

AIR EMISSION TEST REPORT
Wiggins, Mississippi Wood Pellet Production Facility
Enviva Pellets Wiggins, LLC

Submitted to

Enviva Pellets Wiggins, LLC

Submitted by

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TABLE OF CONTENTS

1.	Summary	1
2.	Emission Test Program Description	3
	2.1 Wiggins, Mississippi Plant Description	3
	2.2 Purpose and Scope of the Emission Test Program	3
	2.3 Test Participants	4
3.	Test Matrix and Test Results	6
	3.1 Test Matrix	6
	3.2 Test Results	6
	3.3 Emission Data Evaluation	14
	3.4 VOC and HAP Emission Summary	16
4.	Sampling Locations	18
	4.1 Dryer 1 Stack Sampling Location	18
	4.2 Dryer 2 Stack Sampling Location	19
	4.3 Dry Hammermill 2 Cyclone Outlet Sampling Location	20
	4.4 Pellet Mill Aspiration System Sampling Location	21
	4.5 Pellet Cooler 2 Stack Sampling Location	22
	4.6 Pellet Cooler 1 Stack Sampling Location	23
	4.7 Green Hammermill Stack Sampling Location	24
5.	Testing Procedures	25
	5.1 Flue Gas Velocity and Volumetric Flow Rate – EPA Method 2	25
	5.2 Flue Gas Composition and Molecular Weight – EPA Method 3	25
	5.3 Flue Gas Moisture – EPA Method 4	25
	5.4 Total Hydrocarbon Concentrations – EPA Method 25A	25
	5.5 Organic HAPs – EPA Method 320	26
6.	Quality Assurance	28
	6.1 Method 1 Quality Assurance	28
	6.2 Method 4 Quality Assurance	28
	6.3 Method 25A Quality Assurance	28
	6.4 Method 320 Quality Assurance	33
7.	Process Documentation	35
8.	References	36
Appendices		
	A. Moisture and Gas Flow Rate Data	
	B. Method 25A Data	
	C. Method 320 Data	
	D. Method 320 Log Sheet	
	E. Example Calculations	
	F. Gas Cylinder Certification Sheets	
	G. Equipment Calibration Sheets	

TABLES

1-1.	Total Emissions at Plant Permit Limit of 185,550 ODT per Year	1
1-2	Total Emissions at Plant Permit Limit of 140,000 ODT per Year	2
3-1	Test Matrix, Air Emission Testing, Enviva Pellets Wiggins, MS	6
3-2	Green Hammermill Emission Test Results	7
3-3	Dryer 1 Emission Test Results	8
3-4	Pellet Cooler 1 Emission Test Results	9
3-5	Dryer 2 Emission Test Results	10
3-6	Dry Hammermill 2 Emission Test Results	11
3-7	Pellet Cooler 2 Emission Test Results	12
3-8	Aspiration System Emission Test Results	13
3-9	Alpha-Pinene Method 25A Response Factors	15
3-10	Calculated Method 25A Response Factors in Phase I Laboratory Tests	15
3-11.	Total Emissions at Plant Permit Limit of 185,550 ODT per Year	17
3-12	Total Emissions at Plant Permit Limit of 140,000 ODT per Year	17
6-1	Dryer 1 Quality Assurance Results, Total Hydrocarbons, Method 25A	29
6-2	Pellet Cooler 1 Quality Assurance Results, Total Hydrocarbons, Method 25A	29
6-3	Dryer 2 Quality Assurance Results, Total Hydrocarbons, High Range, Method 25A	30
6-4	Dryer 2 Quality Assurance Results, Total Hydrocarbons, Low Range, Method 25A	30
6-5	Dry Hammermill 2 Quality Assurance Results, Total Hydrocarbons, Method 25A	31
6-6	Pellet Cooler 2 Quality Assurance Results, Total Hydrocarbons, Method 25A	31
6-7	Aspiration System Quality Assurance Results, Total Hydrocarbons, Method 25A	32
6-8	Green Hammermill Quality Assurance Results, Total Hydrocarbons, Method 25A	32
6-9	CTS Results, Method 320	33
6-10	Spike Recovery Results, Method 320	34

FIGURES

4-1	Dryer 1 Stack Sampling Location	18
4-2	Photograph of the Dryer 1 Stack	18
4-3	Dryer 2 Stack Sampling Location	19
4-4	Photograph of the Dryer 2 Stack	19
4-5	Dry Hammermill 2 Sampling Location	20
4-6	Photograph of the Dry Hammermill 2 Sampling Location	20
4-7	Pellet Mill Aspiration System Sampling Location	21
4-8	Photograph of the Pellet Mill Aspiration System Sampling Location	21
4-9	Pellet Mill 2 Cooler Stack Sampling Location	22
4-10	Photograph of the Pellet Mill 2 Cooler Stack Sampling Location	22
4-11	Pellet Mill 1 Cooler Stack Sampling Location	23
4-12	Photograph of the Pellet Mill 1 Cooler Stack Sampling Location	23
4-13	Green Hammermill Stack Sampling Location	24
4-14	Photograph of the Green Hammermill Stack Sampling Location	24
5-1	Method 320 Organic HAP Sampling System	26

Definitions

Total Hydrocarbons	All organic compounds containing hydrogen and carbon that are detected by a flame ionization detector operated in accordance with U.S. EPA Method 25A.
Volatile Organic Compounds	All organic compounds that are emitted to the atmosphere in a gaseous or vapor form that can participate in photochemical reactions to produce ozone. All volatile organic compounds are considered VOCs unless specifically exempted in 40 CFR 51.100(s). Relevant excluded compounds include methane, ethane, and acetone.
VOC Emissions	Mass emissions of VOC measured on a pounds of carbon basis.

Acronyms

EPA	U.S. Environmental Protection Agency
FID	Flame Ionization Detector
FTIR	Fourier Transform Infrared Spectrometer
HAP	Hazardous Air Pollutant
MC	Moisture Content
MDEQ	Mississippi Department of Environmental Quality
ODT	Oven Dried Tons
THC	Total Hydrocarbons
VOC	Volatile Organic Compounds
C1	Carbon

Units of Measure

ppm	Parts per million (wet basis)
ppmvd	Parts per million (dry basis)
ppm C ₃	Parts per million as propane
ppm C ₁	Parts per million as carbon
mg	Milligram
kg	Kilogram
µg	Micrograms

Permit Designations/Titles

Dryer 1	AA-001, 30 MMBTU Wood-Fired Dryer (No. 1) with a Multiclone
Dryer 2	AA-002, 45 MMBTU Wood Fired Dryer (No. 2) with a Cyclone
Dry Hammermill 1	AA-006, No. 1 Secondary Hammermill w/High-Eff. Cyclone
Dry Hammermill 2	AA-007, No. 2 Secondary Hammermill w/High-Eff. Cyclone
Pellet Cooler 1	AA-004, Includes Line 1 Press Aspiration (AA-012)
Pellet Cooler 2	AA-014, Pellet Cooler 2 w/Hi-Efficiency Cyclone
Aspiration System	AA-013, Line 2 Pellet Mill Aspiration System
Green Hammermill	AA-016 (Hammermill Bin)

Air Emission Test Report Wiggins, Mississippi Wood Pellet Production Facility

1. SUMMARY

Enviva Pellets, Wiggins, LLC (Enviva) has sponsored air emission testing to satisfy the requirements of Agreed Order 6366-13 dated June 16, 2013 (the “Order”). These test results are being submitted to the Mississippi Department of Environmental Quality (MDEQ) by October 31, 2013 in accordance with the Order.

The scope of the testing program included volatile organic compounds (VOCs) and six organic hazardous air pollutants (HAPs). Annual emissions of each analyte have been calculated and compared to applicable permit limits. The results of the testing program are summarized in Table 1-1 based on the present maximum permitted production limit of 185,550 ODT per year in the permit.

Table 1-1. Total Emissions at Plant Permit Limit of 185,550 ODT/Year									
Analyte	Dryer 1	Dryer 2	Dry Hammermill 2	Green Hammermill	Pellet Cooler 1	Pellet Cooler 2	Aspirator	Dry Hammermill 1	Total
Total VOC	66.3	57.6	11.1	21.1	15.7	7.8	46.4	7.4	233.5
Organic HAPs									
Methanol	1.85	7.26	0.08	0.27	0.16	0.24	0.34	0.05	10.3
Acetaldehyde	0.00	1.40	0.25	0.61	0.39	0.35	0.23	0.17	2.0
Acrolein	1.03	2.32	0.43	1.24	0.77	0.68	0.20	0.29	7.0
Formaldehyde	2.01	3.48	0.39	0.37	0.49	0.34	0.03	0.26	7.4
Phenol	0.00	0.00	0.00	0.00	0.39	0.00	0.00	0.00	0.4
Propionaldehyde	1.06	1.82	0.17	0.09	0.16	0.11	0.00	0.11	3.5
Total HAPS	5.96	14.87	1.32	2.59	2.35	1.72	0.80	0.88	31.89

At the current maximum permitted production limit, VOC emissions remain below the PSD threshold of 250 tons per year. However, HAP emissions exceed the 25 ton per year threshold for major source classification, and methanol exceeds the 10 ton per year single compound threshold for major source classification. Importantly, the plant has never operated at the maximum permitted production limit of 185,550 ODT per year.

Enviva plans to propose to MDEQ a new maximum permitted production limit of 140,000 ODT/year. VOC and HAP emissions based on this proposed maximum permitted production limit are summarized in Table 1-2. Like the current limit of 185,000 ODT/year, to date, the Wiggins plant has also never achieved 140,000 ODT/year.

VOC emissions at the newly proposed production rate limit would be well below the PSD threshold of 250 tons per year. Furthermore, combined HAPs emissions are less than 25 tons per year, and none of the HAPs are emitted at more than 10 tons per year. Because the plant has never achieved a production rate of 140,000 ODT/year, the plant has never exceeded the major source threshold for VOCs or HAPs.

Table 1-2. Total Emissions at Plant Permit Limit of 140,000 ODT/Year									
Analyte	Dryer 1	Dryer 2	Dry Hammermill 2	Green Hammermill	Pellet Cooler 1	Pellet Cooler 2	Aspirator	Dry Hammermill 1	Total
Total VOC	50.1	43.4	8.4	15.9	11.7	5.9	35.0	5.6	175.9
Organic HAPs									
Methanol	1.40	5.48	0.06	0.21	0.12	0.18	0.26	0.04	7.7
Acetaldehyde	0.00	1.06	0.19	0.46	0.29	0.26	0.17	0.12	2.6
Acrolein	0.78	1.75	0.33	0.93	0.58	0.51	0.15	0.22	5.3
Formaldehyde	1.52	2.62	0.30	0.28	0.37	0.26	0.03	0.20	5.6
Phenol	0.00	0.00	0.00	0.00	0.29	0.00	0.00	0.00	0.3
Propionaldehyde	0.80	1.37	0.13	0.07	0.12	0.08	0.00	0.08	2.7
Total HAPS	4.50	12.28	0.99	1.95	1.78	1.30	0.61	0.66	24.06

These tests were conducted in accordance with the emission test protocol^[1] submitted to MDEQ on July 31, 2013. The scope of the emission test program was increased since submittal of the test program protocol in order to ensure that Enviva evaluated emissions from all possible sources of VOCs and HAPs.

The air emission tests were conducted by Air Control Techniques, P.C. using EPA Reference Methods 1, 2, 3, 4, 25A, and 320. The emission tests were conducted from Thursday, October 10 through Sunday, October 13, 2013. This report summarizes the emissions test data, quality assurance data, test method procedures, sampling equipment calibrations, process operating conditions, and test program participants.

2. EMISSION TEST PROGRAM DESCRIPTION

2.1 Wiggins, Mississippi Plant Description

Enviva operates a plant producing wood pellets. The plant consists of a wood receiving yard, log debarkers and chippers, two rotary dryers, two hammermills, two pellet presses and coolers, and an aspiration system. The plant processes wood composed of a range of hardwoods and softwoods.

2.2 Purpose and Scope of the Emission Test Program

Based on a voluntary self-evaluation, Enviva reported to the Mississippi Department of Environmental Quality (MDEQ) that it may have underreported emissions of volatile organic compounds (VOCs) in its permit application. Enviva's concern was based on a set of engineering-oriented tests^[2] conducted in November 2012 that indicated that VOC emissions from a hammermill source and a press cooler aspiration vent may be higher than previously known. While emissions from specific wood pellet plants are highly dependent on the specific equipment employed and to a lesser degree the hardwood/softwood mix of raw material, Enviva's preliminary findings in the November 2012 engineering test are generally consistent with other recent findings in the Wood Pellet Industry, specifically the engineering-oriented tests^[3] at a Georgia Biomass, Inc. plant in Waycross, Georgia and Green Circle Bio Energy in Cottondale, Florida.

This air emission testing program is intended to address Enviva's concern and fulfills the requirements of the Order. Specifically, Enviva agreed to generate VOC emissions data for the following sources.

- Dryer 1 multiclone stack
- Dryer 2 cyclone stack
- Secondary Hammermill 2 cyclone outlet
- Pellet Mill 2 Aspiration System

Since signing the Order, Enviva has determined that it would be beneficial to expand the scope of the emission testing program to include these three additional sources.

- Green Hammermill
- Pellet Cooler 1
- Pellet Cooler 2

The tests at Secondary Hammermill 2 cyclone outlet also represent emissions from Secondary Hammermill 1. Secondary Hammermill 2 is identical to Secondary Hammermill 1 except for the larger capacity of Secondary Hammermill 2.

2.3 Test Participants

The Enviva project manager for this project was Mr. Michael Doniger, Director of Plant Operations. He was assisted by Mr. Joe Harrell, Environmental Manager, Mr. Mike Jones, and Mr. Gary Williams, Wiggins Plant Manager.

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Legal counsel for Enviva is Mr. Alan McConnell. Mr. McConnell participated in this study to ensure that it addressed the requirements of the Order.

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Enviva retained Air Control Techniques, P.C. to conduct the air emission testing program at the Wiggins plant. The Air Control Techniques, P.C. project manager was John Richards, Ph.D., P.E., QSTI. He was assisted by David Goshaw, P.E., QSTI, Todd Brozell, P.E., QSTI, and Jonas Gilbert. Tom Holder, QSTI provided quality assurance services for the test program. Contact information for Air Control Techniques, P.C. includes the following.

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Enthalpy, Inc. provided the laboratory analyses of the samples. The Enthalpy project manager for this project was Mr. Bryan Tyler. He was assisted by Dr. Grant Plummer, Mr. Clint Thrasher, and Mr. Steve Eckert, President.

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3. TEST MATRIX AND TEST RESULTS

3.1 Test Matrix

Table 3-1 summarizes the test program analytes, sampling methods, and analytical methods used for the seven sources listed in Section 1.1

Table 3-1. Test Matrix, Air Emission Testing Enviva Pellets, Wiggins, Mississippi				
Analyte	Test Method	Number of Runs	Run Length	Analytical Method
Acetaldehyde, Acrolein, Formaldehyde, Methanol, Phenol, Propionaldehyde	EPA Method 320	3	60 min	FTIR
Gas Flow	EPA Method 2	3	60 min	Manometer
Gas Molecular Weight, Oxygen, Carbon Dioxide	EPA Method 3	3	60 min	Fyrite® Analyzer
Gas Moisture	EPA Method 4	3	60 min	Gravimetric
Total Hydrocarbons (THC)	EPA Method 25A	3	60 min	FID

The tests were conducted on Thursday, October 10 through Sunday October 13, 2013. During all of the tests, the plant operated with a 60% softwood/40% hardwood feed.

3.2 Test Results

The VOC and organic HAP test results and calculated annual emission rates are summarized in Tables 3-2 through 3-8. VOC and HAP emissions were measured simultaneously at each of the seven emission units tested.

The VOC emissions have been calculated based on the total hydrocarbon data provided by Method 25A. The Method 25A data have been converted from a wet to a dry basis to account for the moisture in the stack gas stream. Total hydrocarbon concentrations (THC) has been used as a surrogate for VOCs.

The VOC emission calculations do not include any corrections for methane, ethane, or acetone despite the fact that these compounds are detected by Method 25A but are not classified as VOCs. Accordingly, the reported VOC emissions are biased to higher-than-true levels to the extent that these three compounds affected the Method 25A results.

The Method 25A data reflect the combined THC concentrations consisting of (1) alpha and beta pinene, (2) numerous other terpenes such as limonene and 3-carene, and (3) the organic HAPs. The organic HAP emissions discussed later in this report are also classified as VOCs and represent a small fraction of the total VOC emissions reported.

Method 320 was used to measure six organic compounds. Several of the organic compounds were below the detection limits of Method 320 in this matrix of gaseous constituents. These non-detection concentrations are designated by shading in Tables 3-2 through 3-8.

Table 3-2. Green Hammermill ¹ Emission Test Results				
Parameter	Run 1	Run 2	Run 3	Average
Date	10/10/2013	10/10/2013	10/10/2013	N/A
Start	9:17	10:36	11:50	N/A
Stop	10:17	11:36	12:50	N/A
Throughput, tons/hour	36	36	36	36.0
Moisture Content Outlet, %wt.	47.15	47.15	47.15	47.2
Throughput, ODT/hour	19.026	19.026	19.026	19.0
ACFM	27,642	27,273	27,189	27,368.0
DSCFM	25,184	24,803	25,031	25,006
Stack Temperature, °F	70.8	70.6	70.9	70.8
O ₂ , %	20.9	20.9	20.9	20.9
% Moisture	3.41	3.62	2.37	3.1
VOC, ppmvd as Propane	31.9	33.4	27	30.8
VOC, ppmvd as C1	95.7	100.3	81.1	92.4
VOC, lbs/hour as C1	4.5	4.7	3.8	4.3
VOC, lbs/ODT	0.24	0.25	0.20	0.2
Methanol, ppmvd	0.53	0.48	0.39	0.46
Acetaldehyde, ppmvd	0.79	0.75	0.74	0.76
Acrolein, ppmvd	1.17	1.25	1.18	1.20
Formaldehyde, ppmvd	0.77	0.65	0.57	0.66
Phenol, ppmvd	0.91	0.91	0.90	0.91
Propionaldehyde, ppmvd	0.24	0.24	0.26	0.247
Methanol, lbs/hour	0.066	0.060	0.049	0.058
Acetaldehyde, lbs/hour	0.136	0.129	0.127	0.131
Acrolein, lbs/hour	0.257	0.274	0.259	0.263
Formaldehyde, lbs/hour	0.090	0.077	0.068	0.078
Phenol, lbs/hour	0.000	0.000	0.000	0.000
Propionaldehyde, lbs/hour	0.000	0.000	0.058	0.019
Methanol, lbs/ODT	0.003	0.003	0.002	0.003
Acetaldehyde, lbs/ODT	0.007	0.007	0.006	0.007
Acrolein, lbs/ODT	0.013	0.014	0.013	0.013
Formaldehyde, lbs/ODT	0.005	0.004	0.003	0.004
Phenol, lbs/ODT	0.000	0.000	0.000	0.000
Propionaldehyde, lbs/ODT	0.000	0.000	0.003	0.001

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Table 3-3. Dryer 1 Emissions ¹ Emission Test Results				
Parameter	Run 1	Run 2	Run 3	Average
Date	10/10/2013	10/11/2013	10/11/2013	N/A
Start	17:38	10:00	11:37	N/A
Stop	18:38	11:00	12:37	N/A
Throughput, tons/hour	8.5	8.45	9	8.7
Moisture Content Outlet, %wt.	15.5	14.36	18.9	16.3
Throughput, ODT/hour	7.18	7.24	7.30	7.2
ACFM	44,448	42,243	42,593	43,095
DSCFM	32,404	31,700	31,215	31,773
Stack Temperature, °F	146.3	150.1	147.3	147.9
O ₂ , %	19.0	17.0	17.0	17.7
% Moisture	16.07	12.79	15.23	14.7
VOC, ppmvd as Propane	79.5	71	67.4	72.6
VOC, ppmvd as C1	238.8	213.3	202.6	218.2
VOC, lbs/hour as C1	14.4	12.6	11.8	12.93
VOC, lbs/ODT	2.00	1.74	1.62	1.79
Methanol, ppmvd	3.00	1.95	1.88	2.28
Acetaldehyde, ppmvd	1.51	1.46	1.50	1.49
Acrolein, ppmvd	2.13	1.97	2.03	2.04
Formaldehyde, ppmvd	3.96	1.83	2.10	2.63
Phenol, ppmvd	2.43	2.34	2.41	2.39
Propionaldehyde, ppmvd	0.76	0.81	0.59	0.72
Methanol, lbs/hour	0.483	0.308	0.292	0.36
Acetaldehyde, lbs/hour	0.0	0.0	0.0	0.000
Acrolein, lbs/hour	0.598	0.0	0.0	0.199
Formaldehyde, lbs/hour	0.597	0.272	0.307	0.392
Phenol, lbs/hour	0.0	0.0	0.0	0.000
Propionaldehyde, lbs/hour	0.222	0.233	0.167	0.207
Methanol, lbs/ODT	0.067	0.043	0.040	0.050
Acetaldehyde, lbs/ODT	0.0	0.0	0.0	0.000
Acrolein, lbs/ODT	0.083	0.0	0.0	0.028
Formaldehyde, lbs/ODT	0.083	0.038	0.042	0.054
Phenol, lbs/ODT	0.0	0.0	0.0	0.000
Propionaldehyde, lbs/ODT	0.031	0.032	0.023	0.029

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Table 3-4. Pellet Cooler 1 ¹ Emission Test Results				
Parameter	Run 1	Run 2	Run 3	Average
Date	10/12/2013	10/12/2013	10/12/2013	N/A
Start	8:58	10:22	11:41	N/A
Stop	9:58	11:22	12:41	N/A
Throughput, tons/hour	4	4	4	4.0
Moisture Content Outlet, %wt.	7.9	7.9	7.9	7.9
Throughput, ODT/hour	3.68	3.68	3.68	3.68
ACFM	16,168	16,246	16,134	16,182.7
DSCFM	15,189	14,870	14,825	14,961
Stack Temperature, °F	82.3	94.8	97.7	91.6
O ₂ , %	20.9	20.9	20.9	20.9
% Moisture	3.35	3.68	2.79	3.27
VOC, ppmvd as Propane	40.4	34.6	36.7	37.2
VOC, ppmvd as C1	121.2	103.8	110.1	111.7
VOC, lbs/hour as C1	3.44	2.88	3.05	3.12
VOC, lbs/ODT	0.93	0.78	0.83	0.85
Methanol, ppmvd	0.56	0.34	0.36	0.42
Acetaldehyde, ppmvd	0.71	0.73	0.78	0.74
Acrolein, ppmvd	1.01	1.06	1.39	1.15
Formaldehyde, ppmvd	1.49	1.30	1.30	1.36
Phenol, ppmvd	1.03	1.02	1.01	1.02
Propionaldehyde, ppmvd	0.39	0.30	0.25	0.31
Methanol, lbs/hour	0.042	0.026	0.027	0.032
Acetaldehyde, lbs/hour	0.074	0.076	0.081	0.077
Acrolein, lbs/hour	0.135	0.141	0.184	0.153
Formaldehyde, lbs/hour	0.105	0.092	0.092	0.096
Phenol, lbs/hour	0.2	0.0	0.0	0.077
Propionaldehyde, lbs/hour	0.054	0.041	0.000	0.032
Methanol, lbs/ODT	0.011	0.007	0.007	0.009
Acetaldehyde, lbs/ODT	0.020	0.021	0.022	0.021
Acrolein, lbs/ODT	0.037	0.038	0.050	0.042
Formaldehyde, lbs/ODT	0.029	0.025	0.025	0.026
Phenol, lbs/ODT	0.063	0.000	0.0	0.021
Propionaldehyde, lbs/ODT	0.015	0.011	0.000	0.009

