

$$M_{fd} = 1 - \%H_2O/100$$

$$M_{fd} = 1 - [16.21/100]$$

$$M_{fd} = 0.838$$

### **Molecular Weight of Sample Gas, Dry**

$$M_d = 0.44[\%CO_2] + 0.32[\%O_2] + 0.28[100 - \%O_2 - \%CO_2]$$

$$M_d = 0.44[2.0] + 0.32[19.0] + 0.28[100 - 19.0 - 2.0]$$

$$M_d = 29.08 \text{ pounds/pound-mole}$$

### **Molecular Weight of Sample Gas, Actual Conditions**

$$M_s = [M_d \times M_{fd}] + [0.18 \times \%H_2O]$$

$$M_s = [29.08 \times 0.838] + [0.18 \times 16.21]$$

$$M_s = 27.28 \text{ pounds/pound-mole}$$

### **Average Stack Gas Velocity, Feet/second**

$$v_s = K_p C_p \left( \sqrt{(\Delta p)} \right)_{avg} \left[ \sqrt{\frac{T_s + 460}{P_s M_s}} \right]$$

$$v_s = (85.49)(0.84) \left( \sqrt{(0.1.283)} \right) \left[ \sqrt{\frac{606.3}{(29.84)(27.28)}} \right]$$

$$v_s = 70.18 \text{ feet/second}$$

### **Wet Volumetric Flue Gas Flow Rate at Stack Conditions, Cubic Feet per Minute**

$$Q_{aw} = 60 \times v_s \times A$$

$$Q_{aw} = 60 \times 70.18 \times 10.56$$

$$Q_{aw} = 44,461 \text{ Actual Cubic Feet per Minute}$$

### **Dry Volumetric Flue Gas Flow Rate at Standard Conditions, Cubic Feet per Minute**

$$Q_{sd} = 60 \times Mfd \times v_s \times A \times \left[ \frac{528}{ts + 460} \right] \left[ \frac{Ps}{29.92} \right]$$

$$Q_{sd} = 60 \times 0.838 \times 70.18 \times 10.56 \left[ \frac{528}{606.3} \right] \left[ \frac{29.84}{29.92} \right]$$

$$Q_{sd} = 32,360 \text{ Dry Standard Cubic Feet per Minute}$$

### **Average THC Dry Basis Concentration as Propane**

$$C_{THCD} = (C_{THCW}) / (M_{fd})$$

Where:  $C_{THCd}$  = dry basis concentration of THC in ppm  
 $M_{fd}$  = dry mole fraction from Method 4 concurrent run

$$C_{THCD} = 66.7 / 0.838 = 79.6 \text{ ppm THC as propane}$$

### **Average THC Dry Basis Concentration as Carbon**

$$C_{THCD} = (C_{THCW}) \times (3) / (M_{fd})$$

Where:  $C_{THCd}$  = dry basis concentration of THC in ppm  
 $M_{fd}$  = dry mole fraction from Method 4 concurrent run

$$C_{THCD} = (66.7) \times (3) / 0.838 = 238.8 \text{ ppm THC as Carbon}$$

### **VOC Emission Rate in Pounds Per Hour**

$$E_{VOC} = (C_{VOC}) (Q_{SD}) (60 \text{ min/hr}) (C_F)$$

Where:  $Q_{SD}$  = measured flow rate in stack in dscfm  
 $C_F$  = Conversion factor in lb/scf – ppm  
 $C_F = 3.117 \times 10^{-8}$  for Carbon

$$E_{VOC} = (238.8) (32,360) (60 \text{ min/hr}) (3.117 \times 10^{-8}) = 14.5 \text{ lb/hr as Carbon}$$

## **APPENDIX F**

### **Gas Cylinder Certification Sheets**

## CERTIFICATE OF ANALYSIS

### Grade of Product: EPA Protocol

Part Number: E02A199E15A00A6	Reference Number: 122-124323950-1
Cylinder Number: CC410934	Cylinder Volume: 146 Cu.Ft.
Laboratory: ASG - Durham - NC	Cylinder Pressure: 2015 PSIG
PGVP Number: B22012	Valve Outlet: 590
Gas Code: APPVD	Analysis Date: Jul 02, 2012