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Table 3-5. Dryer 2 ¹ Emission Test Results				
Parameter	Run 1	Run 2	Run 3	N/A
Date	10/13/2013	10/13/2013	10/13/2013	N/A
Start	9:21	11:14	12:31	N/A
Stop	10:21	12:52	13:47	N/A
Throughput, tons/hour	14.5	11.2	11.3	12.3
Moisture Content Outlet, %wt.	18.5	13.45	13.75	15.2
Throughput, ODT/hour	11.82	9.69	9.75	10.4
ACFM	24,998	25,318	25,278	25,198.0
DSCFM	14,745	15,224	14,842	14,937
Stack Temperature, °F	174.3	154.9	171.8	167.0
O ₂ , %	16.5	17	17	16.8
% Moisture	29.04	29.86	29.64	29.5
VOC, ppmvd as Propane	129.4	115.8	138.1	127.8
VOC, ppmvd as C1	388.2	347.4	414.3	383.3
VOC, lbs/hour as C1	10.70	9.88	11.49	10.69
VOC, lbs/ODT	0.91	1.02	1.18	1.03
Methanol, ppmvd	26.5	14.5	15.3	18.795
Acetaldehyde, ppmvd	1.4	4.7	1.4	2.498
Acrolein, ppmvd	2.7	3.7	3.5	3.303
Formaldehyde, ppmvd	9.0	9.4	9.6	9.336
Phenol, ppmvd	3.9	4.0	4.0	3.944
Propionaldehyde, ppmvd	3.3	2.0	2.4	2.575
Methanol, lbs/hour	1.949	1.070	1.129	1.383
Acetaldehyde, lbs/hour	0.138	0.473	0.147	0.253
Acrolein, lbs/hour	0.345	0.476	0.456	0.425
Formaldehyde, lbs/hour	0.622	0.647	0.662	0.644
Phenol, lbs/hour	0.0	0.0	0.0	0.000
Propionaldehyde, lbs/hour	0.445	0.262	0.322	0.343
Methanol, lbs/ODT	0.165	0.110	0.116	0.130
Acetaldehyde, lbs/ODT	0.012	0.049	0.015	0.025
Acrolein, lbs/ODT	0.029	0.049	0.047	0.042
Formaldehyde, lbs/ODT	0.053	0.067	0.068	0.062
Phenol, lbs/ODT	0.0	0.0	0.0	0.000
Propionaldehyde, lbs/ODT	0.038	0.027	0.033	0.033

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Table 3-6. Dry Hammermill 2 ¹ Emission Test Results				
Parameter	Run 1	Run 2	Run 3	Average
Date	10/11/2013	10/11/2013	10/11/2013	N/A
Start	18:11	19:35	20:48	N/A
Stop	19:11	20:35	21:48	N/A
Throughput, tons/hour	11.18	11.22	11.12	11.2
Moisture Content Outlet, %wt.	10.2	10.3	10.2	10.2
Throughput, ODT/hour	10.04	10.06	9.99	10.0
ACFM	15,197	14,385	15,165	14,916
DSCFM	13,183	12,366	13,303	12,951
Stack Temperature, °F	122.4	128.4	116.4	122.4
O ₂ , %	20.9	20.9	20.9	20.9
% Moisture	4.25	4.18	4.18	4.20
VOC, ppmvd as Propane	26.3	31.0	25.5	27.6
VOC, ppmvd as C1	78.9	93	76.5	82.8
VOC, lbs/hour as C1	1.94	2.15	1.90	2.00
VOC, lbs/ODT	0.19	0.21	0.19	0.20
Methanol, ppmvd	0.20	0.22	0.21	0.21
Acetaldehyde, ppmvd	0.75	0.74	0.74	0.74
Acrolein, ppmvd	1.02	1.02	1.01	1.02
Formaldehyde, ppmvd	1.09	1.19	1.16	1.14
Phenol, ppmvd	1.13	1.13	1.13	1.13
Propionaldehyde, ppmvd	0.24	0.25	0.27	0.254
Methanol, lbs/hour	0.013	0.014	0.014	0.014
Acetaldehyde, lbs/hour	0.067	0.067	0.000	0.045
Acrolein, lbs/hour	0.118	0.118	0.000	0.078
Formaldehyde, lbs/hour	0.067	0.073	0.071	0.071
Phenol, lbs/hour	0.000	0.000	0.000	0.000
Propionaldehyde, lbs/hour	0.029	0.030	0.032	0.030
Methanol, lbs/ODT	0.001	0.001	0.001	0.0014
Acetaldehyde, lbs/ODT	0.007	0.007	0.000	0.0045
Acrolein, lbs/ODT	0.012	0.012	0.000	0.0078
Formaldehyde, lbs/ODT	0.007	0.007	0.007	0.0070
Phenol, lbs/ODT	0.000	0.000	0.000	0.0000
Propionaldehyde, lbs/ODT	0.003	0.003	0.003	0.0030

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Table 3-7. Pellet Cooler 2 ¹ Emission Test Results				
Parameter	Run 1	Run 2	Run 3	Average
Date	10/11/2013	10/11/2013	10/11/2013	N/A
Start	13:43	15:08	16:39	N/A
Stop	14:43	16:08	17:39	N/A
Throughput, tons/hour	15.0	15.0	15.0	15.0
Moisture Content Outlet, %wt.	7.12	7.36	7.17	7.2
Throughput, ODT/hour	13.93	13.90	13.92	13.9
ACFM	13,252	12,718	12,831	12,934
DSCFM	10,938	10,543	10,488	10,656
Stack Temperature, °F	148.9	143.2	152.3	148.1
O ₂ , %	20.9	20.9	20.9	20.9
% Moisture	4.86	4.64	4.54	4.68
VOC, ppmvd as Propane	25.0	22.3	26.0	24.4
VOC, ppmvd as C1	75	66.9	78	73.3
VOC, lbs/hour as C1	1.53	1.32	1.53	1.46
VOC, lbs/ODT	0.11	0.09	0.11	0.10
Methanol, ppmvd	0.84	0.71	0.88	0.81
Acetaldehyde, ppmvd	0.90	0.87	0.83	0.87
Acrolein, ppmvd	1.36	1.27	1.39	1.34
Formaldehyde, ppmvd	1.12	0.69	1.93	1.25
Phenol, ppmvd	1.14	1.13	1.13	1.13
Propionaldehyde, ppmvd	0.26	0.26	0.38	0.30
Methanol, lbs/hour	0.046	0.039	0.048	0.044
Acetaldehyde, lbs/hour	0.068	0.065	0.062	0.065
Acrolein, lbs/hour	0.130	0.121	0.133	0.128
Formaldehyde, lbs/hour	0.058	0.035	0.099	0.064
Phenol, lbs/hour	0	0	0	0.000
Propionaldehyde, lbs/hour	0.026	0.000	0.037	0.021
Methanol, lbs/ODT	0.003	0.003	0.003	0.003
Acetaldehyde, lbs/ODT	0.005	0.005	0.004	0.005
Acrolein, lbs/ODT	0.009	0.009	0.010	0.009
Formaldehyde, lbs/ODT	0.004	0.003	0.007	0.005
Phenol, lbs/ODT	0.0	0.0	0.0	0.000
Propionaldehyde, lbs/ODT	0.002	0.000	0.003	0.002

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Table 3-8. Aspiration System ¹ Emission Test Results				
Parameter	Run 1	Run 2	Run 3	Average
Date	10/12/2013	10/12/2013	10/12/2013	N/A
Start	15:09	16:36	18:00	N/A
Stop	16:09	17:36	19:00	N/A
Throughput, tons/hour	15	15	15	15.0
Moisture Content Outlet, %wt.	7.12	8.83	7.85	7.93
Throughput, ODT/hour	13.93	13.68	13.82	13.8
ACFM	1,756	1,692	1,624	1,691
DSCFM	1,079	1,016	985	1,027
Stack Temperature, °F	148.6	148.3	152.1	149.7
O ₂ , %	20.9	20.9	20.9	20.9
% Moisture	27.67	29.33	28.19	28.4
VOC, ppmvd as Propane	1485.8	1354.2	1671.1	1,503.7
VOC, ppmvd as C1	4457.4	4062.6	5013.3	4,511.1
VOC, lbs/hour as C1	8.99	7.71	9.23	8.64
VOC, lbs/ODT	0.65	0.56	0.67	0.63
Methanol, ppmvd	11.5	12.6	11.4	11.81
Acetaldehyde, ppmvd	6.4	5.5	5.2	5.73
Acrolein, ppmvd	4.4	4.4	3.1	3.97
Formaldehyde, ppmvd	1.5	2.2	1.5	1.72
Phenol, ppmvd	3.8	3.9	3.8	3.81
Propionaldehyde, ppmvd	4.1	4.2	4.2	4.19
Methanol, lbs/hour	0.062	0.068	0.061	0.064
Acetaldehyde, lbs/hour	0.048	0.041	0.039	0.042
Acrolein, lbs/hour	0.041	0.042	0.030	0.037
Formaldehyde, lbs/hour	0.000	0.011	0.007	0.006
Phenol, lbs/hour	0.000	0.000	0.000	0.000
Propionaldehyde, lbs/hour	0.000	0.000	0.000	0.000
Methanol, lbs/ODT	0.004	0.005	0.004	0.005
Acetaldehyde, lbs/ODT	0.003	0.003	0.003	0.003
Acrolein, lbs/ODT	0.003	0.003	0.002	0.003
Formaldehyde, lbs/ODT	0.000	0.001	0.001	0.000
Phenol, lbs/ODT	0.000	0.000	0.000	0.000
Propionaldehyde, lbs/ODT	0.000	0.000	0.000	0.000

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

3.3 Emissions Data Evaluation

Method 25A VOC Concentrations

The VOC emissions from the various process units ranged from 0.10 to 1.79 pounds per ODT. VOC emissions were highest from the two dryers.

Dryer 1 had an emission rate of 1.79 pounds per ODT, and Dryer 2 had an emission rate of 1.03 pounds per ODT. This is equivalent to a 79% difference despite the fact that the dryers were handling similar hardwood/softwood blends and were generating wood with similar outlet moisture levels. The dryer outlet temperatures were also similar. These data clearly demonstrate that VOC emissions from the dryers are due to two factors: (1) the performance of the wood waste burner supplying the heat to the dryer, and (2) volatilization of VOCs from the wood in the dryer. Of these two sources, contributions of the burner are most important.

Due to the dominance of the burner in establishing the VOC emission rates from the combined burner/dryer source, the importance of the hardwood/softwood ratio is less important than previously thought. Changes in the hardwood/softwood ratio do not necessarily affect the VOC emissions from the burner.

The emissions of organic HAP compounds are not sensitive to the hardwood/softwood ratio. The data summarized in the Phase I report indicate that emissions of organic HAPs decreased slightly as the softwood content increased from 10% to 100%.

The data summarized in Tables 3-2 through 3-8 indicate that the total VOC emissions from the Wiggins Plant exceed 100 tons per year calculated as carbon. These tests confirm that the plant is a major source for VOCs.

The accuracy of the VOC data is demonstrated by a Method 25A response factor of approximately 1 for the group of compounds present in the gas stream. The Method 25A response is expressed in terms of a response factor that is defined as the observed Method 25A concentration divided by the true concentration. The Method 25A FID has a response factor close to 1.0 for a large set of organic compounds. Some high molecular weight organics have a response factor larger than 1, and in some cases, approaching 1.5. For these compounds, Method 25A is biased to higher-than-true concentrations. Some low molecular weight highly oxygenated organic compounds such as methanol and formaldehyde have very low response factors in the range of 0.1 to 0.4. For these compounds, Method 25A is biased to lower-than-true concentrations.

As part of the laboratory tests reported to MDEQ in Enviva's Phase I emission study dated July 31, 2013^[4] (the "Phase I Study"). Air Control Techniques, P.C. has taken the following two independent approaches in assessing the Method 25A response factors: (1) direct measurement of the Method 25A response factor using an alpha-pinene gas standard, the dominant organic compound measured during the laboratory tests and (2) a comparison of the Method 25A concentration data with the summed concentrations of all of the specific organics measured simultaneously using NCASI Method 98.01 and EPA Method 18. The results of these response factor analyses are presented in Tables 3-9 and 3-10.

Table 3-9. Alpha-Pinene Method 25A Response Factor ¹	
Alpha-Pinene Gas Standard, as C ₁₀ H ₁₆	259 ppm
Alpha-Pinene Gas Standard, as C ₃	863 ppm
FID Response, as C ₃	888 ppm
Response Factor as C ₃	1.03

1. Note: This table was included in the Phase I Study report to MDEQ.

Table 3-10. Calculated Method 25A Response Factors in Phase I Laboratory Tests ¹					
Run	Process Type	Softwood Content, %	Method 25A versus Combined NCASI 98.01 and Method 18	Dominant Compounds	Other Important Compounds
4	Dryer	10	0.72	α -and β -Pinene	Acetone, Methanol
5	Dryer	10	0.70	α -and β -Pinene	Acetone, Methanol
6	Dryer	10	0.75	α -and β -Pinene	Methanol, Formaldehyde
21	Dryer	10	1.23	α -and β -Pinene	Acetone, Methanol
22	Press	10	1.05	α -and β -Pinene	Acetone, Methanol
7	Dryer	70	0.85	α -and β -Pinene	Acetone
8	Dryer	70	0.90	α -and β -Pinene	Acetone
9	Dryer	70	1.02	α -and β -Pinene	Acetone
10	Dryer	70	0.91	α -and β -Pinene	Acetone
24	Press	70	1.51	α -and β -Pinene	Acetone, Methanol
11	Dryer	100	0.99	α -and β -Pinene	Acetone
12	Dryer	100	0.96	α -and β -Pinene	Acetone
13	Dryer	100	0.85	α -and β -Pinene	Acetone
14	Dryer	100	0.87	α -and β -Pinene	Acetone
16	Dryer	100	1.09	α -and β -Pinene	Methanol, Acetone
19	Dryer	100	1.21	α -and β -Pinene	Methanol, Acetone
20	Press	100	1.13	α -and β -Pinene	Methanol, Acetone
Test Program Average			0.98		

1. Note: This table was included in the Phase I Study report to MDEQ.

The excellent agreement between the Method 25A total concentration and the combined concentrations of all of the organics measured by NCASI 98.01 and EPA Method 18 demonstrate that Method 25A is an appropriate VOC measurement technique for wood pellet production facilities.

Method 320 HAP Concentrations

At the maximum permitted production limit of 185,550 ODT per year, five of the six organic HAP compounds measured by Method 320 were each emitted at a rate less than 10 tons per year. The methanol emission rate at this production level was 11.0 tons per year. The combined emission rate of all six organic HAPs was slightly over 31.1 tons per year at the maximum permitted production rate.

The list of HAPs specifically included in the test protocol included methanol, acetaldehyde, acrolein, formaldehyde, phenol, and propionaldehyde. This list was compiled based on (1) the organic compounds identified in laboratory analyses of pellet production facilities emissions, (2) previous emission tests conducted in the Pellet Manufacturing Industry, and (3) organic HAPs identified in studies of other wood products industries—specifically, MDF production.

The results of this test program indicate that this list of HAPs compounds needs to be amended. Phenol was detected at low concentration in only one of the tests of the seven process units. Furthermore, propionaldehyde was not detected in most of the tests.

The low to non-detectable phenol emissions data are consistent with the results of the Phase I Study. Phenol was not identified at detectable concentrations in any of the laboratory studies summarized in the Phase I Study report. The emission rates of phenol reported in the November 2012 Wiggins report ^[2] ranged from 0.0002 to 0.0018 pounds per hour—all insignificant emission rates. Phenol was also not listed in previous emission tests reviewed in preparation for this test program. Phenol was included in the test protocol primarily because other researchers such as Beauchemin and Tampier, ^[5] Milot, ^[6] and Milot and Mosher ^[7] listed phenol due to its inclusion in tests conducted at MDF and particleboard facilities. However, phenol emissions in MDF and particleboard production are due to the use of phenolic resins and similar binders. There is no reason to expect any appreciable phenol formation in pellet production considering (1) the lack of binders of any type in pellet production, (2) the higher moisture levels in pellet production as compared to MDF and particleboard processes, and (3) the lower material temperatures in pellet process equipment. Air Control Techniques, P.C. has assigned zero values to non-detected concentrations.

Acetaldehyde, propionaldehyde, and acrolein had very low concentrations in most of the emission tests summarized in this report. The IR absorption spectra of both water and the terpene compounds overlap the absorption spectra of acetaldehyde, propionaldehyde, and acrolein. Accordingly, the reported concentrations of these three compounds are biased to higher-than-true levels to the extent that this interference could not be avoided by Method 320 spectral absorption modeling. Zero values have been assigned when these concentrations were below detection limits of Method 320 due, in part, to the interference bias.

The use of zero values for non-detected compounds is an appropriate approach for any source, such as pellet production, where there are a few dominant compounds (i.e. methanol and formaldehyde) and a large number of possible compounds at extremely low levels such as phenol, acetaldehyde, and propionaldehyde. The use of non-detect or one-half non-detect concentrations in emission calculations for a large number of compounds potentially present at trace levels inherently makes any source “major” regardless of the actual emissions, size, or operations characteristics of the emission unit.

3.4 VOC and Organic HAP Emission Summary

Table 3-11 summarizes annual emissions of VOC and organic HAP compounds. The annual emission rates are based on operation at the permit limited production rate of 185,550 ODT.

As discussed, the plant has never operated at the maximum permitted production limit of 185,550 ODT per year. The VOC and HAP emissions based on the newly proposed maximum production rate of 140,000 ODT/year are summarized in Table 3-12.

The VOC emissions at the lower production rate are well below the PSD threshold of 250 tons per year. The combined HAPs emissions are less than 25 tons per year, and none of the HAPs are emitted at more than 10 tons per year. Accordingly, at this production limit, the plant is not above the major source threshold for HAPs.

Table 3-11. Total Emissions at Plant Permit Limit of 185,550 ODT/Year									
Analyte	Dryer 1	Dryer 2	Dry Hammermill 2	Green Hammermill	Pellet Cooler 1	Pellet Cooler 2	Aspirator	Dry Hammermill 1	Total
Total VOC	66.3	57.6	11.1	21.1	15.7	7.8	46.4	7.4	233.5
Organic HAPs									
Methanol	1.85	7.26	0.08	0.27	0.16	0.24	0.34	0.05	10.3
Acetaldehyde	0.00	1.40	0.25	0.61	0.39	0.35	0.23	0.17	2.0
Acrolein	1.03	2.32	0.43	1.24	0.77	0.68	0.20	0.29	7.0
Formaldehyde	2.01	3.48	0.39	0.37	0.49	0.34	0.03	0.26	7.4
Phenol	0.00	0.00	0.00	0.00	0.39	0.00	0.00	0.00	0.4
Propionaldehyde	1.06	1.82	0.17	0.09	0.16	0.11	0.00	0.11	3.5
Total HAPS	5.96	14.87	1.32	2.59	2.35	1.72	0.80	0.88	31.89

Table 3-12. Total Emissions at Plant Permit Limit of 140,000 ODT/Year									
Analyte	Dryer 1	Dryer 2	Dry Hammermill 2	Green Hammermill	Pellet Cooler 1	Pellet Cooler 2	Aspirator	Dry Hammermill 1	Total
VOC Total	50.1	43.4	8.4	15.9	11.7	5.9	35.0	5.6	175.9
Organic HAPs									
Methanol	1.40	5.48	0.06	0.21	0.12	0.18	0.26	0.04	7.7
Acetaldehyde	0.00	1.06	0.19	0.46	0.29	0.26	0.17	0.12	2.6
Acrolein	0.78	1.75	0.33	0.93	0.58	0.51	0.15	0.22	5.3
Formaldehyde	1.52	2.62	0.30	0.28	0.37	0.26	0.03	0.20	5.6
Phenol	0.00	0.00	0.00	0.00	0.29	0.00	0.00	0.00	0.3
Propionaldehyde	0.80	1.37	0.13	0.07	0.12	0.08	0.00	0.08	2.7
Total HAPS	4.50	12.28	0.99	1.95	1.78	1.30	0.61	0.66	24.06

4. SAMPLING LOCATIONS

4.1 Dryer # 1 Stack Sampling Location

The Dryer 1 sampling location meets EPA Method 1 location requirements as indicated in Figure 4-1. Twelve sampling points were used to measure the gas flow rate.

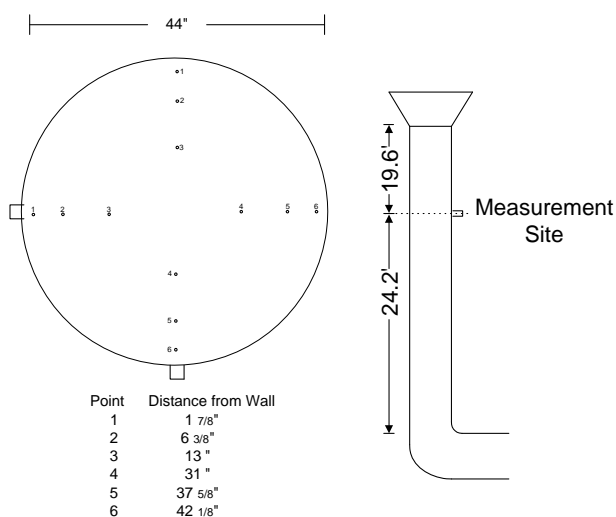


Figure 4-1 Dryer # 1 Stack Sampling Location

The downstream¹ flow disturbance is the stack discharge. The upstream flow disturbance is the duct from the fan entering the base of the stack.

During the sampling program, only the port facing south was used. The port facing east was blocked by the stack support equipment and the Dry Hammermill 1 ductwork. Test personnel reached all of the sampling ports by angling the probe inserted through the south port.

No cyclonic flow conditions were observed in the Dryer 1 stack. The point-by-point cyclonic flow checks indicated an average flow angle 3.1 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Dryer 1 stack is shown in Figure 4-2.



Figure 4-2. Photograph of the Dryer 1 Stack

¹ "Upstream" and "downstream" are defined based on the sampling location as the reference point.

4.2 Dryer 2 Stack Sampling Location

The Dryer 2 sampling location meets EPA Method 1 location requirements as indicated in Figure 4-2. Twelve sampling points were used to measure the gas flow rate.

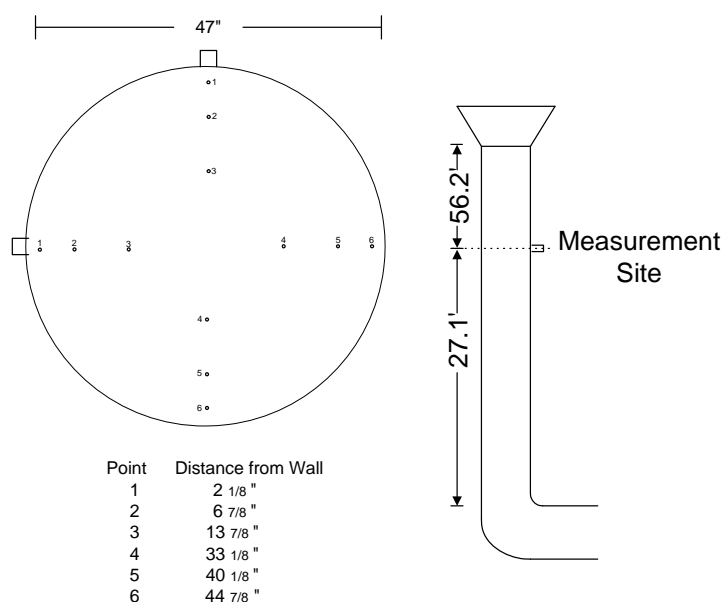


Figure 4-3. Dryer # 2 Stack Sampling Location

The downstream flow disturbance is the stack discharge. The upstream flow disturbance is the duct from the fan entering the base of the stack.

During the sampling program, only the port facing west was used in the test program. The port facing north could not be reached without potentially interrupting operation of the CEM sampling equipment. Test personnel reached all of the sampling ports by angling the probe inserted through the west port.

No cyclonic flow conditions were observed in the Dryer 2 stack. The point-by-point cyclonic flow checks indicated an average flow angle 2.4 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Dryer 2 stack is shown in Figure 4-4.



Figure 4-4. Photograph of the Dryer 2 Stack

4.3 Dry Hammermill 2 Cyclone Outlet Sampling Location

The Dry Hammermill 2 sampling location meets EPA Method 1 location requirements as indicated in Figure 4-5. Twelve sampling points were used to measure the gas flow rate.

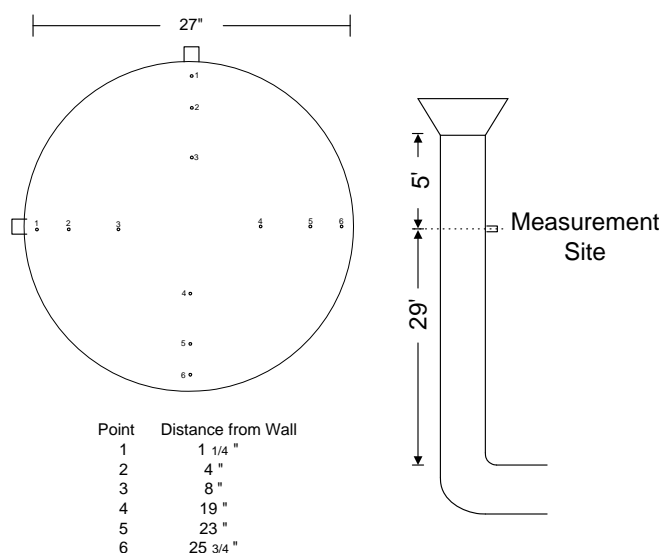


Figure 4-5. Dry Hammermill 2 Sampling Location

The downstream flow disturbance is an elbow in the fan outlet duct. The upstream flow disturbance is the fan discharge. During the sampling program both ports were accessible.

No cyclonic flow conditions were observed in the Dry Hammermill 2 stack. The point-by-point cyclonic flow checks indicated an average flow angle of 0.6 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Dry Hammermill 2 stack is shown in Figure 4-6.



Figure 4-6. Photograph of the Dry Hammermill 2 Sampling Location

4.4 Pellet Mill Aspiration System Sampling Location

The Pellet Mill Aspiration System has a six-inch diameter. Gas flow rate sampling was performed in general accordance with EPA Method 1A. The sampling port location met EPA Method 1 location requirements as indicated in Figure 4-7. A total of eight sampling points were used—four in a horizontal direction and four reached by an angled probe in the vertical direction. Due to the position of the duct and surrounding equipment, it was not possible to sample from any orientation except horizontal.

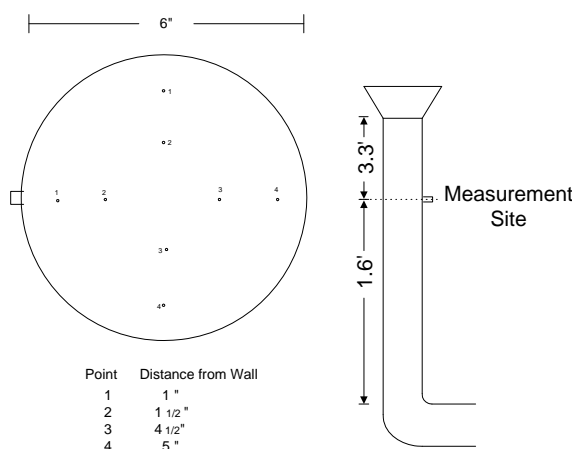


Figure 4-7. Pellet Mill Aspiration System Sampling Location

The upstream flow disturbance was an entry duct from Pellet Mill 6. The downstream flow disturbance was the fan inlet.

No cyclonic flow conditions were observed in the Pellet Mill Aspiration System outlet duct. The point-by-point cyclonic flow checks indicated an average flow angle of 0.75 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Pellet Mill Aspiration System sampling location is shown in Figure 4-8.



Figure 4-8. Photograph of the Pellet Mill Aspiration System Sampling Location

4.5 Pellet Mill 2 Cooler Stack Sampling Location

The Pellet Mill 2 Cooler stack sampling location meets the minimum requirements specified in Method 1, Section 11.1. As indicated in Figure 4-9, the downstream² disturbance (stack exit) is 0.6 stack diameters from the sampling location. The minimum allowed by Method 1 is 0.5 stack diameters. The upstream flow disturbance was the fan outlet duct. The distance to the upstream flow disturbance meets Method 1 requirements. Both sampling ports were used in the test program.

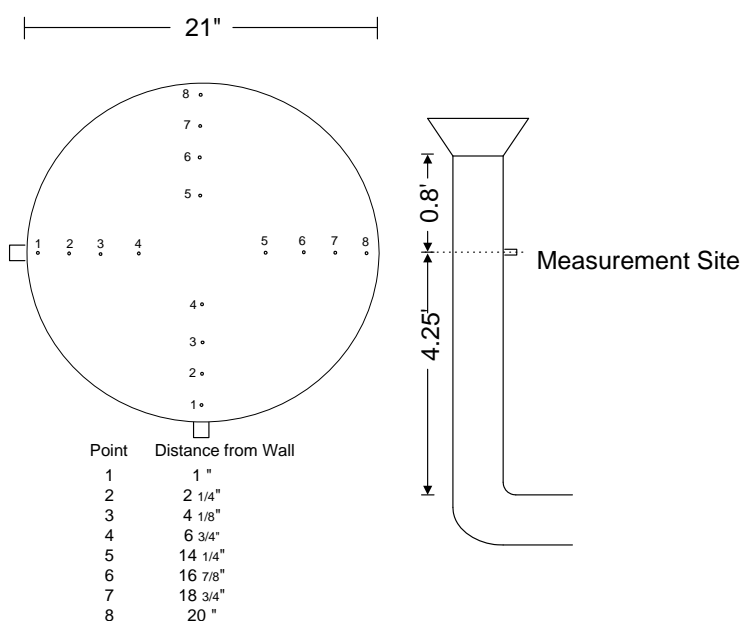


Figure 4-9. Pellet Mill 2 Cooler Stack Sampling Location

No cyclonic flow conditions were observed in the Pellet Mill 2 Cooler stack. The point-by-point cyclonic flow checks indicated an average flow angle of 1.5 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Pellet Cooler 2 stack is shown in Figure 4-10



Figure 4-10. Photograph of the Pellet Cooler 2 Stack

² The terms "upstream" and "downstream" are defined based on the test location as the reference point. A recent change in a figure in EPA Method 1 has these terms incorrectly stated.

4.6 Pellet Mill 1 Cooler Stack

The Pellet Mill 1 Cooler stack sampling location meets the minimum requirements specified in Method 1, Section 11.1. As indicated in Figure 4-11, the downstream disturbance (stack exit) is 0.6 stack diameters from the sampling location. The minimum allowed is 0.5 stack diameters. The upstream flow disturbance is the fan outlet duct. The distance to the upstream flow disturbance meets Method 1 requirements. Four of the six sampling ports were used in the test program. The plugs in two of the ports could not be removed.

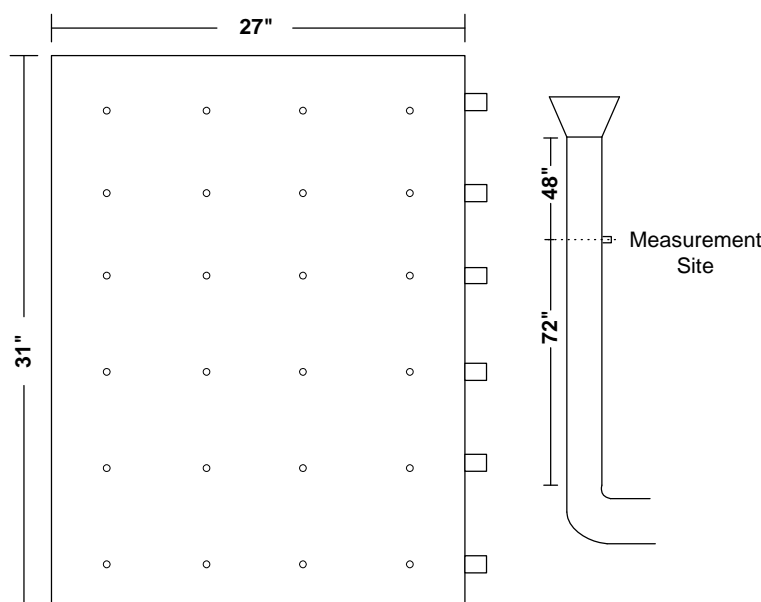


Figure 4-11. Pellet Mill 1 Cooler Stack Sampling Location

No cyclonic flow conditions were observed in the Pellet Mill 1 Cooler stack. The point-by-point cyclonic flow checks indicated an average flow angle of 2.0 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Pellet Mill 1 Cooler Stack is shown in Figure 4-12.



Figure 4-12. Photograph of the Pellet Mill 1 Cooler Stack

4.7 Green Hammermill Stack Sampling Location

The Green Hammermill stack sampling location shown in Figure 4-13 meets the minimum requirements for a downstream flow disturbance specified in Method 1, Section 11.1. The upstream flow disturbance is the fan outlet duct. The downstream flow disturbance is the stack discharge. The distance to the upstream flow disturbance meets Method 1 requirements. Only one sampling port could be reached safely. All of the sampling ports were reached by angling the Pitot tube inserted through the port facing south.

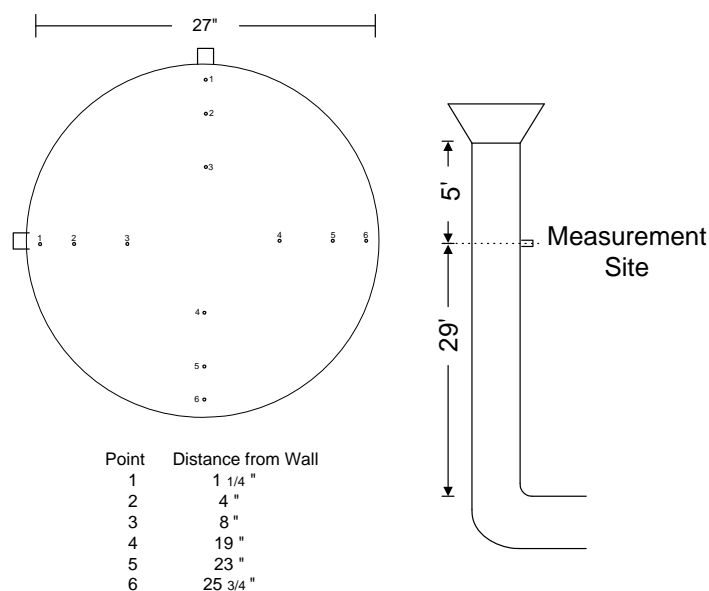


Figure 4-13. Green Hammermill Stack Sampling Location

No cyclonic flow conditions were observed in the Green Hammermill stack. The point-by-point cyclonic flow checks indicated an average flow angle of 1.7 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Green Hammermill stack is shown in Figure 4-14.



Figure 4-14. Photograph of the Green Hammermill Fan Inlet

5. TESTING PROCEDURES

5.1 Flue Gas Velocity and Volumetric Flow Rate - EPA Method 2

The flue gas velocities and volumetric flow rates during all of the emission tests were determined according to the procedures outlined in U.S. EPA Reference Method 2. Velocity measurements were made using S-Type Pitot tubes conforming to the geometric specifications outlined in Method 2. Accordingly, each Pitot was assigned a coefficient of 0.84. Velocity pressures were measured with fluid manometers. Effluent gas temperatures were measured with chromel-alumel thermocouples attached to digital readouts.

5.2 Flue Gas Composition and Molecular Weight - EPA Method 3

Flue gas analyses and calculation of flue gas dry molecular weights were performed in accordance with EPA Method 3. A stainless steel probe was inserted into the gas stream to collect a representative sample of the flue gas during each test run. The samples were analyzed using a Fyrite gas analyzer. Moisture was removed from the sample gas by means of a knockout jar located prior to the sample pump.

5.3 Flue Gas Moisture Content - EPA Method 4

The flue gas moisture content was determined in conjunction with each test run according to the sampling and analytical procedures outlined in EPA Method 4. Wet impinger sampling trains were used to withdraw and analyze the stack gas. The impingers were connected in series and contained water in the first two impingers followed by an empty impinger and then a silica gel impinger. The impingers were contained in an ice bath to assure condensation of the flue gas stream moisture. Any moisture that was not condensed in the impingers was captured in the silica gel; therefore, all moisture was weighed and entered into moisture content calculations.

5.4 Total Hydrocarbons – EPA Method 25A

Continuous emissions monitoring was conducted for volatile organic compounds. The sampling and analytical procedures for VOCs were conducted in accordance with EPA 25A. The CEM system consisted of a sample acquisition system, the THC emission monitor, and a data acquisition system (DAS). A California Analytical Model 300 flame ionization detector was used for the Method 25A tests.

The sample acquisition system included an in-stack probe, a heated out-of-stack glass mat filter for particulate matter removal, a heat-traced Teflon® sample line, a Teflon® heated-head pump, and a gas manifold board. All components of the sample acquisition system that contacted the sampled gas were constructed of Type 316 stainless steel or Teflon®. The sample gas was continuously extracted from a central point within the duct at a constant rate ($\pm 10\%$) for the duration of each test run. The wet, filtered gas was transported to a heated-head pump located at the CEM laboratory. The sample gas was sent directly to the VOC analyzer. Care was taken to ensure that the sample gas was greater than 250°F during transport from the stack to the VOC monitor. All pretest and posttest calibration procedures were performed as outlined in the EPA Reference Method 25A.

Total organic hydrocarbon concentrations were measured on a wet basis using a California Analytical 300 FID continuous emission monitor. The THC concentrations were monitored on a propane (C₃) basis using a flame ionization detector (FID). The FID was fueled by a gas mixture consisting of 40% helium and 60% hydrogen to reduce the effect of oxygen synergism. The

THC analyzer was calibrated with a set of at least four gas standards. Calibration tests were performed prior to and following each test run.

Outputs from the individual emission monitors were connected to a computerized data acquisition system. Outputs from the analyzer were sent to a portable computer via a National InstrumentsTM FieldPoint controller. The signals were downloaded to a STRATA[®] software program every two seconds. The two-second readings were averaged for the duration of the test run.

Total mass emissions of VOCs were determined based on the Method 25A total hydrocarbon concentration data. The mass emissions were expressed on a pounds mass of carbon per hour.

5.5 Organic HAP Compounds – EPA Method 320

Testing for wet-basis organic HAP concentrations was conducted by extractive Fourier transform infrared (FTIR) spectroscopy using EPA Method 320 (40CFR, Part 63, Appendix A). Sample gas was continuously passed through the sampling system, which included an in-stack probe, a heated out-of-stack glass mat filter for particulate matter removal, a Teflon[®] heat-traced sample line, a MIDAC Fourier Transform Infrared (FTIR) spectrometer, a Teflon[®] heated-head pump, and a gas manifold board as shown in Figure 5-1. All components of the sample acquisition system that contacted the sampled gas were Type 316 stainless steel or Teflon[®]. All components of the sampling system and the FTIR cell were maintained at or above 120° C. Air Control Techniques, P.C. took great care to ensure that the sampling system contained no “cold spots” to prevent organic HAP loss. The sampling rate was maintained at approximately 10 liters per minute.

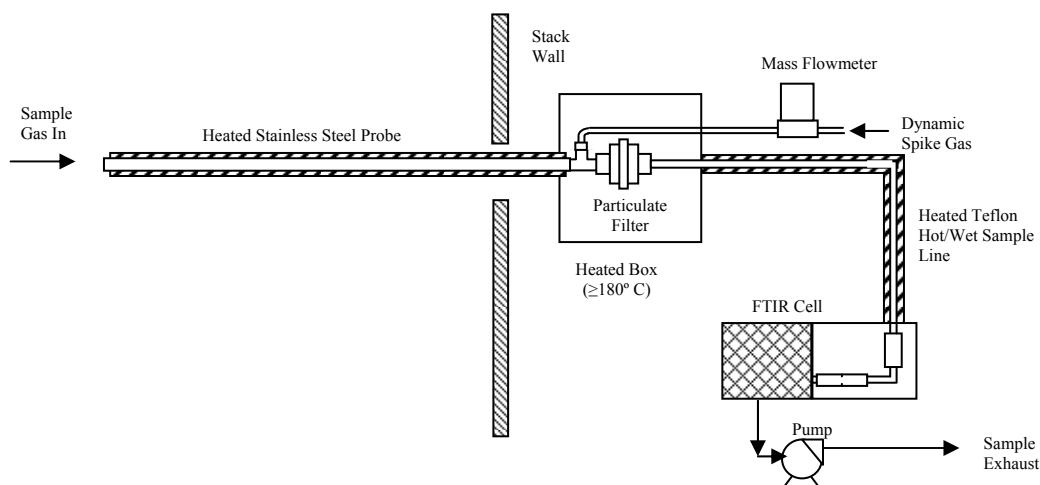


Figure 5-1. Method 320 Organic HAP Sampling System

The FTIR system included a MIDAC Corporation I-1301 spectrometer equipped with a heated, nominal 10-meter path absorption cell, a potassium bromide (KBr) beam splitter, zinc selenide (ZnSe) non-hygroscopic windows, and a liquid nitrogen-cooled Mercury Cadmium Telluride detector. Measurements were made using a MIDAC Model I-1301 high resolution Michelson interferometer with AutoQuant Pro software. Sample gas continuously passed through the sampling system, and sample spectra (based on 50 co-added interferograms) were recorded every

minute. The system's nominal spectral resolution was 0.5 cm^{-1} . Samples and standards were analyzed at temperatures greater than 120°C and near ambient pressures.

The inside walls of the cells were polished stainless steel to minimize interaction of the sample with the cell walls, and the cell mirrors were of bare gold. The gas pressure in the FTIR sample cell was monitored with a pressure transducer connected directly to the sample cell. The heated sample cell was wrapped in an insulating thermal jacket, and the temperature was controlled with type J thermocouples. The absorption cell volume was approximately 2 liters.

The FTIR system was operated via a portable computer, and a data archive storage system (USB Mass Storage Drive) was used for data backup. All interferograms, single beams, absorbance spectra, and background single beams were stored and have been archived. The filename, time, pressure and temperature of the sample cell, scan rate, background identification and other pertinent information was recorded by hand during the test program.

Air Control Techniques used the program AutoquantProTM Version 4.5.0.195, (©Midac Corporation, 2012) to collect and analyze all the infrared field data. The program allows the development and storage of analytical "methods" for analysis of spectral data (absorbance) files. The reference spectra used for these analyses were developed by MIDAC Corporation, EPA, and Enthalpy Analytical, Inc. One "model" was developed for determining the absorption path length and one additional "method" for determining the concentrations of the target compounds for each source.

The concentration uncertainty reported by AutoquantPro is called the Standard Error of the Estimated Concentration, or SEC; it is also known as the Marginal Standard Deviation. The uncertainties in the concentration are proportional to the square root of the sums of the squares of the residual. After the residual spectrum is obtained, which we will call R, the error variance for the case of a single reference spectrum is calculated as follows.

$$\sigma^2 = \frac{\sum_i R_i^2}{(n-1)}$$

Where n is the number of observations. The SEC is given by the following.

$$SEC = \frac{\sigma C}{\sqrt{\sum_i A_i^2}}$$

Where **A** is the spectrum and **C** is the known concentration of the reference.

The 95% confidence interval is 1.96 times the SEC.

6. QUALITY ASSURANCE

6.1 Method 1 Quality Assurance

All S-type Pitot tubes used in this project conformed to EPA guidelines concerning construction and geometry. Pitot tubes were inspected prior to use. Information pertaining to S-type Pitot tubes is presented in detail in Section 3.1.1 of EPA Publication No. 600/4-77-027b. Only S-type Pitot tubes meeting the required EPA specifications were used in this project.

The thermocouples used in this project were calibrated using the procedures described in Section 3.4.2 of EPA Publication No. 600/4-77-027b. Each temperature sensor was calibrated at a minimum of three points over the anticipated range of use against NIST-traceable mercury in glass thermometer.

6.2 Method 4 Quality Assurance

Pretest and posttest leak checks were conducted on each Method 4 sampling train used. The observed leak rates for the sampling trains were below 0.02 actual cubic feet per minute as required by Method 4.

All dry gas meters were fully calibrated to determine the volume correction factor prior to field use. Post-tests calibration checks were performed as soon as possible after the equipment was returned to the laboratory. Pre-and post-test calibrations agreed within ± 5 percent. The calibration procedure is documented in Section 3.3.2 of EPA Publication No. 600/4-77-237b.

The scales used at the test location to determine flue gas moisture content were calibrated using a standard set of weights.

6.3 Method 25A Quality Assurance

At the beginning of the test day, a linearity calibration test was performed on each analyzer. The continuous emission monitoring instrument response did not differ by more ± 5 from the propane calibration standard. Linearity results for the test program are provided in Table 6-1 through 6-8.

Prior to and following each test run, a system calibration test was performed. The system test was performed to verify that the sampling system did not contain leaks (system bias) and to measure a change in analyzer response during the test program (system drift). The system bias was less than $\pm 5\%$ of full-scale, and system drift was less than $\pm 3\%$ of full scale. System calibration results for the test program are provided in Tables 6-1 through 6-8.

Table 6-1. Dryer 1 Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.0		
Low, %	±5	0.4		
Mid, %	±5	2.2		
High, %	±5	0.0		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.8	0.1
Zero Bias (Post), %	±5	0.9	0.1	0.0
Up-scale Bias (Pre), %	±5	0.0	-0.2	-0.6
Up-scale Bias (Post), %	±5	0.1	-0.6	-1.0
Zero Drift, %	±3	0.9	-0.7	-0.2
Up-scale Drift, %	±3	0.1	-0.4	-0.4
Response Time, sec	N/A			

Table 6-2. Pellet Cooler 1 Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.1		
Low, %	±5	0.4		
Mid, %	±5	0.8		
High, %	±5	0.0		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.3	0.2
Zero Bias (Post), %	±5	0.3		0.3
Up-scale Bias (Pre), %	±5	0.1	-0.1	-0.1
Up-scale Bias (Post), %	±5	-0.1		0.3
Zero Drift, %	±3	0.3	-0.1	0.1
Up-scale Drift, %	±3	-0.1	0.0	-0.1
Response Time, sec	N/A			

Table 6-3. Dryer 2 Quality Assurance Results, Total Hydrocarbons, Method 25A, High Range				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.1		
Low, %	±5	0.3		
Mid, %	±5	-0.1		
High, %	±5	0.0		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.1	-0.1
Zero Bias (Post), %	±5	0.1	-0.1	-0.1
Up-scale Bias (Pre), %	±5	0.0	-0.3	-0.4
Up-scale Bias (Post), %	±5	-0.3	-0.4	-0.3
Zero Drift, %	±3	0.1	-0.1	0.0
Up-scale Drift, %	±3	-0.3	-0.1	0.1
Response Time, sec	N/A	28		

Table 6-4. Dryer 2 Quality Assurance Results, Total Hydrocarbons, Method 25A, Low Range				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±8	1.0		
Low, %	±8	1.5		
Mid, %	±8	0.7		
High, %	±8	0.1		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.6	-0.6
Zero Bias (Post), %	±5	0.6	-0.6	-0.7
Up-scale Bias (Pre), %	±5	0.0	0.3	0.1
Up-scale Bias (Post), %	±5	0.3	0.1	-0.1
Zero Drift, %	±3	0.6	-1.2	-0.1
Up-scale Drift, %	±3	0.3	-0.2	-0.2
Response Time, sec	N/A	28		

Table 6-5. Dry Hammermill 2 Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.0		
Low, %	±5	0.4		
Mid, %	±5	2.2		
High, %	±5	0.0		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.2	0.0	0.2
Zero Bias (Post), %	±5	0.0	0.2	0.2
Up-scale Bias (Pre), %	±5	-1.3	-1.1	-1.3
Up-scale Bias (Post), %	±5	-1.1	-1.3	-1.2
Zero Drift, %	±3	-0.1	0.1	0.0
Up-scale Drift, %	±3	0.2	-0.1	0.0
Response Time, sec	N/A	28		

Table 6-6 Pellet Cooler 2 Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0		
Low, %	±5	0.4		
Mid, %	±5	2.2		
High, %	±5	0.0		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.3	0.1
Zero Bias (Post), %	±5	0.3	0.1	0.2
Up-scale Bias (Pre), %	±5	-1.0	-0.9	-1.0
Up-scale Bias (Post), %	±5	-0.9	-1.0	-1.3
Zero Drift, %	±3	0.3	-0.2	0.0
Up-scale Drift, %	±3	0.1	-0.1	-0.3
Response Time, sec	N/A	28		

Table 6-7. Aspiration Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.1		
Low, %	±5	0.7		
Mid, %	±5	0.0		
High, %	±5	0.1		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.1	0.0
Zero Bias (Post), %	±5	0.1	0.0	0.1
Up-scale Bias (Pre), %	±5	0.0	-0.1	-0.1
Up-scale Bias (Post), %	±5	-0.1	-0.1	-0.3
Zero Drift, %	±3	0.1	-0.1	0.1
Up-scale Drift, %	±3	-0.1	0.1	-0.3
Response Time, sec	N/A	28		

Table 6-8. Green Hammermill Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.0		
Low, %	±5	1.1		
Mid, %	±5	1.6		
High, %	±5	0.4		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.1	0.1
Zero Bias (Post), %	±5	0.1	0.1	0.1
Up-scale Bias (Pre), %	±5	0.0	-0.1	-0.7
Up-scale Bias (Post), %	±5	-0.1	-0.7	-1.0
Zero Drift, %	±3	0.1	-0.1	0.1
Up-scale Drift, %	±3	-0.1	-0.5	-0.3
Response Time, sec	N/A	28		

6.4 Method 320 Quality Assurance

Air Control Techniques, P.C. performed daily quality assurance checks. Background scans and calibration transfer standard (CTS) spectra tests were performed prior to and following each test series. An analyte spike was performed using methanol.

The flow rate at the outlet of the pump was measured while the probe was plugged to verify that the sampling system was leaks. The flow rate was less than 200 ml/min.

The FTIR cell was tested for leaks by closing the value while the cell was at minimum absolute pressure.