**Expiration Date: Jul 02, 2015**

Certification performed in accordance with "EPA Traceability Protocol (Sept. 1997)" using the assay procedures listed. Analytical Methodology does not require correction for analytical interferences. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.  
 Do Not Use This Cylinder below 150 psig, i.e. 1 Mega Pascal

ANALYTICAL RESULTS				
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty
PROPANE	28.00 PPM	27.99 PPM	G1	+/- 1% NIST Traceable
Air	Balance			

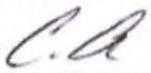
CALIBRATION STANDARDS				
Type	Lot ID	Cylinder No	Concentration	Expiration Date
NTRM	080610	CC263046	49.62PPM PROPANE/AIR	May 14, 2018

ANALYTICAL EQUIPMENT		
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Nicolet 6700 AHR0801333 C3H8	FTIR	Jun 19, 2012

Triad Data Available Upon Request

Notes: ANW PN: 781077



Approved for Release



Praxair Distribution Mid-Atlantic  
 145 Shimersville Rd.  
 Bethlehem, PA 18015  
 Tel: (610) 317-1608 Fax: (610) 758 8382  
 PGVP ID:

DocNumber: 000003740

## CERTIFICATE OF ANALYSIS / EPA PROTOCOL GAS

**Customer & Order Information:**

CHEROKEE INSTRUMENTS INC \*  
 901 BRIDGE ST  
 FUQUAY VARINA NC 275260

Praxair Order Number: 13003732  
 Customer P. O. Number: 10429  
 Customer Reference Number:

Fill Date: 4/7/2010  
 Part Number: EV AIPR60ME-AS  
 Lot Number: 917009747  
 Cylinder Style & Outlet: AS CGA 590  
 Cylinder Pressure & Volume: 2000 psig 140 cu. ft.

**Certified Concentration:**

Expiration Date:	4/12/2018	NIST Traceable
Cylinder Number:	CC283143	Analytical Uncertainty:
50.0 ppm	PROPANE	± 1 %
Balance	AIR	

**Certification Information:** Certification Date: 4/12/2010 Term: 96 Months Expiration Date: 4/12/2018

This cylinder was certified according to the 1997 EPA Traceability Protocol, Document #EPA-600/R-97/121, using Procedure G1. Do Not Use this Standard if Pressure is less than 150 PSIG.

**Analytical Data:**

(R=Reference Standard, Z=Zero Gas, C=Gas Candidate)

1. Component: PROPANE

Requested Concentration: 50 ppm  
 Certified Concentration: 50.0 ppm  
 Instrument Used: VARIAN 3300 INST 023 (PROPANE)  
 Analytical Method: FID  
 Last Multipoint Calibration: 3/16/2010

Reference Standard Type: GMIS  
 Ref. Std. Cylinder #: CC182336  
 Ref. Std. Conc: 50.3 PPM  
 Ref. Std. Traceable to SRM #: 1668b  
 SRM Sample #: 82-J-49  
 SRM Cylinder #: XF003734B

First Analysis Data:		Date:	
Z: 0	R: 50.39	C: 49.84	Conc: 49.777
R: 50.36	Z: 0	C: 50.21	Conc: 50.147
Z: 0	C: 50.2	R: 50.34	Conc: 50.137
UOM: PPM	Mean Test Assay: 50.02 PPM		

Second Analysis Data:		Date:	
Z: 0	R: 0	C: 0	Conc: 0
R: 0	Z: 0	C: 0	Conc: 0
Z: 0	C: 0	R: 0	Conc: 0
UOM: PPM	Mean Test Assay: 0 PPM		

Analyzed by:

*Meegha Patel for*  
 John Pribish

Certified by:

*Robin Morgan*  
 Robin Morgan

Information contained herein has been prepared at your request by qualified experts within Praxair Distribution, Inc. While we believe that the information is accurate within the limits of the analytical methods employed and is complete to the extent of the specific analyses performed, we make no warranty or representation as to the suitability of the use of the information for any purpose. The information is offered with the understanding that any use of the information is at the sole discretion and risk of the user. In no event shall the liability of Praxair Distribution, Inc., arising out of the use of the information contained herein exceed the fee established for providing such information.