Background Spectra

Sample spectra were divided point-by-point by a 128-scan background recorded using N₂. The single beam spectrum was constantly monitored, and a new background was generated approximately following each test series or when residual and absorbance spectra indicated component build-up on the optical surfaces or alignment-related baseline shifts.

Calibration Transfer Standards and Absorption Path Lengths

A cylinder of 100 ppm ethylene in nitrogen served as the CTS. A CTS gas was introduced to the FTIR and allowed to reach steady state. The CTS was used to determine effective cell path length based on comparisons of the “field” CTS spectra to a laboratory CTS spectrum recorded by MIDAC. As shown in Table 6-9, the maximum path length deviation was less than 5% of the average.

Table 6-9. CTS Results Summary							
Date	Time	CTS Scan (pathlength)	SEC (ppm)	Cell Press. (psi)	Cell Temp (deg C)	Deviation from Previous	Deviation from Average
10-Oct	806	8.78	0.137	14.7	121	NA	-0.6%
	1927	8.68	0.120	14.89	121	1.1%	0.5%
11-Oct	1121	8.73	0.134	14.8	121	-0.6%	-0.1%
	1301	8.73	0.133	14.7	121	0.0%	-0.1%
	1755	8.75	0.133	14.6	121	-0.3%	-0.3%
	2204	8.72	0.133	14.8	121	0.4%	0.1%
12-Oct	0809	8.59	0.133	14.9	121	1.4%	1.5%
	1300	8.77	0.137	14.6	121	-2.1%	-0.5%
	1940	8.78	0.134	14.72	121	-0.1%	-0.6%
13-Oct	0810	8.71	0.134	14.82	121	0.7%	0.1%
	1435	8.73	0.135	14.85	121	-0.1%	0.0%
Average		8.725	0.133				

Background Spectra

On-site test personnel performed matrix spiking using a certified calibration standard of methanol and SF₆. The methanol gas standard was introduced into the sampling system upstream of the particulate matter filter at an average dilution ratio of less than 10% of the total sample volume. Analyte spiking was performed to demonstrate the suitability of the sampling system. The dilution factor was calculated based on the ratio of the SF₆ tracer gas analyzed directly by the FTIR and the in-stack measured concentration.

$$\frac{SF_6 \text{ during spike}}{SF_6 \text{ direct}} = DF$$

The recovery was calculated using the mean concentration of the spiked analyte (S_m), the native concentration of the analyte in the stack (S_u), the dilution factor (DF), and the cylinder concentration (C_s).

$$\text{Recovery}(\%) = \frac{S_m - S_u (1 - DF)}{DF \times C_s}$$

As shown in Table 6-10, the percent recovery was $100 \pm 30\%$ as required by Method 320.

Table 6-10. Spike Recovery Results Summary						
Direct Cylinder Spike, ppm		System Spiked Gas, ppm		Native Concentration, ppm		Recovery, %
methanol	SF ₆	methanol	SF ₆	methanol	SF ₆	
101.26	2.84	9.867	0.272	0.496	-0.00789	94.6

Minimum Detectable Concentration

EPA Method 320 and the equivalent ASTM Standard D6348-03 specify a number of analytical uncertainty parameters that the analyst may calculate to characterize the FTIR system performance.

QA Review

Before the test program began, an analysis of possible analytical interferents (e.g., H₂O, CO₂, CO, pinenes) based on previous stack test data. Analytical wavelengths were determined to minimize analytical uncertainty and detection limits using reference spectra and the FTIR instrument that was used for the field testing.

At the conclusion of the testing a quality assurance review of the test data was performed. This review included examination of the sample spectra and the quantitative analytical results. It also included spot-checking the analysis results by hand. These examinations included visual comparisons of the sample and reference spectra.

7. PROCESS DOCUMENTATION

Enviva Pellets Wiggins, LLC personnel logged the following process data during each test run of each process unit.

- Throughput in tons per hour (all process units)
- Inlet temperature (dryer)
- Outlet temperature (dryer)
- Cyclone static pressure drop (dryer, hammermill, presses)
- Wood feed % softwood content

8. REFERENCES

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5. Beauchemin, P. and M. Tampier. "Emissions and Air Pollution Control for the Biomass Pellet Manufacturing Industry." Report submitted to the British Columbia Ministry of the Environment. May 12, 2010.
6. Milota, M.R. "Emissions from Wood Drying" Forest Projects Journal, Volume 50, Number 6, Pages 10-19, June 2000.
7. Milota, M. and P. Mosher. "Emissions of Hazardous Air Pollutants from Lumber Drying." Forest Products Journal, Volume 58, No. 7/8, Pages 50-55, July/August 2008.

APPENDIX A

Moisture and Gas Flow Rate Data

Air Control Techniques, PC: Emissions Calculations

Job # 1911

Enviva	Wiggins	Green Hammermill	Green Hammermill	Green Hammermill	Dryer 1	Dryer 1	Dryer 1
PARAMETER	NOMENCLATURE	1	2	3	4	5	6
Sampling Location		Green Hammermill	Green Hammermill	Green Hammermill	Dryer 1	Dryer 1	Dryer 1
Date		10/10/2013	10/10/2013	10/10/2013	10/10/2013	10/11/2013	10/11/2013
Run Time	θ	60	60	60	60	60	60
Nozzle Diameter	inches	N/A	N/A	N/A	N/A	N/A	N/A
Stack Area	As - sq. ft.	3.98	3.98	3.98	10.56	10.56	10.56
Pitot Tube Coefficient	Cp	0.84	0.84	0.84	0.84	0.84	0.84
Meter Calibration Factor	Y	0.9828	0.9828	0.9828	0.9828	0.9828	0.9828
Barometric Pressure, inches Hg	Bp - in. Hg	29.90	29.90	29.90	29.90	29.80	29.80
Static Pressure	Pg - in. H ₂ O	-20.8	-20.8	-20.8	-0.75	-0.71	-0.71
Stack Pressure	Ps	28.37	28.37	28.37	29.84	29.75	29.75
Meter Box Pressure Differential	ΔH - in. H ₂ O	1.00	1.00	1.00	1.00	1.00	1.00
Average Velocity Head	Δp - in. H ₂ O	3.961	3.854	3.847	1.283	1.172	1.185
Volume of Gas Sampled	Vm - cu. ft.	33.868	33.981	33.156	33.201	33.221	32.565
Dry Gas Meter Temperature	Tm - °F	66.0	70.8	75.5	81.250	76.5	87.0
Stack Temperature	Ts - °F	70.8	70.6	70.9	146.3	150.1	147.3
Liquid Collected	grams	25.1	26.5	16.6	129.5	99.8	117.5
Carbon Dioxide	% CO ₂	0	0	0	2	4	4
Oxygen	% O ₂	20.9	20.9	20.9	19	17	17
Carbon Monoxide	% CO	0	0	0	0	0	0
Nitrogen	% N ₂	79.1	79.1	79.1	79	79	79
Volume of Gas Sampled, Dry	Vmstd - cu. ft.	33.472	33.283	32.187	31.888	32.082	30.845
Volume of Water Vapor	Vwstd - cu. ft.	1.183	1.249	0.783	6.106	4.706	5.540
Moisture Content	% H ₂ O	3.41	3.62	2.37	16.07	12.79	15.23
Saturation Moisture	% H ₂ O	2.7	2.7	2.7	23.1	25.4	23.7
Dry Mole Fraction	Mfd	0.966	0.964	0.976	0.839	0.872	0.848
Fuel Factor	Fo	#DIV/0!	#DIV/0!	#DIV/0!	0.950	0.975	0.975
Gas Molecular Weight, Dry	Md	28.84	28.84	28.84	29.08	29.32	29.32
Gas Molecular Weight, Wet	Ms	28.47	28.44	28.58	27.30	27.87	27.60
Gas Velocity	vs - ft./sec.	115.87	114.32	113.97	70.16	66.68	67.23
Volumetric Air Flow, Actual	Qaw - ACFM	27,642	27,273	27,189	44,448	42,243	42,593
Volumetric Air Flow, Standard	Qsd - DSCFM	25,184	24,803	25,031	32,404	31,700	31,215

Air Control Techniques, PC: Emissions Calculations

Job # 1911

Enviva	Wiggins	Dry Hammermill 2	Dry Hammermill 2	Dry Hammermill 2	Pellet Mill 2 Aspiration	Pellet Mill 2 Aspiration	Pellet Mill 2 Aspiration
PARAMETER	NOMENCLATURE	10	11	12	16	17	18
Sampling Location		Dry Hammermill 2	Dry Hammermill 2	Dry Hammermill 2	Pellet Mill 2 Aspiration	Pellet Mill 2 Aspiration	Pellet Mill 2 Aspiration
Date		10/11/2013	10/11/2001	10/11/2013	10/12/2013	10/12/2013	10/12/2013
Run Time	θ	60	60	60	60	60	60
Nozzle Diameter	inches	N/A	N/A	N/A	N/A	N/A	N/A
Stack Area	As - sq. ft.	2.64	2.64	2.64	0.20	0.20	0.20
Pitot Tube Coefficient	Cp	0.84	0.84	0.84	0.84	0.84	0.84
Meter Calibration Factor	Y	0.9828	0.9828	0.9828	0.9828	0.9828	0.9828
Barometric Pressure, inches Hg	Bp - in Hg	29.80	29.80	29.80	29.85	29.85	29.85
Static Pressure	Pg - in. H ₂ O	1.4	1.4	1.4	-7.5	-7.5	-7.5
Stack Pressure	Ps	29.90	29.90	29.90	29.30	29.30	29.30
Meter Box Pressure Differential	ΔH - in. H ₂ O	1.00	1.00	1.00	1.00	1.00	1.00
Average Velocity Head	Δp - in. H ₂ O	2.601	2.308	2.618	5.359	4.944	4.547
Volume of Gas Sampled	Vm - cu. ft.	33.419	33.679	33.876	33.241	32.149	34.408
Dry Gas Meter Temperature	Tm - °F	80.3	78.8	78.3	85.0	84.8	81.8
Stack Temperature	Ts - °F	122.4	128.2	116.4	148.6	148.3	152.1
Liquid Collected	grams	30.2	30	30.2	256.8	269.6	274.4
Carbon Dioxide	% CO ₂	0	0	0	0	0	0
Oxygen	% O ₂	20.9	20.9	20.9	20.9	20.9	20.9
Carbon Monoxide	% CO	0	0	0	0	0	0
Nitrogen	% N ₂	79.1	79.1	79.1	79.1	79.1	79.1
Volume of Gas Sampled, Dry	Vmstd - cu. ft.	32.050	32.389	32.609	31.654	30.628	32.962
Volume of Water Vapor	Vwstd - cu. ft.	1.424	1.415	1.424	12.108	12.712	12.938
Moisture Content	% H ₂ O	4.25	4.18	4.18	27.67	29.33	28.19
Saturation Moisture	% H ₂ O	12.3	14.4	10.4	24.9	24.7	27.2
Dry Mole Fraction	Mfd	0.957	0.958	0.958	0.723	0.707	0.718
Fuel Factor	Fo	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!
Gas Molecular Weight, Dry	Md	28.84	28.84	28.84	28.84	28.84	28.84
Gas Molecular Weight, Wet	Ms	28.38	28.38	28.38	25.84	25.66	25.78
Gas Velocity	vs - ft./sec.	95.95	90.82	95.74	149.06	143.63	137.85
Volumetric Air Flow, Actual	Qaw - ACFM	15,197	14,385	15,165	1,756	1,692	1,624
Volumetric Air Flow, Standard	Qsd - DSCFM	13,183	12,366	13,303	1,079	1,016	985

Air Control Techniques, PC: Emissions Calculations

Job # 1911

Enviva	Wiggins	Dryer 2	Dryer 2	Dryer 2
PARAMETER	NOMENCLATURE	19	20	21
Sampling Location		Dryer 2	Dryer 2	Dryer 2
Date		10/13/2013	10/13/2013	10/13/2013
Run Time	θ	60	60	60
Nozzle Diameter	inches	N/A	N/A	N/A
Stack Area	As - sq. ft.	12.05	12.05	12.05
Pitot Tube Coefficient	Cp	0.84	0.84	0.84
Meter Calibration Factor	Y	0.9828	0.9828	0.9828
Barometric Pressure, inches Hg	Bp - in Hg	29.90	29.90	29.90
Static Pressure	Pg - in. H ₂ O	-0.33	-0.33	-0.33
Stack Pressure	Ps	29.88	29.88	29.88
Meter Box Pressure Differential	ΔH - in. H ₂ O	1.00	1.00	1.00
Average Velocity Head	Δp - in. H ₂ O	0.285	0.300	0.291
Volume of Gas Sampled	Vm - cu. ft.	31.888	33.650	30.796
Dry Gas Meter Temperature	Tm - °F	77.5	89.5	90.3
Stack Temperature	Ts - °F	174.3	154.9	171.8
Liquid Collected	grams	267.7	287.5	260
Carbon Dioxide	% CO ₂	4.5	4	4
Oxygen	% O ₂	16.5	17	17
Carbon Monoxide	% CO	0	0	0
Nitrogen	% N ₂	79	79	79
Volume of Gas Sampled, Dry	Vmstd - cu. ft.	30.841	31.834	29.094
Volume of Water Vapor	Vwstd - cu. ft.	12.622	13.556	12.259
Moisture Content	% H ₂ O	29.04	29.86	29.64
Saturation Moisture	% H ₂ O	44.9	28.5	42.4
Dry Mole Fraction	Mfd	0.710	0.701	0.704
Fuel Factor	Fo	0.978	0.975	0.975
Gas Molecular Weight, Dry	Md	29.38	29.32	29.32
Gas Molecular Weight, Wet	Ms	26.08	25.94	25.96
Gas Velocity	vs - ft./sec.	34.58	35.02	34.97
Volumetric Air Flow, Actual	Qaw - ACFM	24,998	25,318	25,278
Volumetric Air Flow, Standard	Qsd - DSCFM	14,745	15,224	14,842

Method 1 - Air Control Techniques, P.C.

Date

10/10/2013

Client	Enviva
Job #	1911
Plant Name	Wiggins
State	Mississippi
City	Wiggins
Sampling Location	Dryer 1
No. of Ports Available	2
No. of Ports Used	1
Port Inside Diameter, Inches	4
Distance From Far Wall To Outside Of Port, Inches	46
Nipple Length And/Or Wall Thickness, Inches	2
Depth Of Stack Or Duct, Inches	44
Stack Or Duct Width (if rectangular), Inches	
Equiv. Diameter = 2DW/(D+W), Inches	44
Stack/Duct Area, Square Feet	10.6
$(\square \times R^2 \text{ or } L \times W)$	
	Upstream Downstream
Distance to Flow Disturbances, Inches	290.4 235.2
Diameters	6.60 5.35

2 diff nipples probe marked to inside of port

Point Location Data			
Point	% of Duct Depth	Distance From Inside Wall	Distance From Outside of Port
1	4.4	1 7/8	3 7/8
2	14.6	6 3/8	8 3/8
3	29.6	13	15
4	70.4	31	33
5	85.4	37 5/8	39 5/8
6	95.6	42 1/8	44 1/8
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

Note: If more than 8 and 2 diameters and if duct dia. is less than 24" use 8 or 9 points.			
Velocity	Diameters		Particulate
	UP	Down	
12	8	2	12
12	7	1.75	12
12	6	1.5	16
16	5	1.25	20
16	2	0.5	24 or 25

Location of Points in Circular Stacks or Ducts											
	4	6	8	10	12	14	16	18	20	22	24
1	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	25.0	14.6	10.6	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2
3	75.0	29.6	19.4	14.6	11.8	9.9	8.5	7.5	6.7	6.0	5.5
4	93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7	7.9
5		85.4	67.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6	10.5
6		95.6	80.6	65.8	35.6	26.9	22.0	18.8	16.5	14.6	13.2
7			89.5	77.4	64.4	36.6	28.3	23.6	20.4	18.0	16.1
8			96.8	85.4	75.0	63.4	37.5	29.6	25.0	21.8	19.4
9				91.8	82.3	73.1	62.5	38.2	30.6	26.2	23.0
10				97.4	88.2	79.9	71.7	61.8	38.8	31.5	27.2
11					93.3	85.4	78.0	70.4	61.2	39.3	32.3
12					97.9	90.1	83.1	76.4	69.4	60.7	39.8
13						94.3	87.6	81.2	75.0	68.5	60.2
14						98.2	91.5	85.4	79.6	73.8	67.7
15							95.1	89.1	83.5	78.2	72.8
16							98.4	92.5	87.1	82.0	77.0
17								95.6	90.3	85.4	80.6
18								98.6	93.3	88.4	83.9
19									96.1	91.3	86.8
20									98.7	94.0	89.5
21										96.5	92.1
22										98.9	94.5
23											96.8
24											98.9

Location of Points in Rectangular Stacks or Ducts											
	2	3	4	5	6	7	8	9	10	11	12
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.5
3		83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8
4			87.5	70.0	58.3	50	43.8	28.9	35.0	31.8	29.2
5				90.0	75	64.3	56.3	50	45.0	40.9	37.5
6					91.7	78.6	68.8	61.1	55.0	50	45.8
7						92.9	81.3	72.2	65.0	59.1	54.2
8							93.8	83.3	75.0	68.2	62.5
9								94.4	85.0	77.3	70.8
10									95.0	86.4	79.2
11										95.5	87.5
12											95.8

0.0000 - 0.0625 - 0 0.5625 - 0.6875 - 5/8
0.0625 - 0.1875 - 1/8 0.6875 - 0.8125 - 3/4
0.1875 - 0.3125 - 1/4 0.8125 - 0.9375 - 7/8
0.3125 - 0.4375 - 3/8 0.9375 - 1.0000 - 1
0.4375 - 0.5625 - 1/2

Dryer 1 Run 1

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		4	
Plant	Wiggins			Date		10/10/2013	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Dryer 1			Pitot ID		6Pext	
Averages		1.283	146.3	Thermocouple ID		TC25	
	Delta P	Temp					
Point No.	In Water	Deg F	Angle				
A-1	1.200	144	7	Oxygen %		19	
2	1.100	145	2				
3	1.050	145	4	Carbon Dioxide %		2	
4	1.400	146	-3				
B-1	1.400	147	0	Moisture %		16.07	
2	1.500	147	-4				
B-1	1.100	147	6	Stack Area sq.in.		1520.530867	
2	1.300	147	3				
3	1.200	147	2	Pbar		29.90	
4	1.300	147	0				
5	1.300	147	-4	Static Pressure		-0.75	
6	1.600	147	-3				
0				Pitot Coef.		0.84	
0							
0				Start Time		1732	
0							
0				Stop Time		1738	
0							
0				Absolute Gas Pressure inches water	Ps =	29.84	
0							
0				Dry Mole Fraction of Gas	Mfd =	0.83929	
0							
0				Dry Molecular Weight of Gas lb/lb Mole	Md =	29.08	
0							
0				Wet Molecular Weight of Gas lb/lb Mole	Ms =	27.30	
0							
0				Average Gas Velocity ft/sec	vs =	70.16	
0							
0				Dry Volumetric Gas Flow Rate			
0				at Standard Conditions SCFM	Qsd =	32404	
0							
0				Wet Volumetric Flue Gas Flow Rate			
0				at Stack Conditions ACFM	Qaw =	44448	
0							
0				Wet Volumetric Gas Flow Rate			
0				at Standard Conditions WSCFH	WSCFH =	2316527	
0							
0				LKCH			
0				Pre	3-6	good	
8				Post	5-4	good	
0							
0							

Dryer 1 Run 2

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		5	
Plant	Wiggins			Date		10/11/2013	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Dryer 1			Pitot ID		6Pext	
Averages		1.172	150.1	Thermocouple ID		TC25	
	Delta P	Temp					
Point No.	In Water	Deg F					
A-1	0.900	145		Oxygen %		17	
2	0.990	147					
3	1.000	148		Carbon Dioxide %		4	
4	1.400	150					
B-1	1.400	151		Moisture %		12.79	
2	0.820	150					
B-1	1.200	151		Stack Area sq.in.		1520.530867	
2	1.300	151					
3	1.300	152		Pbar		29.80	
4	1.300	152					
5	1.350	152		Static Pressure		-0.71	
6	1.200	152					
0				Pitot Coef.		0.84	
0							
0				Start Time		840	
0							
0				Stop Time		850	
0							
0				Absolute Gas Pressure inches water		Ps =	29.75
0							
0				Dry Mole Fraction of Gas		Mfd =	0.87209
0							
0				Dry Molecular Weight of Gas lb/lb Mole		Md =	29.32
0							
0				Wet Molecular Weight of Gas lb/lb Mole		Ms =	27.87
0							
0				Average Gas Velocity ft/sec		vs =	66.68
0							
0				Dry Volumetric Gas Flow Rate			
0				at Standard Conditions SCFM		Qsd =	31700
0							
0				Wet Volumetric Flue Gas Flow Rate			
0				at Stack Conditions ACFM		Qaw =	42243
0							
0				Wet Volumetric Gas Flow Rate			
0				at Standard Conditions WSCFH		WSCFH =	2180938
0							
0				LKCH			
0				Pre		3-4	good
8				Post		5-3	good
0							
0							

Dryer 1 Run 3

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		6	
Plant	Wiggins			Date		10/11/2013	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Dryer 1			Pitot ID		6Pext	
Averages	1.185	147.3		Thermocouple ID		TC25	
	Delta P	Temp					
Point No.	In Water	Deg F					
A-1	1.050	148		Oxygen %		17	
2	1.050	147					
3	1.050	146		Carbon Dioxide %		4	
4	1.500	147					
B-1	1.500	147		Moisture %		15.23	
2	0.940	147					
B-1	1.100	147		Stack Area sq.in.		1520.530867	
2	1.200	147					
3	1.200	147		Pbar		29.80	
4	1.300	148					
5	1.300	148		Static Pressure		-0.71	
6	1.100	148					
0				Pitot Coef.		0.84	
0							
0				Start Time		1112	
0							
0				Stop Time		1115	
0							
0				Absolute Gas Pressure inches water		Ps =	29.75
0							
0				Dry Mole Fraction of Gas		Mfd =	0.84774
0							
0				Dry Molecular Weight of Gas lb/lb Mole		Md =	29.32
0							
0				Wet Molecular Weight of Gas lb/lb Mole		Ms =	27.60
0							
0				Average Gas Velocity ft/sec		vs =	67.23
0							
0				Dry Volumetric Gas Flow Rate			
0				at Standard Conditions SCFM		Qsd =	31215
0							
0				Wet Volumetric Flue Gas Flow Rate			
0				at Stack Conditions ACFM		Qaw =	42593
0							
0				Wet Volumetric Gas Flow Rate			
0				at Standard Conditions WSCFH		WSCFH =	2209261
0							
0				LKCH			
0				Pre		3-4	good
8				Post		5-3	good
0							
0							

Method 1 - Air Control Techniques, P.C.

Date

10/13/2013

Client Enviva
Job # 1911
Plant Name Wiggins
State Mississippi
City Wiggins
Sampling Location Dryer 2

No. of Ports Available 2
No. of Ports Used 1
Port Inside Diameter, Inches 4
Distance From Far Wall To Outside Of Port, Inches 55.5
Nipple Length And/Or Wall Thickness, Inches 8.5
Depth Of Stack Or Duct, Inches 47
Stack Or Duct Width (if rectangular), Inches
Equiv. Diameter = 2DW/(D+W), Inches 47
Stack/Duct Area, Square Feet 12.05
(□ x R² or L x W)

Upstream Downstream
Distance to Flow Disturbances, Inches 325.2 674.4
Diameters 6.92 14.35

2 diff nipples probe marked to inside of port

Point Location Data

Point	% of Duct Depth	Distance From Inside Wall	Distance From Outside of Port
1	4.4	2 1/8	10 5/8
2	14.6	6 7/8	15 3/8
3	29.6	13 7/8	22 3/8
4	70.4	33 1/8	41 5/8
5	85.4	40 1/8	48 5/8
6	95.6	44 7/8	53 3/8
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

Note: If more than 8 and 2 diameters and if duct dia.
is less than 24" use 8 or 9 points.

Velocity	UP	Down	Particulate
12	8	2	12
12	7	1.75	12
12	6	1.5	16
16	5	1.25	20
16	2	0.5	24 or 25

Location of Points in Circular Stacks or Ducts

	4	6	8	10	12	14	16	18	20	22	24
1	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	25.0	14.6	10.6	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2
3	75.0	29.6	19.4	14.6	11.8	9.9	8.5	7.5	6.7	6.0	5.5
4	93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7	7.9
5		85.4	67.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6	10.5
6		95.6		65.8	35.6	26.9	22.0	18.8	16.5	14.6	13.2
7			89.5	77.4	64.4	36.6	28.3	23.6	20.4	18.0	16.1
8			96.8	85.4	75.0	63.4	37.5	29.6	25.0	21.8	19.4
9				91.8	82.3	73.1	62.5	38.2	30.6	26.2	23.0
10				97.4	88.2	79.9	71.7	61.8	38.8	31.5	27.2
11					93.3	85.4	78.0	70.4	61.2	39.3	32.3
12					97.9	90.1	83.1	76.4	69.4	60.7	39.8
13						94.3	87.6	81.2	75.0	68.5	60.2
14						98.2	91.5	85.4	79.6	73.8	67.7
15							95.1	89.1	83.5	78.2	72.8
16							98.4	92.5	87.1	82.0	77.0
17								95.6	90.3	85.4	80.6
18								98.6	93.3	88.4	83.9
19									96.1	91.3	86.8
20									98.7	94.0	89.5
21										96.5	92.1
22										98.9	94.5
23											96.8
24											96.9

Location of Points in Rectangular Stacks or Ducts

	2	3	4	5	6	7	8	9	10	11	12
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.5
3		83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8
4			87.5	70.0	58.3	50	43.8	38.9	35.0	31.8	29.2
5				90.0	75	64.3	56.3	50	45.0	40.9	37.5
6					91.7	78.6	68.8	61.1	55.0	50	45.8
7						92.9	81.3	72.2	65.0	59.1	54.2
8							93.8	83.3	75.0	68.2	62.5
9								94.4	85.0	77.3	70.8
10									95.0	86.4	79.2
11										95.5	87.5
12											96.8

0.0000 - 0.0625 - 0 0.5625 - 0.6875 - 5/8
0.0625 - 0.1875 - 1/8 0.6875 - 0.8125 - 3/4
0.1875 - 0.3125 - 1/4 0.8125 - 0.9375 - 7/8
0.3125 - 0.4375 - 3/8 0.9375 - 1.0000 - 1
0.4375 - 0.5625 - 1/2

Dryer 2 Run 1

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		19	
Plant	Wiggins			Date		10/13/2013	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Dryer 2			Pitot ID		6Pext	
Averages		0.285	174.3	Thermocouple ID		TC25	
	Delta P	Temp					
Point No.	In Water	Deg F	Angle				
A-1	0.200	168	5	Oxygen %		16.5	
2	0.280	173	2				
3	0.330	175	0	Carbon Dioxide %		4.5	
4	0.330	175	5				
5	0.300	174	0	Moisture %		29.04	
6	0.230	170	0				
B-1	0.210	174	6	Stack Area sq.in.		1734.94	
2	0.360	176	3				
3	0.350	177	0	Pbar		29.90	
4	0.330	177	0				
5	0.300	177	-4	Static Pressure		-0.33	
6	0.230	175	4				
0				Pitot Coef.		0.84	
0							
0				Start Time		843	
0							
0				Stop Time		859	
2							
3				Absolute Gas Pressure inches water	Ps =	29.88	
4							
5				Dry Mole Fraction of Gas	Mfd =	0.70959	
6							
7				Dry Molecular Weight of Gas lb/lb Mole	Md =	29.38	
8							
D-1				Wet Molecular Weight of Gas lb/lb Mole	Ms =	26.08	
2							
3				Average Gas Velocity ft/sec	vs =	34.58	
4							
5				Dry Volumetric Gas Flow Rate			
6				at Standard Conditions SCFM	Qsd =	14745	
7							
8				Wet Volumetric Flue Gas Flow Rate			
E-1				at Stack Conditions ACFM	Qaw =	24998	
2							
3				Wet Volumetric Gas Flow Rate			
4				at Standard Conditions WSCFH	WSCFH =	1246788	
5							
6				LKCH			
7				Pre	6-5	good	
8				Post	5-3	good	

Dryer 2 Run 2

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		20	
Plant	Wiggins			Date		10/13/13	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Dryer 2			Pitot ID		6Pext	
Averages		0.300	154.9	Thermocouple ID		TC25	
	Delta P	Temp					
Point No.	In Water	Deg F					
A-1	0.200	167		Oxygen %		17	
2	0.800	167					
3	0.310	167		Carbon Dioxide %		4	
4	0.330	168					
5	0.340	169		Moisture %		29.86	
6	0.200	167					
B-1	0.220	170		Stack Area sq.in.		1734.94	
2	0.310	170					
3	0.310	2		Pbar		29.90	
4	0.290	170					
5	0.260	171		Static Pressure		-0.33	
6	0.190	171					
0				Pitot Coef.		0.84	
0							
0				Start Time		1047	
0							
0				Stop Time		1051	
2							
3				Absolute Gas Pressure inches water		Ps =	29.88
4							
5				Dry Mole Fraction of Gas		Mfd =	0.70135
6							
7				Dry Molecular Weight of Gas lb/lb Mole		Md =	29.32
8							
D-1				Wet Molecular Weight of Gas lb/lb Mole		Ms =	25.94
2							
2				Average Gas Velocity ft/sec		vs =	35.02
4							
5				Dry Volumetric Gas Flow Rate			
6				at Standard Conditions SCFM		Qsd =	15224
7							
8				Wet Volumetric Flue Gas Flow Rate			
E-1				at Stack Conditions ACFM		Qaw =	25318
2							
3				Wet Volumetric Gas Flow Rate			
4				at Standard Conditions WSCFH		WSCFH =	1302430
5							
6				LKCH			
7				Pre		6-5	good
8				Post		5-3	good

Dryer 2 Run 3

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		21	
Plant	Wiggins			Date		10/13/13	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Dryer 2			Pitot ID		6Pext	
Averages		0.291	171.8	Thermocouple ID		TC25	
	Delta P	Temp					
Point No.	In Water	Deg F					
A-1	0.220	169		Oxygen %		17	
2	0.250	172		Carbon Dioxide %		4	
3	0.320	173		Moisture %		29.64	
4	0.320	174		Stack Area sq.in.		1734.94	
5	0.330	174		Pbar		29.90	
6	0.260	168		Static Pressure		-0.33	
B-1	0.240	168		Pitot Coef.		0.84	
2	0.310	171		Start Time		1208	
3	0.340	172		Stop Time		1215	
4	0.330	172					
5	0.310	173					
6	0.280	175					
0							
0							
0							
0							
0							
2							
3				Absolute Gas Pressure inches water		Ps =	29.88
4				Dry Mole Fraction of Gas		Mfd =	0.70356
5				Dry Molecular Weight of Gas lb/lb Mole		Md =	29.32
6				Wet Molecular Weight of Gas lb/lb Mole		Ms =	25.96
7				Average Gas Velocity ft/sec		vs =	34.97
8				Dry Volumetric Gas Flow Rate at Standard Conditions SCFM		Qsd =	14842
D-1				Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM		Qaw =	25278
2				Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH		WSCFH =	1265741
3							
4							
5							
6				LKCH			
7				Pre		3-4	good
8				Post		5-3	good

Method 1 - Air Control Techniques, P.C.

Date

10/10/2013

Client	Enviva
Job #	1911
Plant Name	Wiggins
State	Mississippi
City	Wiggins
Sampling Location	Green Hammermill
No. of Ports Available	2
No. of Ports Used	1
Port Inside Diameter, Inches	3
Distance From Far Wall To Outside Of Port, Inches	30
Nipple Length And/Or Wall Thickness, Inches	3
Depth Of Stack Or Duct, Inches	27
Stack Or Duct Width (if rectangular), Inches	
Equiv. Diameter = 2DW/(D+W), Inches	27
Stack/Duct Area, Square Feet	3.9761
($\square \times R^2$ or L x W)	
Distance to Flow Disturbances, Inches	Upstream 348 Downstream 60
Diameters	12.89 2.22

2 diff nipples probe marked to inside of port

Point Location Data			
Point	% of Duct Depth	Distance From Inside Wall	Distance From Outside of Port
1	4.4	1 2/8	4 2/8
2	14.6	4	7
3	29.6	8	11
4	70.4	19	22
5	85.4	23	26
6	95.6	25 6/8	28 6/8
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

Note: If more than 8 and 2 diameters and if duct dia. is less than 24" use 8 or 9 points.			
Diameters			
Velocity	UP	Down	Particulate
12	8	2	12
12	7	1.75	12
12	6	1.5	16
16	5	1.25	20
16	2	0.5	24 or 25

Location of Points in Circular Stacks or Ducts											
	4	6	8	10	12	14	16	18	20	22	24
1	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	25.0	14.6	10.6	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2
3	75.0	29.6	19.4	14.6	11.8	9.9	8.5	7.5	6.7	6.0	5.5
4	93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7	7.9
5		85.4	67.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6	10.5
6		95.6	80.6	65.8	35.6	26.9	22.0	18.8	16.5	14.6	13.2
7			89.5	77.4	64.4	36.6	28.3	23.6	20.4	18.0	16.1
8			96.8	85.4	75.0	63.4	37.5	29.6	25.0	21.8	19.4
9				91.8	82.3	73.1	62.5	38.2	30.6	26.2	23.0
10				97.4	88.2	79.9	71.7	61.8	38.8	31.5	27.2
11					93.3	85.4	78.0	70.4	61.2	39.3	32.3
12					97.9	90.1	83.1	76.4	69.4	60.7	39.8
13						94.3	87.6	81.2	75.0	68.5	60.2
14						98.2	91.5	85.4	79.6	73.8	67.7
15							95.1	89.1	83.5	78.2	72.8
16							98.4	92.5	87.1	82.0	77.0
17								95.6	90.3	85.4	80.6
18								98.6	93.3	88.4	83.9
19									96.1	91.3	86.8
20									98.7	94.0	89.5
21										96.5	92.1
22										98.9	94.5
23											96.8
24											98.9

Location of Points in Rectangular Stacks or Ducts											
	2	3	4	5	6	7	8	9	10	11	12
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.5
3		83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8
4			87.5	70.0	58.3	50	43.8	28.9	35.0	31.8	29.2
5				90.0	75	64.3	56.3	50	45.0	40.9	37.5
6					91.7	78.6	68.8	61.1	55.0	50	45.8
7						92.9	81.3	72.2	65.0	59.1	54.2
8							93.8	83.3	75.0	68.2	62.5
9								94.4	85.0	77.3	70.8
10									95.0	86.4	79.2
11										95.5	87.5
12											95.8

0.0000 - 0.0625 - 0 0.5625 - 0.6875 - 5/8
0.0625 - 0.1875 - 1/8 0.6875 - 0.8125 - 3/4
0.1875 - 0.3125 - 1/4 0.8125 - 0.9375 - 7/8
0.3125 - 0.4375 - 3/8 0.9375 - 1.0000 - 1
0.4375 - 0.5625 - 1/2

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		1	
Plant	Wiggins			Date		10/10/2013	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Green Hammermill			Pitot ID		4Pext	
				Thermocouple ID		TC25	
Averages	3.961	70.8					
	Delta P	Temp					
Point No.	In Water	Deg F	Angle				
A-1	2.800	71	0	Oxygen %	20.9		
2	3.900	71	1				
3	4.400	71	1	Carbon Dioxide %	0		
4	3.800	71	2				
5	3.800	70	4	Moisture %	3.41		
6	3.000	70	3				
B-1	4.200	72	0	Stack Area sq.in.	572.5552696		
2	4.500	71	0				
3	4.600	71	0	Pbar	29.90		
4	4.600	70	2				
5	4.400	71	4	Static Pressure	-20.8		
6	3.800	70	3				
0				Pitot Coef.	0.84		
0							
0				Start Time	855		
0							
0				Stop Time	908		
2							
3				Absolute Gas Pressure inches water	Ps =	28.37	
4							
5				Dry Mole Fraction of Gas	Mfd =	0.96585	
6							
7				Dry Molecular Weight of Gas lb/lb Mole	Md =	28.84	
8							
D-1				Wet Molecular Weight of Gas lb/lb Mole	Ms =	28.47	
2							
3				Average Gas Velocity ft/sec	vs =	115.87	
4							
5				Dry Volumetric Gas Flow Rate			
6				at Standard Conditions SCFM	Qsd =	25184	
7							
8				Wet Volumetric Flue Gas Flow Rate			
E-1				at Stack Conditions ACFM	Qaw =	27642	
2							
3				Wet Volumetric Gas Flow Rate			
4				at Standard Conditions WSCFH	WSCFH =	1564487	
5							
6				LKCH			
7				Pre	3-4	good	
8				Post	5-3	good	
0							
0							

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		2	
Plant	Wiggins			Date		10/10/2013	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Green Hammermill			Pitot ID		4Pext	
Averages				Thermocouple ID		TC25	
	Delta P	Temp					
Point No.	In Water	Deg F					
A-1	2.700	71		Oxygen %	20.9		
2	3.800	71					
3	4.400	71		Carbon Dioxide %	0		
4	3.800	70					
5	3.300	70		Moisture %	3.62		
6	3.100	68					
B-1	3.900	72		Stack Area sq.in.	572.5552696		
2	4.200	70					
3	4.400	70		Pbar	29.90		
4	4.400	70					
5	4.300	71		Static Pressure	-20.8		
6	4.200	73					
0				Pitot Coef.	0.84		
0							
0				Start Time	1026		
0							
0				Stop Time	1030		
2							
3				Absolute Gas Pressure inches water	Ps =	28.37	
4							
5				Dry Mole Fraction of Gas	Mfd =	0.96382	
6							
7				Dry Molecular Weight of Gas lb/lb Mole	Md =	28.84	
8							
D-1				Wet Molecular Weight of Gas lb/lb Mole	Ms =	28.44	
2							
3				Average Gas Velocity ft/sec	vs =	114.32	
4							
5				Dry Volumetric Gas Flow Rate			
6				at Standard Conditions SCFM	Qsd =	24803	
7							
8				Wet Volumetric Flue Gas Flow Rate			
E-1				at Stack Conditions ACFM	Qaw =	27273	
2							
3				Wet Volumetric Gas Flow Rate			
4				at Standard Conditions WSCFH	WSCFH =	1544072	
5							
6				LKCH			
7				Pre	3-4	good	
8				Post	5-3	good	
0							
0							

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		3	
Plant	Wiggins			Date		10/10/2013	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Green Hammermill			Pitot ID		4Pext	
Averages		3.847	70.9	Thermocouple ID		TC25	
	Delta P	Temp					
Point No.	In Water	Deg F					
A-1	2.700	71		Oxygen %		20.9	
2	3.600	71					
3	4.400	71		Carbon Dioxide %		0	
4	3.700	71					
5	3.200	71		Moisture %		2.37	
6	3.300	69					
B-1	4.000	72		Stack Area sq.in.		572.5552696	
2	4.300	71					
3	4.300	71		Pbar		29.90	
4	4.300	71					
5	4.300	71		Static Pressure		-20.8	
6	4.300	71					
0				Pitot Coef.		0.84	
0							
0				Start Time		1141	
0							
0				Stop Time		1144	
2							
3				Absolute Gas Pressure inches water		Ps =	28.37
4							
5				Dry Mole Fraction of Gas		Mfd =	0.97626
6							
7				Dry Molecular Weight of Gas lb/lb Mole		Md =	28.84
8							
D-1				Wet Molecular Weight of Gas lb/lb Mole		Ms =	28.58
2							
3				Average Gas Velocity ft/sec		vs =	113.97
4							
5				Dry Volumetric Gas Flow Rate			
6				at Standard Conditions SCFM		Qsd =	25031
7							
8				Wet Volumetric Flue Gas Flow Rate			
E-1				at Stack Conditions ACFM		Qaw =	27189
2							
3				Wet Volumetric Gas Flow Rate			
4				at Standard Conditions WSCFH		WSCFH =	1538379
5							
6				LKCH			
7				Pre		3-4	good
8				Post		6-4	good
0							
0							

Method 1 - Air Control Techniques, P.C.

Date

10/12/2013

Client Enviva
Job # 1911
Plant Name Wiggins
State Mississippi
City Wiggins
Sampling Location Pellet Mill 2 Aspiration

No. of Ports Available 1
No. of Ports Used 1
Port Inside Diameter, Inches 1
Distance From Far Wall To Outside Of Port, Inches 6
Nipple Length And/Or Wall Thickness, Inches 0
Depth Of Stack Or Duct, Inches 6
Stack Or Duct Width (if rectangular), Inches
Equiv. Diameter = 2DW/(D+W), Inches 6
Stack/Duct Area, Square Feet 0.20
(□ x R² or L x W)
Upstream Downstream
Distance to Flow Disturbances, Inches 19 39
Diameters 3.17 6.50

Point Location Data

Point	% of Duct Depth	Distance From Inside Wall	Distance From Outside of Port
1	6.7	3/8	1
2	25.0	1 4/8	1 4/8
3	75.0	4 4/8	4 4/8
4	93.3	5 5/8	5
5			
6			
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

Used 8 points because
of diameter otherwise
first 3 points are
at 1" from wall

Note: If more than 8 and 2 diameters and if duct dia.
is less than 24" use 8 or 9 points.

Velocity	UP	Down	Particulate
12	8	2	12
12	7	1.75	12
12	6	1.5	16
16	5	1.25	20
16	2	0.5	24 or 25

Location of Points in Circular Stacks or Ducts

	4	6	8	10	12	14	16	18	20	22	24
1	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	25.0	14.6	10.6	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2
3	75.0	29.6	19.4	14.6	11.8	9.9	8.5	7.5	6.7	6.0	5.5
4	93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7	7.9
5		85.4	67.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6	10.5
6		95.6	80.6	65.8	35.6	26.9	22.0	18.8	16.5	14.6	13.2
7			89.5	77.4	64.4	36.6	28.3	23.6	20.4	18.0	16.1
8			96.8	85.4	75.0	63.4	37.5	29.6	25.0	21.8	19.4
9				91.8	82.3	73.1	62.5	38.2	30.6	26.2	23.0
10				97.4	88.2	79.9	71.7	61.8	38.8	31.5	27.2
11					93.3	85.4	78.0	70.4	61.2	39.3	32.3
12					97.9	90.1	83.1	76.4	69.4	60.7	39.8
13						94.3	87.6	81.2	75.0	68.5	60.2
14						98.2	91.5	85.4	79.6	73.8	67.7
15							95.1	89.1	83.5	78.2	72.8
16							98.4	92.5	87.1	82.0	77.0
17								95.6	90.3	85.4	80.6
18								98.6	93.3	88.4	83.9
19									96.1	91.3	86.8
20									98.7	94.0	89.5
21										96.5	92.1
22										98.9	94.5
23											96.8
24											96.9

Location of Points in Rectangular Stacks or Ducts

	2	3	4	5	6	7	8	9	10	11	12
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.5
3		83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8
4			87.5	70.0	58.3	50	43.8	28.9	35.0	31.8	29.2
5				90.0	75	64.3	56.3	50	45.0	40.9	37.5
6					91.7	78.6	68.8	61.1	55.0	50	45.8
7						92.9	81.3	72.2	65.0	59.1	54.2
8							93.8	83.3	75.0	68.2	62.5
9								94.4	85.0	77.3	70.8
10									95.0	86.4	79.2
11										95.5	87.5
12											96.8

0.0000 - 0.0625 - 0 0.5625 - 0.6875 - 5/8
0.0625 - 0.1875 - 1/8 0.6875 - 0.8125 - 3/4
0.1875 - 0.3125 - 1/4 0.8125 - 0.9375 - 7/8
0.3125 - 0.4375 - 3/8 0.9375 - 1.0000 - 1
0.4375 - 0.5625 - 1/2

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		16	
Plant	Wiggins			Date		10/12/2013	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Pellet Mill 2 Aspiration			Pitot ID		4Pext	
Averages		5.359	148.6	Thermocouple ID		TC25	
	Delta P	Temp					
Point No.	In Water	Deg F	Angle				
A-1	5.400	149	0	Oxygen %	20.9		
2	5.700	148	0				
3	5.100	149	2	Carbon Dioxide %	0		
4	5.000	149	1				
B-1	5.700	149	0	Moisture %	27.67		
2	5.600	148	1				
3	5.400	149	2	Stack Area sq.in.	28.2743343		
4	5.000	148	0				
0				Pbar	29.85		
0							
0				Static Pressure	-7.5		
0							
0				Pitot Coef.	0.84		
0							
0				Start Time	1445		
0							
0				Stop Time	1448		
0							
0				Absolute Gas Pressure inches water	Ps =	29.30	
0							
0				Dry Mole Fraction of Gas	Mfd =	0.72332	
0							
0				Dry Molecular Weight of Gas lb/lb Mole	Md =	28.84	
0							
0				Wet Molecular Weight of Gas lb/lb Mole	Ms =	25.84	
0							
0				Average Gas Velocity ft/sec	vs =	149.06	
0							
0				Dry Volumetric Gas Flow Rate			
0				at Standard Conditions SCFM	Qsd =	1079	
0							
0				Wet Volumetric Flue Gas Flow Rate			
0				at Stack Conditions ACFM	Qaw =	1756	
0							
0				Wet Volumetric Gas Flow Rate			
0				at Standard Conditions WSCFH	WSCFH =	89506.7	
0							
0				LKCH			
0				Pre	4-3	good	
8				Post	5-5	good	

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		17	
Plant	Wiggins			Date		10/12/13	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Pellet Mill 2 Aspiration			Pitot ID		4Pext	
Averages		4.944	148.3	Thermocouple ID		TC25	
	Delta P	Temp					
Point No.	In Water	Deg F					
A-1	3.700	147		Oxygen %		20.9	
2	5.500	149					
3	5.400	148		Carbon Dioxide %		0	
4	5.200	148					
B-1	5.600	148		Moisture %		29.33	
2	4.800	148					
3	4.900	149		Stack Area sq.in.		28.2743	
4	4.600	149					
0				Pbar		29.85	
0							
0				Static Pressure		-7.5	
0							
0				Pitot Coef.		0.84	
0							
0				Start Time		1611	
0							
0				Stop Time		1615	
0							
0				Absolute Gas Pressure inches water		Ps =	29.30
0							
0				Dry Mole Fraction of Gas		Mfd =	0.7067
0							
0				Dry Molecular Weight of Gas lb/lb Mole		Md =	28.84
0							
0				Wet Molecular Weight of Gas lb/lb Mole		Ms =	25.66
0							
0				Average Gas Velocity ft/sec		vs =	143.63
0							
0				Dry Volumetric Gas Flow Rate			
0				at Standard Conditions SCFM		Qsd =	1016
0							
0				Wet Volumetric Flue Gas Flow Rate			
0				at Stack Conditions ACFM		Qaw =	1692
0							
0				Wet Volumetric Gas Flow Rate			
0				at Standard Conditions WSCFH		WSCFH =	86302.3
0							
0				LKCH			
0				Pre		4-3	good
8				Post		5-5	good

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		18	
Plant	Wiggins			Date		10/12/13	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Pellet Mill 2 Aspiration			Pitot ID		4Pext	
Averages		4.547	152.1	Thermocouple ID		TC25	
	Delta P	Temp					
Point No.	In Water	Deg F					
A-1	4.400	152		Oxygen %		20.9	
2	4.600	153					
3	4.600	152		Carbon Dioxide %		0	
4	4.300	152					
B-1	4.800	152		Moisture %		28.19	
2	5.000	152					
3	4.400	153		Stack Area sq.in.		28.2743	
4	4.300	151					
0				Pbar		29.85	
0							
0				Static Pressure		-7.5	
0							
0				Pitot Coef.		0.84	
0							
0				Start Time		1739	
0							
0				Stop Time		1742	
0							
0				Absolute Gas Pressure inches water		Ps =	29.30
0							
0				Dry Mole Fraction of Gas		Mfd =	0.71813
0							
0				Dry Molecular Weight of Gas lb/lb Mole		Md =	28.84
0							
0				Wet Molecular Weight of Gas lb/lb Mole		Ms =	25.78
0							
0				Average Gas Velocity ft/sec		vs =	137.85
0							
0				Dry Volumetric Gas Flow Rate			
0				at Standard Conditions SCFM		Qsd =	985
0							
0				Wet Volumetric Flue Gas Flow Rate			
0				at Stack Conditions ACFM		Qaw =	1624
0							
0				Wet Volumetric Gas Flow Rate			
0				at Standard Conditions WSCFH		WSCFH =	82302.1
0							
0				LKCH			
0				Pre		4-3	good
8				Post		5-5	good

Method 1 - Air Control Techniques, P.C.