## CERTIFICATE OF ANALYSIS

### Grade of Product: EPA Protocol

Part Number: E02AI99E15A3227	Reference Number: 122-124370084-1
Cylinder Number: SG9164792BAL	Cylinder Volume: 146.2 CF
Laboratory: ASG - Durham - NC	Cylinder Pressure: 2015 PSIG
PGVP Number: B22013	Valve Outlet: 590
Gas Code: PPN	Certification Date: Apr 17, 2013

**Expiration Date: Apr 17, 2021**

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS					
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
PROPANE	86.00 PPM	86.13 PPM	G1	+/- 1% NIST Traceable	04/17/2013
AIR	Balance				

CALIBRATION STANDARDS					
Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
NTRM	09061735	CC304058	97.82 PPM PROPANE/AIR	+/- 0.5%	Oct 02, 2013

ANALYTICAL EQUIPMENT		
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Nicolet 6700 AHR0801333 C3H8	FTIR	Mar 20, 2013

Triad Data Available Upon Request

Notes:

Approved for Release



Praxair Distribution Mid-Atlantic  
 145 Shimersville Rd.  
 Bethlehem, PA 18015  
 Telephone: (610) 317-1608  
 Facsimile: (610) 758-8382

DocNumber: 000007981

## CERTIFICATE OF ANALYSIS / EPA PROTOCOL GAS

**Customer & Order Information:**

CHEROKEE INSTRUMENTS INC \*  
 901 BRIDGE ST  
 FUQUAY VARINA NC 275260

Praxair Order Number: 15303079  
 Customer P. O. Number: 11036  
 Customer Reference Number:

FBI Date: 12/8/2010  
 Part Number: AI PR260ZE-AS  
 Lot Number: 917034266  
 Cylinder Style & Outlet: AS CGA 590  
 Cylinder Pressure & Volume: 2000 psig 140 cu. ft.

**Certified Concentration:**

Expiration Date:	12/13/2013	NIST Traceable
Cylinder Number:	CC109519	Analytical Uncertainty:
258.1 ppm	PROPANE	± 1 %
Balance	AIR	

**Certification Information:** Certification Date: 12/13/2010 Term: 36 Months Expiration Date: 12/13/2013

This cylinder was certified according to the 1997 EPA Traceability Protocol, Document #EPA-600/R-97/121, using Procedure G1  
 Do Not Use this Standard if Pressure is less than 150 PSIG

**Analytical Data:**

(R=Reference Standard, Z=Zero Gas, C=Gas Candidate)

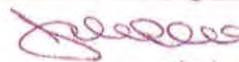
**1. Component: PROPANE**

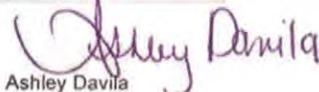
Requested Concentration: 260 ppm  
 Certified Concentration: 258.1 ppm  
 Instrument Used: VARIAN 3300 INST 023 (PROPANE)  
 Analytical Method: FID  
 Last Multipoint Calibration: 11/19/2010

Reference Standard Type: GMIS  
 Ref. Std. Cylinder #: CC138736  
 Ref. Std. Conc: 499.9 PPM  
 Ref. Std. Traceable to SRM #: 1669b  
 SRM Sample #: 81-H-14  
 SRM Cylinder #: XF004157b

First Analysis Data:		Date:	
Z:	0	R:	501.2
C:	258.6	Conc:	258.07
R:	501.4	Z:	0
C:	258.5	Conc:	257.97
Z:	0	R:	500.2
C:	258.7	Conc:	258.17
UOM:	PPM	Mean Test Assay:	258.07 PPM

Second Analysis Data:		Date:	
Z:	0	R:	0
C:	0	Conc:	0
R:	0	Z:	0
C:	0	Conc:	0
Z:	0	R:	0
C:	0	Conc:	0
UOM:	PPM	Mean Test Assay:	0 PPM

Analyzed by:   
 John Pribish 12/28/10

Certified by:   
 Ashley Davila

Information contained herein has been prepared at your request by qualified experts within Praxair Distribution, Inc. While we believe that the information is accurate within the limits of the analytical methods employed and is complete to the extent of the specific analyses performed, we make no warranty or representation as to the suitability of the use of the information for any purpose. The information is offered with the understanding that any use of the information is at the sole discretion and risk of the user. In no event shall the liability of Praxair Distribution, Inc., arising out of the use of the information contained herein exceed the fee established for providing such information.



Praxair Distribution Mid-Atlantic  
 145 Shimersville Rd.  
 Bethlehem, PA 18015  
 Telephone: (610) 317-1608  
 Facsimile: (610) 758-8382

DocNumber: 000009995

## CERTIFICATE OF ANALYSIS / EPA PROTOCOL GAS

**Customer & Order Information:**

CHEROKEE INSTRUMENTS INC \*  
 901 BRIDGE ST  
 FUQUAY VARINA NC 275260

Praxair Order Number: 16230993  
 Customer P. O. Number: 11207  
 Customer Reference Number:

Fill Date: 3/17/2011  
 Part Number: EV AIPR500ME-AS  
 Lot Number: 917117666  
 Cylinder Style & Outlet: AS CGA 590  
 Cylinder Pressure & Volume: 2000 psig 140 cu. ft.

**Certified Concentration:**

Expiration Date:	3/21/2014	NIST Traceable
Cylinder Number:	SA20675	Analytical Uncertainty:
507.1 ppm	PROPANE	± 1 %
Balance	AIR	

**Certification Information:** Certification Date: 3/21/2011 Term: 36 Months Expiration Date: 3/21/2014

This cylinder was certified according to the 1997 EPA Traceability Protocol, Document #EPA-600/R-97/121, using Procedure G1  
 Do Not Use this Standard if Pressure is less than 150 PSIG

**Analytical Data:**

(R=Reference Standard, Z=Zero Gas, C=Gas Candidate)

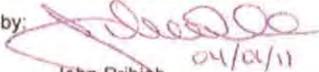
**1. Component: PROPANE**

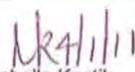
Requested Concentration: 500 ppm  
 Certified Concentration: 507.1 ppm  
 Instrument Used: VARIAN 3300 INST 023 (PROPANE)  
 Analytical Method: FID  
 Last Multipoint Calibration: 3/16/2011

Reference Standard Type: GMIS  
 Ref. Std. Cylinder #: CC103865  
 Ref. Std. Conc: 749.3 PPM  
 Ref. Std. Traceable to SRM #: 2646a  
 SRM Sample #: 103-C-23  
 SRM Cylinder #: XF000820B

First Analysis Data:		Date:	3/21/2011
Z: 0	R: 749.9	C: 508.2	Conc: 507.86
R: 749.1	Z: 0	C: 507.2	Conc: 506.86
Z: 0	C: 506.8	R: 750.4	Conc: 506.46
UOM: PPM	Mean Test Assay:		507.06 PPM

Second Analysis Data:		Date:	
Z: 0	R: 0	C: 0	Conc: 0
R: 0	Z: 0	C: 0	Conc: 0
Z: 0	C: 0	R: 0	Conc: 0
UOM: PPM	Mean Test Assay:		0 PPM

Analyzed by:   
 John Pribish 04/01/11

Certified by:   
 Michelle Kostik

Information contained herein has been prepared at your request by qualified experts within Praxair Distribution, Inc. While we believe that the information is accurate within the limits of the analytical methods employed and is complete to the extent of the specific analyses performed, we make no warranty or representation as to the suitability of the use of the information for any purpose. The information is offered with the understanding that any use of the information is at the sole discretion and risk of the user. In no event shall the liability of Praxair Distribution, Inc., arising out of the use of the information contained herein exceed the fee established for providing such information.