Date

10/11/2013

Client Enviva
Job # 1911
Plant Name Wiggins
State Mississippi
City Wiggins
Sampling Location Dry Hammermill 2

No. of Ports Available 2
No. of Ports Used 2
Port Inside Diameter, Inches 0
Distance From Far Wall To Outside Of Port, Inches 22
Nipple Length And/Or Wall Thickness, Inches 0
Depth Of Stack Or Duct, Inches 22
Stack Or Duct Width (if rectangular), Inches
Equiv. Diameter = 2DW/(D+W), Inches 22
Stack/Duct Area, Square Feet 2.6
(□ x R² or L x W)

Upstream Downstream
Distance to Flow Disturbances, inches 52 8
Diameters 2.36 0.36

2 diff nipples probe marked to inside of port

Point Location Data

Point	% of Duct Depth	Distance From Inside Wall	Distance From Outside of Port
1	3.2	6/8	6/8
2	10.6	2 3/8	2 3/8
3	19.4	4 2/8	4 2/8
4	32.3	7 1/8	7 1/8
5	67.7	14 7/8	14 7/8
6	80.6	17 6/8	17 6/8
7	89.5	19 6/8	19 6/8
8	96.8	21 2/8	21 2/8
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

1

21

Note: If more than 8 and 2 diameters and if duct dia.
is less than 24" use 8 or 9 points.

Velocity	Diameters		Particulate
	UP	Down	
12	8	2	12
12	7	1.75	12
12	6	1.5	16
16	5	1.25	20
16	2	0.5	24 or 25

Location of Points in Circular Stacks or Ducts

	4	6	8	10	12	14	16	18	20	22	24
1	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	25.0	14.6	10.6	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2
3	75.0	29.6	19.4	14.6	11.8	9.9	8.5	7.5	6.7	6.0	5.5
4	93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7	7.9
5		85.4	67.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6	10.5
6		95.6	80.6	65.8	35.6	26.9	22.0	18.8	16.5	14.6	13.2
7			89.5	77.4	64.4	36.6	28.3	23.6	20.4	18.0	16.1
8			96.8	85.4	75.0	63.4	37.5	29.6	25.0	21.8	19.4
9				91.8	82.3	73.1	62.5	38.2	30.6	26.2	23.0
10				97.4	88.2	79.9	71.7	61.8	38.8	31.5	27.2
11					93.3	85.4	78.0	70.4	61.2	39.3	32.3
12					97.9	90.1	83.1	76.4	69.4	60.7	39.8
13						94.3	87.6	81.2	75.0	68.5	60.2
14						98.2	91.5	85.4	79.6	73.8	67.7
15							95.1	89.1	83.5	78.2	72.8
16							98.4	92.5	87.1	82.0	77.0
17								95.6	90.3	85.4	80.6
18								98.6	93.3	88.4	83.9
19									96.1	91.3	86.8
20									98.7	94.0	89.5
21										96.5	92.1
22										98.9	94.5
23											96.8
24											98.9

Location of Points in Rectangular Stacks or Ducts

	2	3	4	5	6	7	8	9	10	11	12
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.5
3		83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8
4			87.5	70.0	58.3	50	43.8	28.9	35.0	31.8	29.2
5				90.0	75	64.3	56.3	50	45.0	40.9	37.5
6					91.7	78.6	68.8	61.1	55.0	50	45.8
7						92.9	81.3	72.2	65.0	59.1	54.2
8							93.8	83.3	75.0	68.2	62.5
9								94.4	85.0	77.3	70.8
10									95.0	86.4	79.2
11										95.5	87.5
12											95.8

0.0000 - 0.0625 - 0 0.5625 - 0.6875 - 5/8
0.0625 - 0.1875 - 1/8 0.6875 - 0.8125 - 3/4
0.1875 - 0.3125 - 1/4 0.8125 - 0.9375 - 7/8
0.3125 - 0.4375 - 3/8 0.9375 - 1.0000 - 1
0.4375 - 0.5625 - 1/2

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		10	
Plant	Wiggins			Date		10/11/2013	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Dry Hammermill 2			Pitot ID		4Pext	
Averages		2.601	122.4	Thermocouple ID		TC25	
	Delta P	Temp					
Point No.	In Water	Deg F	Angle				
A-1	2.400	121	0	Oxygen %	20.9		
2	2.600	122	1				
3	2.550	122	0	Carbon Dioxide %	0		
4	2.400	123	0				
5	2.600	123	2	Moisture %	4.25		
6	3.000	122	0				
7	3.000	121	0	Stack Area sq.in.	380.13272		
8	3.300	120	0				
B-1	2.200	122	2	Pbar	29.80		
2	2.200	122	0				
3	2.300	123	1	Static Pressure	1.4		
4	2.300	123	0				
5	2.800	123	2	Pitot Coef.	0.84		
6	2.700	123	0				
7	2.800	125	1	Start Time	1745		
8	2.600	124	1				
0				Stop Time	1758		
2							
3				Absolute Gas Pressure inches water	Ps =	29.90	
4							
5				Dry Mole Fraction of Gas	Mfd =	0.95746	
6							
7				Dry Molecular Weight of Gas lb/lb Mole	Md =	28.84	
8							
D-1				Wet Molecular Weight of Gas lb/lb Mole	Ms =	28.38	
2							
3				Average Gas Velocity ft/sec	vs =	95.95	
4							
5				Dry Volumetric Gas Flow Rate			
6				at Standard Conditions SCFM	Qsd =	13183	
7							
8				Wet Volumetric Flue Gas Flow Rate			
E-1				at Stack Conditions ACFM	Qaw =	15197	
2							
3				Wet Volumetric Gas Flow Rate			
4				at Standard Conditions WSCFH	WSCFH =	826137	
5							
6				LKCH			
7				Pre	4-3	good	
8				Post	5-5	good	
0							
0							

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		11	
Plant	Wiggins			Date		10/11/2001	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Dry Hammermill 2			Pitot ID		4Pext	
Averages	2.308	128.2		Thermocouple ID		TC25	
	Delta P	Temp					
Point No.	In Water	Deg F					
A-1	2.200	124		Oxygen %		20.9	
2	2.150	127					
3	2.000	129		Carbon Dioxide %		0	
4	2.100	129					
5	2.000	129		Moisture %		4.18	
6	2.600	130					
7	2.600	130		Stack Area sq.in.		380.132717	
8	2.600	129					
B-1	1.800	129		Pbar		29.80	
2	2.200	127					
3	2.200	128		Static Pressure		1.4	
4	2.300	128					
5	2.600	128		Pitot Coef.		0.84	
6	2.500	128					
7	2.600	128		Start Time		1917	
8	2.600	128					
0				Stop Time		1923	
2							
3				Absolute Gas Pressure inches water		Ps =	29.90
4							
5				Dry Mole Fraction of Gas		Mfd =	0.95816
6							
7				Dry Molecular Weight of Gas lb/lb Mole		Md =	28.84
8							
D-1				Wet Molecular Weight of Gas lb/lb Mole		Ms =	28.38
2							
3				Average Gas Velocity ft/sec		vs =	90.82
4							
5				Dry Volumetric Gas Flow Rate			
6				at Standard Conditions SCFM		Qsd =	12366
7							
8				Wet Volumetric Flue Gas Flow Rate			
E-1				at Stack Conditions ACFM		Qaw =	14385
2							
3				Wet Volumetric Gas Flow Rate			
4				at Standard Conditions WSCFH		WSCFH =	774351
5							
6				LKCH			
7				Pre		4-3	good
8				Post		5-5	good
0							
0							

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		12	
Plant	Wiggins			Date		10/11/2013	
City/State	Wiggins, MS			Gauge ID		909033	
Location	Dry Hammermill 2			Pitot ID		4Pext	
Averages		2.618	116.4	Thermocouple ID		TC25	
	Delta P	Temp					
Point No.	In Water	Deg F					
A-1	2.700	114		Oxygen %		20.9	
2	2.700	116					
3	2.700	116		Carbon Dioxide %		0	
4	2.500	117					
5	2.800	117		Moisture %		4.18	
6	2.800	118					
7	3.000	117		Stack Area sq.in.		380.1327167	
8	2.900	116					
B-1	3.000	117		Pbar		29.80	
2	2.900	116					
3	2.600	117		Static Pressure		1.4	
4	2.500	116					
5	2.300	116		Pitot Coef.		0.84	
6	2.300	116					
7	2.100	116		Start Time		2038	
8	2.200	117					
0				Stop Time		2043	
2							
3				Absolute Gas Pressure inches water		Ps =	29.90
4							
5				Dry Mole Fraction of Gas		Mfd =	0.95816
6							
7				Dry Molecular Weight of Gas lb/lb Mole		Md =	28.84
8							
D-1				Wet Molecular Weight of Gas lb/lb Mole		Ms =	28.38
2							
3				Average Gas Velocity ft/sec		vs =	95.74
4							
5				Dry Volumetric Gas Flow Rate			
6				at Standard Conditions SCFM		Qsd =	13303
7							
8				Wet Volumetric Flue Gas Flow Rate			
E-1				at Stack Conditions ACFM		Qaw =	15165
2							
3				Wet Volumetric Gas Flow Rate			
4				at Standard Conditions WSCFH		WSCFH =	833051
5							
6				LKCH			
7				Pre		4-3	good
8				Post		5-5	good
0							
0							

Air Control Techniques, PC: Emissions Calculations

Enviva, Wiggins, MS		Job 1911		Pellet Mill 2	Pellet Mill 2	Pellet Mill 2	Pellet Mill 1	Pellet Mill 1	Pellet Mill 1
				Cooler	Cooler	Cooler	Cooler	Cooler	Cooler
PARAMETER		NOMENCLATURE		7	8	9	13	14	15
Sampling Location				Pellet Mill 2	Pellet Mill 2	Pellet Mill 2	Pellet Mill 1	Pellet Mill 1	Pellet Mill 1
				Cooler	Cooler	Cooler	Cooler	Cooler	Cooler
Date				10/11/2013	10/11/2013	10/11/2013	10/12/2013	10/12/2013	10/12/2013
Run Time	θ			60	60	60	60	60	60
Nozzle Diameter	inches			N/A	N/A	N/A	N/A	N/A	N/A
Stack Area	As - sq. ft.			2.4	2.4	2.4	5.81	5.8	5.8
Pitot Tube Coefficient	Cp			0.84	0.84	0.84	0.84	0.84	0.84
Meter Calibration Factor	Y			0.9828	0.9828	0.9828	0.9828	0.9828	0.9828
Barometric Pressure, inches Hg	Bp - in Hg			29.80	29.80	29.80	29.90	29.90	29.90
Static Pressure	Pg - in. H ₂ O			-1.2	-1.2	-1.2	-0.4	-0.4	-0.4
Stack Pressure	Ps			29.71	29.71	29.71	29.87	29.87	29.87
Meter Box Pressure Differential	Δ H - in. H ₂ O			1.00	1.00	1	1.00	1.00	1.00
Average Velocity Head	Δ p - in. H ₂ O			2.293	2.102	2.108	0.654	0.644	0.634
Volume of Gas Sampled	Vm - cu. ft.			34.310	34.423	33.681	33.818	35.845	34.567
Dry Gas Meter Temperature	Tm - °F			87.3	89.3	83.8	71.8	82.5	89.0
Stack Temperature	Ts - °F			148.9	143.2	152.3	82.3	94.8	97.7
Liquid Collected	Grams			35.2	33.5	32.4	24.3	27.8	19.9
Carbon Dioxide	% CO ₂			0	0	0	0	0	0
Oxygen	% O ₂			20.9	20.9	20.9	20.9	20.9	20.9
Carbon Monoxide	% CO			0	0	0	0	0	0
Nitrogen	% N ₂			79.1	79.1	79.1	79.1	79.1	79.1
Volume of Gas Sampled, Dry	Vmstd - cu. ft.			32.483	32.472	32.093	33.061	34.348	32.731
Volume of Water Vapor	Vwstd - cu. ft.			1.660	1.580	1.528	1.146	1.311	0.938
Moisture Content	% H ₂ O			4.86	4.64	4.54	3.35	3.68	2.79
Saturation Moisture	% H ₂ O			24.8	21.4	26.9	3.7	5.5	6.0
Dry Mole Fraction	Mfd			0.951	0.954	0.955	0.967	0.963	0.972
Gas Molecular Weight, Dry	Md			28.84	28.84	28.84	28.84	28.84	28.84
Gas Molecular Weight, Wet	Ms			28.31	28.33	28.34	28.47	28.44	28.53
Gas Velocity	vs - ft./sec.			92.52	88.13	88.91	46.36	46.58	46.26
Volumetric Air Flow, Actual	Qaw - ACFM			13,352	12,718	12,831	16,168	16,246	16,134
Volumetric Air Flow, Standard	Qsd - DSCFM			10,938	10,543	10,488	15,189	14,870	14,825

Method 1 - Air Control Techniques, P.C.

Date

10/12/2013

Client	Enviva
Job #	1911
Plant Name	Wiggins
State	Mississippi
City	Wiggins
Sampling Location	Pellet Mill 1 Cooler
No. of Ports Available	6
No. of Ports Used	4
Port Inside Diameter, Inches	3
Distance From Far Wall To Outside Of Port, Inches	30.5
Nipple Length And/Or Wall Thickness, Inches	3.5
Depth Of Stack Or Duct, Inches	27
Stack Or Duct Width (if rectangular), Inches	31
Equiv. Diameter = 2DW/(D+W), Inches	28.86207
Stack/Duct Area, Square Feet	5.8
(□ x R ² or L x W)	
Distance to Flow Disturbances, Inches	Upstream 72 Downstream 48
Diameters	2.49 1.66

2 diff nipples probe marked to inside of port

Point Location Data			
Point	% of Duct Depth	Distance From Inside Wall	Distance From Outside of Port
1	12.5	3 3/8	6 7/8
2	37.5	10 1/8	13 5/8
3	62.5	16 7/8	20 3/8
4	87.5	23 5/8	27 1/8
5			
6			
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

Note: If more than 8 and 2 diameters and if duct dia. is less than 24" use 8 or 9 points.			
Velocity	Diameters		Particulate
	UP	Down	
12	8	2	12
12	7	1.75	12
12	6	1.5	16
16	5	1.25	20
16	2	0.5	24 or 25

Location of Points in Circular Stacks or Ducts											
	4	6	8	10	12	14	16	18	20	22	24
1	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	25.0	14.6	10.6	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2
3	75.0	29.6	19.4	14.6	11.8	9.9	8.5	7.5	6.7	6.0	5.5
4	93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7	7.9
5		85.4	67.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6	10.5
6		95.6	80.6	65.8	35.6	26.9	22.0	18.8	16.5	14.6	13.2
7			89.5	77.4	64.4	36.6	28.3	23.6	20.4	18.0	16.1
8			96.8	85.4	75.0	63.4	37.5	29.6	25.0	21.8	19.4
9				91.8	82.3	73.1	62.5	38.2	30.6	26.2	23.0
10				97.4	88.2	79.9	71.7	61.8	38.8	31.5	27.2
11					93.3	85.4	78.0	70.4	61.2	39.3	32.3
12					97.9	90.1	83.1	76.4	69.4	60.7	39.8
13						94.3	87.6	81.2	75.0	68.5	60.2
14						98.2	91.5	85.4	79.6	73.8	67.7
15							95.1	89.1	83.5	78.2	72.8
16							98.4	92.5	87.1	82.0	77.0
17								95.6	90.3	85.4	80.6
18								98.6	93.3	88.4	83.9
19									96.1	91.3	86.8
20									98.7	94.0	89.5
21										96.5	92.1
22										98.9	94.5
23											96.8
24											98.9

Location of Points in Rectangular Stacks or Ducts											
	2	3	4	5	6	7	8	9	10	11	12
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.5
3		83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8
4			87.5	70.0	58.3	50	43.8	28.9	35.0	31.8	29.2
5				90.0	75	64.3	56.3	50	45.0	40.9	37.5
6					91.7	78.6	68.8	61.1	55.0	50	45.8
7						92.9	81.3	72.2	65.0	59.1	54.2
8							93.8	83.3	75.0	68.2	62.5
9								94.4	85.0	77.3	70.8
10									95.0	86.4	79.2
11										95.5	87.5
12											95.8

0.0000 - 0.0625 - 0 0.5625 - 0.6875 - 5/8
0.0625 - 0.1875 - 1/8 0.6875 - 0.8125 - 3/4
0.1875 - 0.3125 - 1/4 0.8125 - 0.9375 - 7/8
0.3125 - 0.4375 - 3/8 0.9375 - 1.0000 - 1
0.4375 - 0.5625 - 1/2

Pellet Mill 1 Run 1

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		13	
Plant	Wiggins			Date		10/12/2013	
City/State	Mississippi			Gauge ID		909033	
Location	Pellet Mill 1 Cooler			Pitot ID		4Pext	
Averages		0.654	82.3	Thermocouple ID		4Pext	
	Delta P	Temp					
Point No.	In Water	Deg F	Angle				
A-1	0.380	78	0	Oxygen %		20.9	
2	0.340	79	0				
3	0.330	79	0	Carbon Dioxide %		0	
4	0.340	77	2				
B-1	0.680	82	8	Moisture %		3.35	
2	0.650	81	2				
3	0.540	82	-5	Stack Area sq.in.		837	
4	0.570	82	3				
C-1	0.680	84	-2	Pbar		29.90	
2	0.700	84	-3				
3	0.690	84	0	Static Pressure		-0.4	
4	0.710	84	3				
D-1	1.050	85	0	Pitot Coef.		0.84	
2	1.050	85	-2				
3	1.050	85	-1	Start Time		830	
4	1.100	86	2				
0				Stop Time		847	
0							
0				Absolute Gas Pressure inches water	Ps =	29.87	
0							
0				Dry Mole Fraction of Gas	Mfd =	0.96651	
0							
0				Dry Molecular Weight of Gas lb/lb Mole	Md =	28.84	
0							
0				Wet Molecular Weight of Gas lb/lb Mole	Ms =	28.47	
0							
0				Average Gas Velocity ft/sec	vs =	46.36	
0							
0				Dry Volumetric Gas Flow Rate			
0				at Standard Conditions SCFM	Qsd =	15189	
0							
0				Wet Volumetric Flue Gas Flow Rate			
0				at Stack Conditions ACFM	Qaw =	16168	
0							
0				Wet Volumetric Gas Flow Rate			
0				at Standard Conditions WSCFH	WSCFH =	942901	
0							
0				LKCH			
0				Pre	3-4	good	
0				Post	5-3	good	
#REF!							
#REF!							

Pellet Mill 1 Run 2

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		14	
Plant	Wiggins			Date		10/12/2013	
City/State	Mississippi			Gauge ID		909033	
Location	Pellet Mill 1 Cooler			Pitot ID		4PEXT	
Averages		0.644	94.8	Thermocouple ID		4PEXT	
	Delta P	Temp					
Point No.	In Water	Deg F					
A-1	0.380	92		Oxygen %		20.9	
2	0.400	93					
3	0.380	93		Carbon Dioxide %		0	
4	0.370	93					
B-1	0.530	94		Moisture %		3.68	
2	0.550	95					
3	0.480	95		Stack Area sq.in.		837	
4	0.500	95					
C-1	0.670	95		Pbar		29.90	
2	0.690	95					
3	0.660	96		Static Pressure		-0.4	
4	0.680	96					
D-1	1.300	96		Pitot Coef.		0.84	
2	1.050	96					
3	1.050	96		Start Time		1009	
4	1.050	96					
0				Stop Time		1015	
0							
0				Absolute Gas Pressure inches water		Ps =	29.87
0							
0				Dry Mole Fraction of Gas		Mfd =	0.96324
0							
0				Dry Molecular Weight of Gas lb/lb Mole		Md =	28.84
0							
0				Wet Molecular Weight of Gas lb/lb Mole		Ms =	28.44
0							
0				Average Gas Velocity ft/sec		vs =	46.58
0							
0				Dry Volumetric Gas Flow Rate			
0				at Standard Conditions SCFM		Qsd =	14870
0							
0				Wet Volumetric Flue Gas Flow Rate			
0				at Stack Conditions ACFM		Qaw =	16246
0							
0				Wet Volumetric Gas Flow Rate			
0				at Standard Conditions WSCFH		WSCFH =	926248
0							
0				LKCH			
0				Pre		3-4	good
0				Post		5-3	good
#REF!							
#REF!							

Pellet Mill 1 Run 3

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		15	
Plant	Wiggins			Date		10/12/2013	
City/State	Mississippi			Gauge ID		909033	
Location	Pellet Mill 1 Cooler			Pitot ID		4Pext	
Averages		0.634	97.7	Thermocouple ID		4Pext	
	Delta P	Temp					
Point No.	In Water	Deg F					
A-1	0.340	94		Oxygen %		20.9	
2	0.290	96					
3	0.280	97		Carbon Dioxide %		0	
4	0.330	97					
B-1	0.530	98		Moisture %		2.79	
2	0.540	98					
3	0.500	98		Stack Area sq.in.		837	
4	0.480	98					
C-1	0.730	98		Pbar		29.90	
2	0.740	98					
3	0.670	98		Static Pressure		-0.4	
4	0.670	99					
D-1	1.400	98		Pitot Coef.		0.84	
2	1.050	99					
3	1.000	99		Start Time		1125	
4	1.200	98					
0				Stop Time		1134	
0							
0				Absolute Gas Pressure inches water		Ps =	29.87
0							
0				Dry Mole Fraction of Gas		Mfd =	0.97213
0							
0				Dry Molecular Weight of Gas lb/lb Mole		Md =	28.84
0							
0				Wet Molecular Weight of Gas lb/lb Mole		Ms =	28.53
0							
0				Average Gas Velocity ft/sec		vs =	46.26
0							
0				Dry Volumetric Gas Flow Rate			
0				at Standard Conditions SCFM		Qsd =	14825
0							
0				Wet Volumetric Flue Gas Flow Rate			
0				at Stack Conditions ACFM		Qaw =	16134
0							
0				Wet Volumetric Gas Flow Rate			
0				at Standard Conditions WSCFH		WSCFH =	915021
0							
0				LKCH			
0				Pre		3-4	good
0				Post		5-3	good
#REF!							
#REF!							

Method 1 - Air Control Techniques, P.C.

Date

10/11/2013

 Client Enviva
 Job # 1911
 Plant Name Wiggins
 State Mississippi
 City Wiggins
 Sampling Location Pellet Mill 2 Cooler

 No. of Ports Available 2
 No. of Ports Used 2
 Port Inside Diameter, Inches 3
 Distance From Far Wall To Outside Of Port, Inches 21
 Nipple Length And/Or Wall Thickness, Inches 0
 Depth Of Stack Or Duct, Inches 21
 Stack Or Duct Width (if rectangular), Inches
 Equiv. Diameter = 2DW/(D+W), Inches 21
 Stack/Duct Area, Square Feet 2.4
 (□ x R² or L x W)
 Upstream Downstream
 Distance to Flow Disturbances, inches 51 9.5
 Diameters 2.43 0.45

2 diff nipples probe marked to inside of port

Point Location Data

Point	% of Duct Depth	Distance From Inside Wall	Distance From Outside of Port
1	3.2	0.672	1
2	10.6	2.226	2 1/4
3	19.4	4.074	4 1/8
4	32.3	6.783	6 3/4
5	67.7	14.217	14 1/4
6	80.6	16.926	16 7/8
7	89.5	18.795	18 3/4
8	96.8	20.328	20
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

Note: If more than 8 and 2 diameters and if duct dia. is less than 24" use 8 or 9 points.