## CERTIFICATE OF ANALYSIS

### Grade of Product: EPA Protocol

**Airgas Specialty Gases**  
 630 United Drive  
 Durham, NC 27713  
 919-544-3773 Fax: 919-544-3774  
 www.airgas.com

Part Number: E02AI99E15A0333	Reference Number: 122-124344171-1
Cylinder Number: CC148274	Cylinder Volume: 146 Cu.Ft.
Laboratory: ASG - Durham - NC	Cylinder Pressure: 2015 PSIG
PGVP Number: B22012	Valve Outlet: 590
Gas Code: APPVD	Analysis Date: Nov 05, 2012

**Expiration Date: Nov 05, 2020**

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS				
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty
PROPANE	850.0 PPM	836.9 PPM	G1	+/- 1% NIST Traceable
Air	Balance			

CALIBRATION STANDARDS				
Type	Lot ID	Cylinder No	Concentration	Expiration Date
NTRM	110609	CC343416	1000.3PPM PROPANE/NITROGEN	Mar 04, 2017

ANALYTICAL EQUIPMENT		
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Nicolet 6700 AHR0801333 C3H8	FTIR	Oct 11, 2012

Triad Data Available Upon Request

Notes: ANW PN: 781018



Approved for Release



Air Liquide America  
Specialty Gases LLC



# CERTIFIED WORKING CLASS

*Single-Certified Calibration Standard*

6141 EASTON ROAD, BLDG 1, PLUMSTEADVILLE, PA 18949-0310

Phone: 800-331-4953 Fax: 215-766-7226

## CERTIFICATE OF ACCURACY: Certified Working Class Calibration Standard

### Product Information

Document # : 46628943-001  
Item No.: MM301080-T-30AL  
P.O. No.: 06081203

Cylinder Number: ALM018055  
Cylinder Size: 30AL  
Certification Date: 21Jun2012  
Expiration Date: 21Jun2014  
Lot Number: PLU0109851

### Customer

ENTHALPY ANAYTICAL, INC.  
06081203  
800-1 CAPITOLA DRIVE  
DURHAM, NC 27703  
US

## CERTIFIED CONCENTRATION

<u>Component Name</u>	<u>Concentration (Moles)</u>	<u>Accuracy (+/-%)</u>
METHANOL	105. PPM	5
SULFUR HEXAFLUORIDE	3.0 PPM	5
NITROGEN	BALANCE	

## TRACEABILITY

### Traceable To

Scott Reference Standard

APPROVED BY:

  
DAVID ASHNOFF

DATE:

6-21-2012

## CERTIFICATE OF ANALYSIS

**Grade of Product: CERTIFIED STANDARD-SPEC**

Part Number: X03NI99C15A1FX5  
Cylinder Number: CC90659  
Laboratory: ASG - Port Allen - LA  
Analysis Date: Sep 30, 2013  
Lot Number: 83-124390037-1A

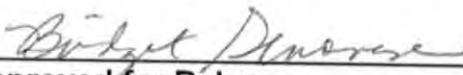
Reference Number: 83-124390037-1A  
Cylinder Volume: 144.4 CF  
Cylinder Pressure: 2015 PSIG  
Valve Outlet: 350S

Product composition verified by direct comparison to calibration standards traceable to N.I.S.T. weights and/or N.I.S.T. Gas Mixture reference materials.