Velocity	Diameters		Particulate
	UP	Down	
12	8	2	12
12	7	1.75	12
12	6	1.5	16
16	5	1.25	20
16	2	0.5	24 or 25

Location of Points in Circular Stacks or Ducts											
	4	6	8	10	12	14	16	18	20	22	24
1	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	25.0	14.6	10.6	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2
3	75.0	29.6	19.4	14.6	11.8	9.9	8.5	7.5	6.7	6.0	5.5
4	93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7	7.9
5		85.4	67.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6	10.5
6		95.6	80.6	65.8	35.6	26.9	22.0	18.8	16.5	14.6	13.2
7			89.5	77.4	64.4	36.6	28.3	23.6	20.4	18.0	16.1
8			96.8	85.4	75.0	63.4	37.5	29.6	25.0	21.8	19.4
9				91.8	82.3	73.1	62.5	38.2	30.6	26.2	23.0
10				97.4	88.2	79.9	71.7	61.8	38.8	31.5	27.2
11					93.3	85.4	78.0	70.4	61.2	39.3	32.3
12					97.9	90.1	83.1	76.4	69.4	60.7	39.8
13						94.3	87.6	81.2	75.0	68.5	60.2
14						98.2	91.5	85.4	79.6	73.8	67.7
15							95.1	89.1	83.5	78.2	72.8
16							98.4	92.5	87.1	82.0	77.0
17								95.6	90.3	85.4	80.6
18								98.6	93.3	88.4	83.9
19									96.1	91.3	86.8
20									98.7	94.0	89.5
21										96.5	92.1
22										98.9	94.5
23											96.8
24											98.9

Location of Points in Rectangular Stacks or Ducts											
	2	3	4	5	6	7	8	9	10	11	12
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.5
3		83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8
4			87.5	70.0	58.3	50	43.8	28.9	35.0	31.8	29.2
5				90.0	75	64.3	56.3	50	45.0	40.9	37.5
6					91.7	78.6	68.8	61.1	55.0	50	45.8
7						92.9	81.3	72.2	65.0	59.1	54.2
8							93.8	83.3	75.0	68.2	62.5
9								94.4	85.0	77.3	70.8
10									95.0	86.4	79.2
11										95.5	87.5
12											95.8

 0.0000 - 0.0625 - 0 0.5625 - 0.6875 - 5/8
 0.0625 - 0.1875 - 1/8 0.6875 - 0.8125 - 3/4
 0.1875 - 0.3125 - 1/4 0.8125 - 0.9375 - 7/8
 0.3125 - 0.4375 - 3/8 0.9375 - 1.0000 - 1
 0.4375 - 0.5625 - 1/2

Pellet Mill 2 Cooler Run 1

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		7	
Plant	Wiggins			Date		10/11/2013	
City/State	Mississippi			Gauge ID		909033	
Location	Pellet Mill 2 Cooler			Pitot ID		4PEXT	
Averages	2.293	148.9		Thermocouple ID		4PEXT	
	Delta P	Temp					
Point No.	In Water	Deg F	Angle				
A-1	1.800	150	-2	Oxygen %	20.9		
2	2.400	153	-5				
3	2.800	150	-8	Carbon Dioxide %	0		
4	2.900	150	-4				
5	2.800	150	6	Moisture %	4.86		
6	2.500	150	5				
7	2.300	149	-2	Stack Area sq.in.	346.360595		
8	1.900	144	-2				
B-1	2.300	142	8	Pbar	29.80		
2	2.300	147	6				
3	2.500	149	7	Static Pressure	-1.2		
4	2.500	149	6				
5	2.200	150	-5	Pitot Coef.	0.84		
6	2.100	150	-4				
7	1.900	150	-2	Start Time	1315		
8	1.700	150	-7				
#REF!				Stop Time	1335		
#REF!							
#REF!				Absolute Gas Pressure inches water	Ps =	29.71	
#REF!							
#REF!				Dry Mole Fraction of Gas	Mfd =	0.95139	
#REF!							
#REF!				Dry Molecular Weight of Gas lb/lb Mole	Md =	28.84	
#REF!							
#REF!				Wet Molecular Weight of Gas lb/lb Mole	Ms =	28.31	
#REF!							
#REF!				Average Gas Velocity ft/sec	vs =	92.52	
#REF!							
#REF!				Dry Volumetric Gas Flow Rate			
#REF!				at Standard Conditions SCFM	Qsd =	10938	
#REF!							
#REF!				Wet Volumetric Flue Gas Flow Rate			
#REF!				at Stack Conditions ACFM	Qaw =	13352	
#REF!							
#REF!				Wet Volumetric Gas Flow Rate			
#REF!				at Standard Conditions WSCFH	WSCFH =	689797	
#REF!							
#REF!				LKCH			
#REF!				Pre	3-4	good	
#REF!				Post	5-3	good	
#REF!							
#REF!							

Pellet Mill 2 Cooler Run 2

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		8	
Plant	Wiggins			Date		10/11/2013	
City/State	Mississippi			Gauge ID		909033	
Location	Pellet Mill 2 Cooler			Pitot ID		4PEXT	
Averages	2.102	143.2		Thermocouple ID		4PEXT	
	Delta P	Temp					
Point No.	In Water	Deg F					
A-1	2.400	147		Oxygen %	20.9		
2	2.300	143					
3	2.200	144		Carbon Dioxide %	0		
4	2.000	144					
5	1.800	142		Moisture %	4.64		
6	1.800	139					
7	1.800	140		Stack Area sq.in.	346.360595		
8	1.700	140					
B-1	1.800	142		Pbar	29.80		
2	2.050	144					
3	2.250	143		Static Pressure	-1.2		
4	2.200	144					
5	2.300	144		Pitot Coef.	0.84		
6	2.350	145					
7	2.400	145		Start Time	1450		
8	2.400	145					
0				Stop Time	1458		
0							
0				Absolute Gas Pressure inches water	Ps =	29.71	
0							
0				Dry Mole Fraction of Gas	Mfd =	0.95361	
0							
0				Dry Molecular Weight of Gas lb/lb Mole	Md =	28.84	
0							
0				Wet Molecular Weight of Gas lb/lb Mole	Ms =	28.33	
0							
0				Average Gas Velocity ft/sec	vs =	88.13	
0							
0				Dry Volumetric Gas Flow Rate			
0				at Standard Conditions SCFM	Qsd =	10543	
0							
0				Wet Volumetric Flue Gas Flow Rate			
0				at Stack Conditions ACFM	Qaw =	12718	
0							
0				Wet Volumetric Gas Flow Rate			
0				at Standard Conditions WSCFH	WSCFH =	663328	
0							
0				LKCH			
0				Pre	3-4	good	
0				Post	5-3	good	
#REF!							
#REF!							

Pellet Mill 2 Cooler Run 3

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number		1911	
Client	Enviva			ACT Run Number		9	
Plant	Wiggins			Date		10/11/2013	
City/State	Mississippi			Gauge ID		909033	
Location	Pellet Mill 2 Cooler			Pitot ID		4PEXT	
Averages	2.108	152.3		Thermocouple ID		4PEXT	
	Delta P	Temp					
Point No.	In Water	Deg F					
A-1	1.900	150		Oxygen %	20.9		
2	2.300	151					
3	2.300	154		Carbon Dioxide %	0		
4	2.200	152					
5	2.150	152		Moisture %	4.54		
6	2.200	152					
7	2.000	152		Stack Area sq.in.	346.360595		
8	2.100	146					
B-1	1.900	151		Pbar	29.80		
2	2.000	154					
3	2.050	154		Static Pressure	-1.2		
4	2.200	154					
5	2.100	154		Pitot Coef.	0.84		
6	2.200	154					
7	2.050	154		Start Time	1614		
8							
0				Stop Time	1621		
0							
0				Absolute Gas Pressure inches water	Ps =	29.71	
0							
0				Dry Mole Fraction of Gas	Mfd =	0.95456	
0							
0				Dry Molecular Weight of Gas lb/lb Mole	Md =	28.84	
0							
0				Wet Molecular Weight of Gas lb/lb Mole	Ms =	28.34	
0							
0				Average Gas Velocity ft/sec	vs =	88.91	
0							
0				Dry Volumetric Gas Flow Rate			
0				at Standard Conditions SCFM	Qsd =	10488	
0							
0				Wet Volumetric Flue Gas Flow Rate			
0				at Stack Conditions ACFM	Qaw =	12831	
0							
0				Wet Volumetric Gas Flow Rate			
0				at Standard Conditions WSCFH	WSCFH =	659261	
0							
0				LKCH			
0				Pre	3-4	good	
0				Post	5-3	good	
#REF!							
#REF!							

Air Control Techniques, P.C.
Moisture Sampling Train Field Data Sheet

Date 10/10/13
8/4/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	ENVNA	Umbilical ID	200
City, State	Wiggins, MS	Meterbox ID	909033
Test Location	Green Hammer Mill	$\Delta H @$	1.917
Personnel	TJB JBG	Gamma (γ)	0.9828

Run Identification		<table border="1"> <thead> <tr> <th></th> <th>Actual</th> <th>Req'd</th> <th>Vac</th> </tr> </thead> <tbody> <tr> <td>Pre Leak Check</td> <td>0.000</td> <td>< 0.02 or 4%</td> <td>10</td> </tr> <tr> <td>Post Leak Check</td> <td>0.000</td> <td>< 0.02 or 4%</td> <td>10</td> </tr> </tbody> </table>								Actual	Req'd	Vac	Pre Leak Check	0.000	< 0.02 or 4%	10	Post Leak Check	0.000	< 0.02 or 4%	10
	Actual	Req'd	Vac																	
Pre Leak Check	0.000	< 0.02 or 4%	10																	
Post Leak Check	0.000	< 0.02 or 4%	10																	
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)												
9:17	0	470.600	65	1.0	N/A	N/A	55	5												
9:32	15	479.71	66	1.0	↓	↓	55	5												
9:47	30	487.5	66	1.0	↓	↓	56	5												
10:02	45	496.2	67	1.0	↓	↓	60	6												
10:17	60	504.468			↓	↓														

Run Identification		<table border="1"> <thead> <tr> <th></th> <th>Actual</th> <th>Req'd</th> <th>Vac</th> </tr> </thead> <tbody> <tr> <td>Pre Leak Check</td> <td>0.000</td> <td>< 0.02 or 4%</td> <td>10</td> </tr> <tr> <td>Post Leak Check</td> <td>0.000</td> <td>< 0.02 or 4%</td> <td>9</td> </tr> </tbody> </table>								Actual	Req'd	Vac	Pre Leak Check	0.000	< 0.02 or 4%	10	Post Leak Check	0.000	< 0.02 or 4%	9
	Actual	Req'd	Vac																	
Pre Leak Check	0.000	< 0.02 or 4%	10																	
Post Leak Check	0.000	< 0.02 or 4%	9																	
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)												
10:36	0	504.700	68	1.0	N/A	N/A	60	5												
10:51	15	513.10	70		↓	↓	55	5												
11:06	30	521.9	72		↓	↓	55	5												
11:21	45	530.0	73		↓	↓	57	5												
11:36	60	538.681			↓	↓														

Run Identification		<table border="1"> <thead> <tr> <th></th> <th>Actual</th> <th>Req'd</th> <th>Vac</th> </tr> </thead> <tbody> <tr> <td>Pre Leak Check</td> <td>0.000</td> <td>< 0.02 or 4%</td> <td>11</td> </tr> <tr> <td>Post Leak Check</td> <td>0.000</td> <td>< 0.02 or 4%</td> <td>9</td> </tr> </tbody> </table>								Actual	Req'd	Vac	Pre Leak Check	0.000	< 0.02 or 4%	11	Post Leak Check	0.000	< 0.02 or 4%	9
	Actual	Req'd	Vac																	
Pre Leak Check	0.000	< 0.02 or 4%	11																	
Post Leak Check	0.000	< 0.02 or 4%	9																	
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)												
11:50	0	538.900	74	1.0	N/A	N/A	59	5												
12:05	15	549.0	75		↓	↓	50	5												
12:20	30	557.8	76		↓	↓	51	5												
12:35	45	563.4	77		↓	↓	53	5												
12:50	60	572.056			↓	↓														

Method 4 - Air Control Techniques, P.C.

Date 10/10/13

Identification Information

Client	<u>ENLIVA</u>	Job	<u>1911</u>
Plant Name	<u>Wiggins</u>	Process	<u>Green Hammer Mill</u>
City	<u>Wiggins</u>	State	<u>MS</u>

Sampling Information

Run Number		Balance Number	<u>600</u>
Sampling Date		Balance Type	<u>ELECTRONIC</u>
Recovery Date		Balance Level	<u>EVI-1000</u>
Personnel	<u>TJB JBG</u>	Recovery Area	<input checked="" type="checkbox"/>

Location Moisture Data

	Run Number	M4-1	M4-2	M4-3
Impinger 1				
Final Weight, grams/mls		<u>809.3</u>	<u>743.0</u>	<u>822.7</u>
Initial Weight, grams/mls		<u>735.6</u>	<u>724.5</u>	<u>809.3</u>
Condensed Water, grams		<u>73.7</u>	<u>18.5</u>	<u>13.4</u>
Impinger 2				
Final Weight, grams/mls		<u>661.1</u>	<u>729.5</u>	<u>661.5</u>
Initial Weight, grams/mls		<u>719.0</u>	<u>728.8</u>	<u>661.1</u>
Condensed Water, grams		<u>-57.9</u>	<u>0.7</u>	<u>0.4</u>
Impinger 3				
Final Weight, grams/mls		<u>595.9</u>	<u>597.0</u>	<u>596.1</u>
Initial Weight, grams/mls		<u>594.4</u>	<u>595.6</u>	<u>595.9</u>
Condensed Water, grams		<u>1.5</u>	<u>1.4</u>	<u>0.2</u>
Condensed Water, grams		<u>17.3</u>	<u>20.6</u>	
Silica Gel				
Final Weight, grams		<u>815.3</u>	<u>797.7</u>	<u>817.9</u>
Initial Weight, grams		<u>807.5</u>	<u>791.1</u>	<u>815.3</u>
Adsorbed Water, grams		<u>7.8</u>	<u>5.9</u>	<u>2.6</u>
Adsorbed Water, grams		<u>—</u>	<u>—</u>	<u>—</u>
Total Water, grams		<u>25.1</u>	<u>26.5</u>	<u>16.6</u>

$Vm(std) = \text{Volume of gas sampled at standard conditions (dscf)}$
 $Vm(std) = ((\text{Gamma} * 17.64 * Vm * (Pbar + (\Delta H / 13.6))) / (Tm + 460))$
 $Vwc(std) = \text{volume of water vapor at standard conditions (scf)}$
 $Vwc(std) = (0.04707) * (\text{volume of water collected (mls)})$
 $Bws = \text{Mole fraction of water vapor}$
 $Bws = Vwc(std) / (Vm(std) + Vwc(std))$
 $\text{Percent Moisture} = 100 * Bws$

Air Control Techniques, P.C.
Moisture Sampling Train Field Data Sheet

Date 8/19/13
10/10/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	ENVIVA	Umbilical ID	200
City, State	Wagons, MS	Meterbox ID	909033
Test Location	DRYER #1	$\Delta H @$	1.917
Personnel	TJB, JBS	Gamma (γ)	0.9828

Run Identification		Actual		Req'd		Vac	
144		Pre Leak Check	0.000	< 0.02 or 4%	10		
		Post Leak Check	0.000	< 0.02 or 4%	9		

Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
1734	0	572.300	80	1.0	N/A	N/A	58	3
1753	15	580.90	81	↓	↓	↓	54	3
1808	30	581.10	82	↓	↓	↓	56	3
1823	45	597.2	82	↓	↓	↓	57	3
1838	60	605.501		↓	↓	↓		

10/11/13

Run Identification		Actual		Req'd		Vac	
5		Pre Leak Check	0.000	< 0.02 or 4%	10		
		Post Leak Check	0.000	< 0.02 or 4%	10		

Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
1000	0	605.700	70	1.0	N/A	N/A	59	3
1015	15	614.00	74	↓	↓	↓	63	3
1030	30	622.24	79	↓	↓	↓	66	3
1045	45	630.61	83	↓	↓	↓	67	3
1100	60	638.921		↓	↓	↓		

10/11/13

Run Identification		Actual		Req'd		Vac	
6		Pre Leak Check	0.000	< 0.02 or 4%	10		
		Post Leak Check	0.000	< 0.02 or 4%	10		

Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
1137	0	639.106	86	1.0	N/A	N/A	56	3
1152	15	647.5	87	↓	↓	↓	58	3
1207	30	655.17	87	↓	↓	↓	59	3
1222	45	663.24	88	↓	↓	↓	61	3
1237	60	671.665		↓	↓	↓		

Method 4 - Air Control Techniques, P.C.

Date 10/10/2013

Identification Information

Client	Enviya	Job	2911
Plant Name	Wiggins	Process	DRYER #1
City	Wiggins	State	MS

Sampling Information

Run Number		Balance Number	V1000
Sampling Date		Balance Type	Electronic
Recovery Date		Balance Level	✓
Personnel	TTB JB6	Recovery Area	✓

Location Moisture Data

Run Number	4	5	6
<u>Impinger 1</u>			
Final Weight, grams/mls	858.1	943.8	826.7
Initial Weight, grams/mls	743.0	822.7	722.7
Condensed Water, grams	115.1	121.1	104.0
<u>Impinger 2</u>			
Final Weight, grams/mls	736.5	630.7	744.4
Initial Weight, grams/mls	729.5	601.5	736.5
Condensed Water, grams	7.0	29.2	7.9
<u>Impinger 3</u>			
Final Weight, grams/mls	597.1	599.5	597.8
Initial Weight, grams/mls	597.0	596.1	597.1
Condensed Water, grams	0.1	3.4	0.7
Condensed Water, grams			
<u>Silica Gel</u>			
Final Weight, grams	805.0	824.0	809.9
Initial Weight, grams	797.7	817.9	805.0
Adsorbed Water, grams	7.3	6.1	4.9
Adsorbed Water, grams	129.5	99.8	
	↓	↓	
Total Water, grams			117.5

$Vm(std) = \text{Volume of gas sampled at standard conditions (dscf)}$
 $Vm(std) = ((\text{Gamma} * 17.64 * Vm * (Pbar + (\Delta H / 13.6))) / (Tm + 460))$
 $Vwc(std) = \text{volume of water vapor at standard conditions (scf)}$
 $Vwc(std) = (0.04707) * (\text{volume of water collected (mls)})$
 $Bws = \text{Mole fraction of water vapor}$
 $Bws = Vwc(std) / (Vm(std) + Vwc(std))$
 $\text{Percent Moisture} = 100 * Bws$

Air Control Techniques, P.C.
Moisture Sampling Train Field Data Sheet

Date 10/11/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	ENVIVA	Umbilical ID	200
City, State	Wiggins MS	Meterbox ID	909833
Test Location	Polystyrene Mill Coolers #2	$\Delta H @$	1.917
Personnel	TJB JBB	Gamma (γ)	0.9828

Run Identification <u>M4-7</u>				<table border="1"> <thead> <tr> <th></th> <th>Actual</th> <th>Req'd</th> <th>Vac</th> </tr> </thead> <tbody> <tr> <td>Pre Leak Check</td> <td>0.000</td> <td>< 0.02 or 4%</td> <td>10</td> </tr> <tr> <td>Post Leak Check</td> <td>0.000</td> <td>< 0.02 or 4%</td> <td>8</td> </tr> </tbody> </table>						Actual	Req'd	Vac	Pre Leak Check	0.000	< 0.02 or 4%	10	Post Leak Check	0.000	< 0.02 or 4%	8
	Actual	Req'd	Vac																	
Pre Leak Check	0.000	< 0.02 or 4%	10																	
Post Leak Check	0.000	< 0.02 or 4%	8																	
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)												
1343	0	672.000	85	1.0	N/A	N/A	57	3												
1358	15	680.60	86	↓	↓	↓	61	3												
1413	30	689.23	89	↓	↓	↓	61	3												
1428	45	698.1	89	↓	↓	↓	60	3												
1443	60	706.310		↓	↓	↓														

Run Identification <u>M4-8</u>				<table border="1"> <thead> <tr> <th></th> <th>Actual</th> <th>Req'd</th> <th>Vac</th> </tr> </thead> <tbody> <tr> <td>Pre Leak Check</td> <td>0.000</td> <td>< 0.02 or 4%</td> <td>10</td> </tr> <tr> <td>Post Leak Check</td> <td>0.000</td> <td>< 0.02 or 4%</td> <td>4</td> </tr> </tbody> </table>						Actual	Req'd	Vac	Pre Leak Check	0.000	< 0.02 or 4%	10	Post Leak Check	0.000	< 0.02 or 4%	4
	Actual	Req'd	Vac																	
Pre Leak Check	0.000	< 0.02 or 4%	10																	
Post Leak Check	0.000	< 0.02 or 4%	4																	
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)												
1508	0	706.100	89	1.0	N/A	N/A	58	3												
1523	15	715.19	89	↓	↓	↓	59	3												
1538	30	723.95	89	↓	↓	↓	59	3												
1553	45	732.97	90	↓	↓	↓	61	3												
1608	60	741.023		↓	↓	↓														

Run Identification <u>M4-9</u>				<table border="1"> <thead> <tr> <th></th> <th>Actual</th> <th>Req'd</th> <th>Vac</th> </tr> </thead> <tbody> <tr> <td>Pre Leak Check</td> <td>0.000</td> <td>< 0.02 or 4%</td> <td>12</td> </tr> <tr> <td>Post Leak Check</td> <td>0.000</td> <td>< 0.02 or 4%</td> <td>9</td> </tr> </tbody> </table>						Actual	Req'd	Vac	Pre Leak Check	0.000	< 0.02 or 4%	12	Post Leak Check	0.000	< 0.02 or 4%	9
	Actual	Req'd	Vac																	
Pre Leak Check	0.000	< 0.02 or 4%	12																	
Post Leak Check	0.000	< 0.02 or 4%	9																	
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)												
0	1629	741.300	85	1.0	N/A	N/A	57	3												
15	1644	749.90	84	↓	↓	↓	60	3												
30	1659	758.29	83	↓	↓	↓	59	3												
45	1714	766.105	83	↓	↓	↓	60	3												
60	1729	774.981		↓	↓	↓														

Method 4 - Air Control Techniques, P.C.

Date

Identification Information

Client	ENVIVA	Job	1911
Plant Name	Wiggins, MS	Process	Helix m, 11 #2
City	Wiggins, MS	State	MS

codes

Sampling Information

Run Number		Balance Number	1020
Sampling Date		Balance Type	Electronic
Recovery Date		Balance Level	✓
Personnel	TTB JBG	Recovery Area	✓

Location Moisture Data

	Run Number	7	8	9
<u>Impinger 1</u>				
Final Weight, grams/mls		719.2	852.1	746.3
Initial Weight, grams/mls		695.2	826.7	719.2
Condensed Water, grams		24.0	25.4	27.1
<u>Impinger 2</u>				
Final Weight, grams/mls		715.4	747.4	717.5
Initial Weight, grams/mls		712.2	744.4	715.4
Condensed Water, grams		3.2	3.0	2.1
<u>Impinger 3</u>				
Final Weight, grams/mls		603.6	598.2	603.8
Initial Weight, grams/mls		599.5	597.8	603.6
Condensed Water, grams		4.1	0.4	0.2
Condensed Water, grams				
<u>Silica Gel</u>				
Final Weight, grams		827.9	814.6	830.9
Initial Weight, grams		824.0	809.9	827.9
Adsorbed Water, grams		3.9	4.7	3.0
Adsorbed Water, grams		—	—	—
Total Water, grams		35.2	33.5	32.4

$V_m(\text{std})$ = Volume of gas sampled at standard conditions (dscf)

$V_m(\text{std}) = ((\text{Gamma} * 17.64 * V_m * (\text{Pbar} + (\Delta H / 13.6))) / (T_m + 460))$

$V_{wc}(\text{std})$ = volume of water vapor at standard conditions (scf)

$V_{wc}(\text{std}) = (0.04707) * (\text{volume of water collected (mls)})$

Bws = Mole fraction of water vapor

$Bws = V_{wc}(\text{std}) / (V_m(\text{std}) + V_{wc}(\text{std}))$

Percent Moisture = $100 * Bws$

Air Control Techniques, P.C.
Moisture Sampling Train Field Data Sheet

Date 10/11/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	ENVIVA	Umbilical ID	200
City, State	WIGGINS, MS	Meterbox ID	909033
Test Location	DRY Hammer Mill #2	ΔH	1.917
Personnel	Mr. J.B.G.	Gamma (γ)	0.9828

Run Identification				Actual					Req'd	Vac
				Pre Leak Check					< 0.02 or 4%	10
				Post Leak Check					< 0.02 or 4%	10
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)		
1811	0	775.300	80	1.0	N/A	N/A	55	3		
1826	15	784.200	80	↓	↓	↓	54	3		
1841	30	786.71	80	↓	↓	↓	54	3		
1846	45	800.71	81	↓	↓	↓	55	3		
1851	60	808.71		↓	↓	↓				
				795, 100						

Run Identification				Actual					Req'd	Vac
				Pre Leak Check					< 0.02 or 4%	10
				Post Leak Check					< 0.02 or 4%	10
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)		
1935	0	809.400	79	1.0	N/A	N/A	57	3		
1950	15	817.9	78	↓	↓	↓	55	3		
2005	30	826.5	79	↓	↓	↓	56	3		
2020	45	835.3	79	↓	↓	↓	56	3		
2035	60	843.84		↓	↓	↓				

Run Identification				Actual					Req'd	Vac
				Pre Leak Check					< 0.02 or 4%	12
				Post Leak Check					< 0.02 or 4%	9
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)		
2048	0	843.300	78	1.0	N/A	N/A	57	3		
2103	15	852.17	78	↓	↓	↓	57	3		
2118	30	860.25	79	↓	↓	↓	57	3		
2133	45	868.82	78	↓	↓	↓	56	3		
2148	60	877.176		↓	↓	↓				

32.4
32.5

Method 4 - Air Control Techniques, P.C.