### ANALYTICAL RESULTS

Component	Requested Concentration	Actual Concentration (Mole %)	Analytical Uncertainty
SULFUR HEXAFLUORIDE	3.000 PPM	3.127 PPM	+/- 5%
METHANOL	100.0 PPM	91.71 PPM	+/- 2%
NITROGEN	Balance		

Notes:

  
Approved for Release

## CERTIFICATE OF ANALYSIS

**Grade of Product: CERTIFIED STANDARD-SPEC**

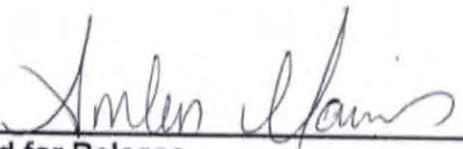
Part Number:	X02NI99C15A1268	Reference Number:	122-124373993-1
Cylinder Number:	CC432538	Cylinder Volume:	144.4 CF
Laboratory:	ASG - Durham - NC	Cylinder Pressure:	2015 PSIG
Analysis Date:	May 08, 2013	Valve Outlet:	350
Lot Number:	122-124373993-1		

Product composition verified by direct comparison to calibration standards traceable to N.I.S.T. weights and/or N.I.S.T. Gas Mixture reference materials.

### ANALYTICAL RESULTS

Component	Requested Concentration	Actual Concentration (Mole %)	Analytical Uncertainty
ETHYLENE	100.0 PPM	99.88 PPM	+/- 2%
NITROGEN	Balance		

Notes:

  
Approved for Release

## **APPENDIX F**

### **Equipment Calibration Sheets**

**APEX INSTRUMENTS METHOD 5 POST-TEST CONSOLE CALIBRATION  
USING CALIBRATED CRITICAL ORIFICES  
3-POINT ENGLISH UNITS**

Meter Console Information	
Console Model Number	522
Console Serial Number	909033
DGM Model Number	RW 110
DGM Serial Number	961167

Calibration Conditions			
Date	Time	10/23/13	1030
Barometric Pressure		29.46	in Hg
Theoretical Critical Vacuum <sup>1</sup>		13.91	in Hg
Calibration Technician		TTB	

Factors/Conversions		
Std Temp	528	°R
Std Press	29.92	in Hg
K <sub>1</sub>	17.647	oR/in Hg

<sup>1</sup>For valid test results, the Actual Vacuum should be 1 to 2 in. Hg greater than the Theoretical Critical Vacuum shown above.

<sup>2</sup>The Critical Orifice Coefficient, K', must be entered in English units, (ft<sup>3</sup>\*°R<sup>1/2</sup>)/(in.Hg\*min).

Calibration Data										
Run Time	Metering Console				Critical Orifice					
Elapsed	DGM Orifice ΔH	Volume Initial	Volume Final	Outlet Temp Initial	Outlet Temp Final	Serial Number	Coefficient	Amb Temp Initial	Amb Temp Final	Actual Vacuum
(θ)	(P <sub>m</sub> )	(V <sub>m</sub> )	(V <sub>m</sub> )	(t <sub>m</sub> )	(t <sub>m</sub> )	FO55	K'	(t <sub>amb</sub> )	(t <sub>amb</sub> )	
min	in H <sub>2</sub> O	cubic feet	cubic feet	°F	°F	FO55	see above <sup>2</sup>	°F	°F	in Hg
16.0	1.20	637.000	646.659	62	63	FO55	0.4594	63	65	19.00
13.0	1.20	647.000	654.859	64	64	FO55	0.4594	65	65	19.00
13.0	1.20	655.100	662.965	64	65	FO55	0.4594	65	66	19.00

Results								
Standardized Data				Dry Gas Meter				
Dry Gas Meter		Critical Orifice		Calibration Factor		Flowrate	ΔH @	
(V <sub>m(Std)</sub> )	(Q <sub>m(Std)</sub> )	(V <sub>Cr(Std)</sub> )	(Q <sub>Cr(Std)</sub> )	Value	Variation	Std & Corr	0.75 SCFM	Variation
(cubic feet)	(cfm)	(cubic feet)	(cfm)	(Y)	(ΔY)	(Q <sub>m(Std)(Corr)</sub> )	(ΔH@)	(ΔΔH@)
						(cfm)	(in H <sub>2</sub> O)	
9.639	0.602	9.460	0.591	0.981	0.000	0.591	1.934	0.001
7.821	0.602	7.679	0.591	0.982	0.000	0.591	1.933	-0.001
7.819	0.601	7.675	0.590	0.982	0.000	0.590	1.933	-0.001
<b>Pretest Gamma</b>	0.9828	<b>% Deviation</b>	0.1	0.982	Y Average		1.933	ΔH@ Average

Note: For Calibration Factor Y, the ratio of the reading of the calibration meter to the dry gas meter, acceptable tolerance of individual values from the average is +/-0.02.

I certify that the above Dry Gas Meter was calibrated in accordance with USEPA Methods, CFR Title 40, Part 60, Appendix A-3, Method 5, 16.2.3

Signature \_\_\_\_\_ Todd Brozell

Date \_\_\_\_\_ 10/23/2013

**GENERAL INFORMATION**

Probe ID	4H	Personnel	DLS
Date	9/21/2011	Coefficient Value	0.84

**PITOT TUBE INSPECTION**

Pitot Tube assembly level? (yes/no)	yes
Pitot Tube obstruction? (yes/no)	no
Pitot Tube openings damaged? (yes/no)	no

$\alpha_1$	1.4	$\leq \pm 10^\circ$
$\alpha_2$	0.4	$\leq \pm 10^\circ$
$\beta_1$	1.9	$\leq \pm 5^\circ$
$\beta_2$	1.2	$\leq \pm 5^\circ$
$\gamma$	2.9	
$\theta$	0.2	
$z = A \tan(\gamma)$	0.049	$\leq \pm 1/8''$
$\omega = A \tan(\theta)$	0.003	$\leq \pm 1/32''$
$D_t$	0.375	$(3/16'' < D_t < 3/8'' \text{ Recommended})$
A	0.9375	
$P_A$		
$P_B$	1.29	$(1.05 < P/D_t < 1.50 \text{ Recommended})$

**STACK THERMOCOUPLE CALIBRATION**

Ref. Type	Hg Thermometer	Ref. ID	Hg-1
-----------	----------------	---------	------

Source	Ref., °F	Stack TC, °F	Abs. Diff., °F
Ice bath	43	45	2
Ambient	75	75	0
Hot water	193	194	1
Maximum Temp. Difference, °F			2

**GENERAL INFORMATION**

Probe ID	6H	Personnel	DLS
Date	9/21/2011	Coefficient Value	0.84

**PITOT TUBE INSPECTION**

Pitot Tube assembly level? (yes/no)	yes
Pitot Tube obstruction? (yes/no)	no
Pitot Tube openings damaged? (yes/no)	no

$\alpha_1$	1.4	$\leq \pm 10^\circ$
$\alpha_2$	0.4	$\leq \pm 10^\circ$
$\beta_1$	1.9	$\leq \pm 5^\circ$
$\beta_2$	1.2	$\leq \pm 5^\circ$
$\gamma$	2.9	
$\theta$	0.2	
$z = A \tan(\gamma)$	0.049	$\leq \pm 1/8''$
$\omega = A \tan(\theta)$	0.003	$\leq \pm 1/32''$
$D_t$	0.375	$(3/16'' < D_t < 3/8'' \text{ Recommended})$
A	0.9375	
$P_A$		
$P_B$	1.29	$(1.05 < P/D_t < 1.50 \text{ Recommended})$

**STACK THERMOCOUPLE CALIBRATION**

Ref. Type	Hg Thermometer	Ref. ID	Hg-1
-----------	----------------	---------	------

Source	Ref., °F	Stack TC, °F	Abs. Diff., °F
Ice bath	43	45	2
Ambient	75	75	0
Hot water	193	192	1
Maximum Temp. Difference, °F			2