Date

Identification Information

Client ENVIVA
Plant Name Wiggins
City Wiggins

Job 1911
Process DRY Hammermill #2
State MS

Sampling Information

Run Number
Sampling Date
Recovery Date
Personnel TJB JBG

Balance Number V1000
Balance Type Electronic
Balance Level ✓
Recovery Area ✓

Location Moisture Data

Run Number 10 11 12

Impinger 1

Final Weight, grams/mls	<u>875.7</u>	<u>770.2</u>	<u>898.8</u>
Initial Weight, grams/mls	<u>852.1</u>	<u>746.3</u>	<u>875.7</u>
Condensed Water, grams	<u>23.6</u>	<u>23.9</u>	<u>23.1</u>

Impinger 2

Final Weight, grams/mls	<u>749.9</u>	<u>720.5</u>	<u>752.8</u>
Initial Weight, grams/mls	<u>747.4</u>	<u>717.5</u>	<u>749.9</u>
Condensed Water, grams	<u>2.5</u>	<u>3.0</u>	<u>2.9</u>

Impinger 3

Final Weight, grams/mls	<u>598.4</u>	<u>604.4</u>	<u>598.8</u>
Initial Weight, grams/mls	<u>598.2</u>	<u>603.8</u>	<u>598.4</u>
Condensed Water, grams	<u>0.2</u>	<u>0.6</u>	<u>0.4</u>

Condensed Water, grams

Silica Gel

Final Weight, grams	<u>818.5</u>	<u>833.4</u>	<u>822.3</u>
Initial Weight, grams	<u>814.6</u>	<u>830.9</u>	<u>818.5</u>
Adsorbed Water, grams	<u>3.9</u>	<u>2.5</u>	<u>3.8</u>

Adsorbed Water, grams

Total Water, grams 30.2 30.0 30.2

$Vm(std)$ = Volume of gas sampled at standard conditions (dscf)
 $Vm(std) = ((\text{Gamma} * 17.64 * Vm * (Pbar + (\Delta H / 13.6))) / (Tm + 460))$
 $Vwc(std)$ = volume of water vapor at standard conditions (scf)
 $Vwc(std) = (0.04707) * (\text{volume of water collected (mls)})$
 Bws = Mole fraction of water vapor
 $Bws = Vwc(std) / (Vm(std) + Vwc(std))$
Percent Moisture = $100 * Bws$

Air Control Techniques, P.C.
Moisture Sampling Train Field Data Sheet

Date 10/12/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	ENVIVA	Umbilical ID	200
City, State	Wiggins MS	Meterbox ID	09033
Test Location	Pellet Mill #1 Cooler	$\Delta H @$	1.917
Personnel	TJR JBB	Gamma (γ)	0.9808

Run Identification <u>M4-13</u>				Actual		Req'd		Vac
				Pre Leak Check	0.000	< 0.02 or 4%	12	
				Post Leak Check	0.000	< 0.02 or 4%	8	
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
858	0	877.400	67	1.0	N/A	N/A	52	3
913	15	886.03	70	↓	↓	↓	55	3
928	30	895.1	73	↓	↓	↓	56	3
943	45	903.1	77	↓	↓	↓	58	3
958	60	911.268		↓	↓	↓		

Run Identification <u>M4-14</u>				Actual		Req'd		Vac
				Pre Leak Check	0.000	< 0.02 or 4%	10	
				Post Leak Check	0.000	< 0.02 or 4%	10	
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
1022	0	911.500	74	1.0	N/A	N/A	59	3
1037	15	920.39	82	↓	↓	↓	60	3
1052	30	929.10	86	↓	↓	↓	54	3
1107	45	938.32	88	↓	↓	↓	55	3
1122	60	947.345		↓	↓	↓		

Run Identification <u>M4-15</u>				Actual		Req'd		Vac
				Pre Leak Check	0.000	< 0.02 or 4%	11	
				Post Leak Check	0.010	< 0.02 or 4%	9	
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
1141	0	947.600	89	1.0	N/A	N/A	56	3
1156	15	956.32	89	↓	↓	↓	60	3
1211	30	964.92	89	↓	↓	↓	60	3
1226	45	973.55	89	↓	↓	↓	61	3
1241	60	982.167		↓	↓	↓		

Method 4 - Air Control Techniques, P.C.

Date

Identification Information

Client Envira
Plant Name Wiggins
City Wiggins

Job 1911
Process Rellet Codes # 1
State MS

Sampling Information

Run Number
Sampling Date
Recovery Date
Personnel TTB JBG

Balance Number
Balance Type
Balance Level
Recovery Area

Location Moisture Data

Run Number 13 14 15

Impinger 1

Final Weight, grams/mls	<u>748.2</u>	<u>787.3</u>	<u>765.0</u>
Initial Weight, grams/mls	<u>728.1</u>	<u>763.4</u>	<u>748.2</u>
Condensed Water, grams	<u>20.1</u>	<u>23.9</u>	<u>16.8</u>

Impinger 2

Final Weight, grams/mls	<u>722.1</u>	<u>754.0</u>	<u>722.9</u>
Initial Weight, grams/mls	<u>720.5</u>	<u>752.8</u>	<u>722.1</u>
Condensed Water, grams	<u>1.6</u>	<u>1.2</u>	<u>0.8</u>

Impinger 3

Final Weight, grams/mls	<u>604.4</u>	<u>598.6</u>	<u>604.9</u>
Initial Weight, grams/mls	<u>604.4</u>	<u>598.8</u>	<u>604.4</u>
Condensed Water, grams	<u>0.0</u>	<u>-0.2</u>	<u>0.5</u>

Condensed Water, grams

Silica Gel

Final Weight, grams	<u>838.0</u>	<u>825.2</u>	<u>837.9</u>
Initial Weight, grams	<u>833.4</u>	<u>822.3</u>	<u>836.0</u>
Adsorbed Water, grams	<u>2.6</u>	<u>2.9</u>	<u>1.9</u>

Adsorbed Water, grams — — —

Total Water, grams 24.3 27.8 19.9

$Vm(std) = \text{Volume of gas sampled at standard conditions (dscf)}$
 $Vm(std) = ((\text{Gamma} * 17.64 * Vm * (Pbar + (\Delta H / 13.6))) / (Tm + 460))$
 $Vwc(std) = \text{volume of water vapor at standard conditions (scf)}$
 $Vwc(std) = (0.04707) * (\text{volume of water collected (mls)})$
 $Bws = \text{Mole fraction of water vapor}$
 $Bws = Vwc(std) / (Vm(std) + Vwc(std))$
 $\text{Percent Moisture} = 100 * Bws$

Method 4 - Air Control Techniques, P.C.

Date

Identification Information

Client **ENVIVA**
Plant Name **Wiggins**
City **Wiggins**

Job **1911**
Process **ASPIRATOR**
State **MS**

Sampling Information

Run Number
Sampling Date
Recovery Date
Personnel **TB JBG**

Balance Number
Balance Type
Balance Level
Recovery Area

Location Moisture Data

Run Number **16** **17** **18**

Impinger 1

Final Weight, grams/mls	914.9	958.8	946.7
Initial Weight, grams/mls	787.3	760.0	743.8
Condensed Water, grams	127.6	198.8	202.9

Impinger 2

Final Weight, grams/mls	877.1	790.3	814.9
Initial Weight, grams/mls	754.0	722.9	746.0
Condensed Water, grams	123.1	67.4	68.9

Impinger 3

Final Weight, grams/mls	599.7	605.0	600.3
Initial Weight, grams/mls	598.6	604.9	599.7
Condensed Water, grams	1.1	0.1	0.6

Condensed Water, grams

Silica Gel

Final Weight, grams	830.2	841.2	832.2
Initial Weight, grams	825.2	837.9	830.2
Adsorbed Water, grams	5.0	3.3	2.0

Adsorbed Water, grams

Total Water, grams **256.8** **269.6** **274.4**

$Vm(std) = \text{Volume of gas sampled at standard conditions (dscf)}$
 $Vm(std) = ((\text{Gamma} * 17.64 * Vm * (Pbar + (\Delta H / 13.6))) / (Tm + 460))$
 $Vwc(std) = \text{volume of water vapor at standard conditions (scf)}$
 $Vwc(std) = (0.04707) * (\text{volume of water collected (mls)})$
 $Bws = \text{Mole fraction of water vapor}$
 $Bws = Vwc(std) / (Vm(std) + Vwc(std))$
 $\text{Percent Moisture} = 100 * Bws$

24.7
1016

Air Control Techniques, P.C.
Moisture Sampling Train Field Data Sheet

Date 10/12/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	ENVIVA	Umbilical ID	30
City, State	Wiggins, MS	Meterbox ID	48033
Test Location	Relief M. H. Aspirator	$\Delta H @$	1.917
Personnel	TIB JBG	Gamma (γ)	0.9828

Run Identification <u>M4-16</u>				Actual			Req'd		Vac	
				Pre Leak Check			< 0.02 or 4%		12	
				Post Leak Check			< 0.02 or 4%		9	
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)		
1509	0	982.400	83	1.0	N/A	N/A	54	3		
1524	15	989.81	85				60	3		
1539	30	998.62	86				62	3		
1554	45	1007.31	86				65	3		
1609	60	1015.641								

Run Identification <u>M4-17</u>				Actual			Req'd		Vac	
				Pre Leak Check			< 0.02 or 4%		10	
				Post Leak Check			< 0.02 or 4%		11	
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)		
1636	0	16.000	85	1.0	N/A	N/A	56	3		
1651	15	24.21	84				65	3		
1706	30	32.27	85				59	3		
1721	45	40.18	85				61	3		
1736	60	48.149								

Run Identification <u>M4-18</u>				Actual			Req'd		Vac	
				Pre Leak Check			< 0.02 or 4%		12	
				Post Leak Check			< 0.02 or 4%		8	
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)		
1800	0	48.300	84	1.0	N/A	N/A	57	3		
1816	15	57.41	82				51	3		
1832	30	66.20	81				52	3		
1848	45	79.55	80				52	3		
1900	60	82.708								

Air Control Techniques, P.C.
Moisture Sampling Train Field Data Sheet

Date 10/13/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	<u>WVIA</u>	Umbilical ID	<u>200</u>
City, State	<u>Wiggins MS</u>	Meterbox ID	<u>981033</u>
Test Location	<u>ISPER #2</u>	$\Delta H @$	<u>1.917</u>
Personnel	<u>115 JBG</u>	Gamma (γ)	<u>0.9828</u>

Run Identification <u>M4-19</u>				Actual		Req'd		Vac	
				Pre Leak Check	<u>0.000</u>	< 0.02 or 4%	<u>15</u>		
				Post Leak Check	<u>0.000</u>	< 0.02 or 4%	<u>10</u>		
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
<u>921</u>	<u>0</u>	<u>82.900</u>	<u>72</u>	<u>1.0</u>	<u>N/A</u>	<u>N/A</u>	<u>56</u>	<u>3</u>	
<u>936</u>	<u>15</u>	<u>90.93</u>	<u>76</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>58</u>	<u>3</u>	
<u>951</u>	<u>30</u>	<u>99.15</u>	<u>79</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>59</u>	<u>3</u>	
<u>1006</u>	<u>45</u>	<u>106.85</u>	<u>83</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>60</u>	<u>3</u>	
<u>1021</u>	<u>60</u>	<u>114.788</u>							

Run Identification <u>M4-20</u>				Actual		Req'd		Vac	
				Pre Leak Check	<u>0.000</u>	< 0.02 or 4%	<u>2</u>		
				Post Leak Check	<u>0.000</u>	< 0.02 or 4%	<u>2</u>		
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
<u>1104</u>	<u>0</u>	<u>115.000</u>	<u>88</u>	<u>1.0</u>	<u>N/A</u>	<u>N/A</u>	<u>57</u>	<u>3</u>	
<u>1119</u>	<u>15</u>	<u>123.65</u>	<u>89</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>61</u>	<u>3</u>	
<u>1134</u>	<u>30</u>	<u>131.96</u>	<u>90</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>61</u>	<u>3</u>	
<u>1149</u>	<u>45</u>	<u>140.32</u>	<u>91</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>56</u>	<u>3</u>	
<u>1204</u>	<u>60</u>	<u>148.650</u>							

Run Identification <u>M4-21</u>				Actual		Req'd		Vac	
				Pre Leak Check	<u>0.000</u>	< 0.02 or 4%	<u>10</u>		
				Post Leak Check		< 0.02 or 4%			
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
<u>1231</u>	<u>0</u>	<u>149.200</u>	<u>89</u>	<u>1.0</u>	<u>N/A</u>	<u>N/A</u>	<u>51</u>	<u>3</u>	
<u>1301</u>	<u>15</u>	<u>157.72</u>	<u>90</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>58</u>	<u>4</u>	
<u>1316</u>	<u>30</u>	<u>166.39</u>	<u>91</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>60</u>	<u>7</u>	
<u>1346</u>	<u>45</u>	<u>172.82</u>	<u>91</u>	<u>↓</u>	<u>↓</u>	<u>↓</u>	<u>59</u>	<u>10</u>	
<u>1346</u>	<u>60</u>	<u>179.996</u>							

off 1238 upset condition
 ON 1252

Method 4 - Air Control Techniques, P.C.

Date 10/13/13

29.85
15224

Identification Information

Client	ENVIVA	Job	1911
Plant Name	Wiggins	Process	DRYER #2
City	Wiggins	State	MS

Sampling Information

Run Number		Balance Number	V1200
Sampling Date		Balance Type	Electronic
Recovery Date		Balance Level	✓
Personnel		Recovery Area	✓

Location Moisture Data

Run Number	19	20	21
<u>Impinger 1</u>			
Final Weight, grams/mls	970.0	908.2	922.2
Initial Weight, grams/mls	749.2	748.2	681.2
Condensed Water, grams	220.8	160	241.0
<u>Impinger 2</u>			
Final Weight, grams/mls	829.0	800.3	687.8
Initial Weight, grams/mls	790.3	680.0	674.0
Condensed Water, grams	38.7	120.3	13.8
<u>Impinger 3</u>			
Final Weight, grams/mls	609.3	603.1	612.5
Initial Weight, grams/mls	605.0	600.4	609.3
Condensed Water, grams	4.3	2.7	3.2
Condensed Water, grams			
<u>Silica Gel</u>			
Final Weight, grams	845.1	835.7	847.1
Initial Weight, grams	841.2	832.2	845.1
Adsorbed Water, grams	3.9	3.5	2.0
Adsorbed Water, grams			
Total Water, grams	267.7	286.5	260.0

$V_m(\text{std})$ = Volume of gas sampled at standard conditions (dscf)

$V_m(\text{std}) = ((\text{Gamma} * 17.64 * V_m * (\text{Pbar} + (\Delta H / 13.6))) / (T_m + 460))$

$V_{wc}(\text{std})$ = volume of water vapor at standard conditions (scf)

$V_{wc}(\text{std}) = (0.04707) * (\text{volume of water collected (mls)})$

B_{ws} = Mole fraction of water vapor

$B_{ws} = V_{wc}(\text{std}) / (V_m(\text{std}) + V_{wc}(\text{std}))$

Percent Moisture = $100 * B_{ws}$

APPENDIX B

Method 25A Data

Test Run 1 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/10/2013	10:17:27	29.2
10/10/2013	10:18:26	29.1
10/10/2013	10:19:26	29.4
10/10/2013	10:20:26	28.5
10/10/2013	10:21:26	29.2
10/10/2013	10:22:27	29.8
10/10/2013	10:23:27	30.5
10/10/2013	10:24:27	31.5
10/10/2013	10:25:27	30.8
10/10/2013	10:26:26	29.3
10/10/2013	10:27:26	29.3
10/10/2013	10:28:26	28.9
10/10/2013	10:29:27	29.5
10/10/2013	10:30:27	31.4
10/10/2013	10:31:27	31.1
10/10/2013	10:32:26	31.3
10/10/2013	10:33:26	31.2
10/10/2013	10:34:26	30.4
10/10/2013	10:35:27	30.4
10/10/2013	10:36:27	30.1
10/10/2013	10:37:27	29.7
10/10/2013	10:38:27	30.2
10/10/2013	10:39:26	29.2
10/10/2013	10:40:26	30.1
10/10/2013	10:41:26	30.3
10/10/2013	10:42:26	29.1
10/10/2013	10:43:27	29.5
10/10/2013	10:44:27	30.6
10/10/2013	10:45:27	29.7
10/10/2013	10:46:25	31
10/10/2013	10:47:26	30.1
10/10/2013	10:48:26	30.7
10/10/2013	10:49:26	31.6
10/10/2013	10:50:27	31.6
10/10/2013	10:51:27	32.3
10/10/2013	10:52:27	31.4
10/10/2013	10:53:27	30.4
10/10/2013	10:54:26	31.9
10/10/2013	10:55:26	31.8
10/10/2013	10:56:26	33.1
10/10/2013	10:57:26	32.8
10/10/2013	10:58:27	31.8
10/10/2013	10:59:27	32.5
10/10/2013	11:00:27	32.8
10/10/2013	11:01:26	30.2

10/10/2013	11:02:26	31.2
10/10/2013	11:03:26	30.7
10/10/2013	11:04:26	31.2
10/10/2013	11:05:27	32.7
10/10/2013	11:06:27	31.6
10/10/2013	11:07:27	31.2
10/10/2013	11:08:25	32.5
10/10/2013	11:09:26	31
10/10/2013	11:10:26	30.8
10/10/2013	11:11:26	28.9
10/10/2013	11:12:26	30.9
10/10/2013	11:13:27	31.9
10/10/2013	11:14:27	32.1
10/10/2013	11:15:27	32.6
10/10/2013	11:16:26	34
Average	1807 sampl	30.8
Test Run 1 End		

Test Run 2 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/10/2013	10:37:12	33.22
10/10/2013	10:38:13	32.73
10/10/2013	10:39:13	33.22
10/10/2013	10:40:13	33.21
10/10/2013	10:41:13	31.78
10/10/2013	10:42:14	29.83
10/10/2013	10:43:14	31.37
10/10/2013	10:44:12	31.5
10/10/2013	10:45:13	33.24
10/10/2013	10:46:13	32.96
10/10/2013	10:47:13	32.52
10/10/2013	10:48:13	32.17
10/10/2013	10:49:14	31.8
10/10/2013	10:50:14	30.68
10/10/2013	10:51:12	29.76
10/10/2013	10:52:12	31.03
10/10/2013	10:53:13	31.9
10/10/2013	10:54:13	32.57
10/10/2013	10:55:13	32.4
10/10/2013	10:56:14	32.68
10/10/2013	10:57:14	33.18
10/10/2013	10:58:12	33.26
10/10/2013	10:59:12	32.76
10/10/2013	11:00:13	31.1
10/10/2013	11:01:12	30.85
10/10/2013	11:02:14	30.84
10/10/2013	11:03:13	30.27
10/10/2013	11:04:12	30.6
10/10/2013	11:05:14	32.18
10/10/2013	11:06:13	30.96
10/10/2013	11:07:12	31.41
10/10/2013	11:08:12	30.82
10/10/2013	11:09:13	31.24
10/10/2013	11:10:13	31.94
10/10/2013	11:11:14	31.25
10/10/2013	11:12:13	30.81
10/10/2013	11:13:12	32.84
10/10/2013	11:14:12	32.11
10/10/2013	11:15:14	32.71
10/10/2013	11:16:13	32.57
10/10/2013	11:17:12	33.7
10/10/2013	11:18:14	33.87
10/10/2013	11:19:13	32.8
10/10/2013	11:20:13	31.93
10/10/2013	11:21:14	33.89

10/10/2013	11:22:13	33.12
10/10/2013	11:23:13	32.56
10/10/2013	11:24:14	32.31
10/10/2013	11:25:13	33.49
10/10/2013	11:26:12	34.83
10/10/2013	11:27:14	34.8
10/10/2013	11:28:13	33.96
10/10/2013	11:29:13	33.5
10/10/2013	11:30:14	34.21
10/10/2013	11:31:13	32.7
10/10/2013	11:32:13	31.67
10/10/2013	11:33:12	31.32
10/10/2013	11:34:13	31.95
10/10/2013	11:35:13	31.59
10/10/2013	11:36:14	31.24
10/10/2013	11:37:13	32.88

Test Run 3 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/10/2013	11:51:37	27.47
10/10/2013	11:52:37	25.81
10/10/2013	11:53:37	25.62
10/10/2013	11:54:38	26.13
10/10/2013	11:55:36	27.21
10/10/2013	11:56:36	27.54
10/10/2013	11:57:36	27.06
10/10/2013	11:58:37	27.89
10/10/2013	11:59:37	27.66
10/10/2013	12:00:37	26.76
10/10/2013	12:01:38	26.92
10/10/2013	12:02:38	26.42
10/10/2013	12:03:36	25.01
10/10/2013	12:04:36	25.47
10/10/2013	12:05:37	25.98
10/10/2013	12:06:37	26.95
10/10/2013	12:07:37	27.79
10/10/2013	12:08:37	26.71
10/10/2013	12:09:38	27.38
10/10/2013	12:10:38	27.84
10/10/2013	12:11:36	25.99
10/10/2013	12:12:36	25.7
10/10/2013	12:13:37	24.64
10/10/2013	12:14:37	25.2
10/10/2013	12:15:37	25.22
10/10/2013	12:16:37	24.65
10/10/2013	12:17:38	24.05
10/10/2013	12:18:36	23.8
10/10/2013	12:19:36	22.94
10/10/2013	12:20:36	23.17
10/10/2013	12:21:37	24.1
10/10/2013	12:22:37	25.63
10/10/2013	12:23:37	26.37
10/10/2013	12:24:37	26.85
10/10/2013	12:25:38	26.02
10/10/2013	12:26:36	25.65
10/10/2013	12:27:36	25.72
10/10/2013	12:28:37	27.03
10/10/2013	12:29:37	26.23
10/10/2013	12:30:37	25.87
10/10/2013	12:31:37	25.97
10/10/2013	12:32:38	25.53
10/10/2013	12:33:38	25.25
10/10/2013	12:34:36	26.76
10/10/2013	12:35:36	27.16

10/10/2013	12:36:37	27.29
10/10/2013	12:37:37	27.02
10/10/2013	12:38:37	27.31
10/10/2013	12:39:37	28.11
10/10/2013	12:40:38	28.86
10/10/2013	12:41:36	28.19
10/10/2013	12:42:36	27.22
10/10/2013	12:43:37	27.74
10/10/2013	12:44:37	28.08
10/10/2013	12:45:37	26.91
10/10/2013	12:46:38	26.97
10/10/2013	12:47:38	27.99
10/10/2013	12:48:36	27.63
10/10/2013	12:49:36	26.3
10/10/2013	12:50:37	25.95
Average	1802 sampl	26.38
Test Run 3 End		

Test Run 4 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/10/2013	17:39:30	73.6
10/10/2013	17:40:31	73.7
10/10/2013	17:41:31	74.2
10/10/2013	17:42:31	74.3
10/10/2013	17:43:31	74.4
10/10/2013	17:44:32	74.6
10/10/2013	17:45:32	75.3
10/10/2013	17:46:32	75.7
10/10/2013	17:47:30	75.7
10/10/2013	17:48:31	75.6
10/10/2013	17:49:31	75
10/10/2013	17:50:31	74.2
10/10/2013	17:51:31	72.5
10/10/2013	17:52:32	71.5
10/10/2013	17:53:32	70.7
10/10/2013	17:54:30	70
10/10/2013	17:55:30	69.3
10/10/2013	17:56:31	68.6
10/10/2013	17:57:31	68
10/10/2013	17:58:31	67.7
10/10/2013	17:59:32	67.1
10/10/2013	18:00:32	66.8
10/10/2013	18:01:30	66.4
10/10/2013	18:02:30	66
10/10/2013	18:03:31	65
10/10/2013	18:04:31	64.5
10/10/2013	18:05:31	64.3
10/10/2013	18:06:31	64.1
10/10/2013	18:07:32	64.8
10/10/2013	18:08:32	65.5
10/10/2013	18:09:30	65.6
10/10/2013	18:10:31	65.7
10/10/2013	18:11:31	65.8
10/10/2013	18:12:31	65.8
10/10/2013	18:13:31	66.6
10/10/2013	18:14:32	66.7
10/10/2013	18:15:32	67
10/10/2013	18:16:30	67
10/10/2013	18:17:30	66.2
10/10/2013	18:18:31	65.5
10/10/2013	18:19:31	65
10/10/2013	18:20:31	64.5
10/10/2013	18:21:32	63.4
10/10/2013	18:22:32	62.8
10/10/2013	18:23:30	62.2

10/10/2013	18:24:30	62
10/10/2013	18:25:31	62.2
10/10/2013	18:26:31	62.2
10/10/2013	18:27:31	62.6
10/10/2013	18:28:31	62.4
10/10/2013	18:29:32	61.7
10/10/2013	18:30:32	61.8
10/10/2013	18:31:30	61.4
10/10/2013	18:32:30	61.5
10/10/2013	18:33:31	61.3
10/10/2013	18:34:31	61.3
10/10/2013	18:35:31	61.1
10/10/2013	18:36:31	61.3
10/10/2013	18:37:32	60.8
10/10/2013	18:38:30	60.2
10/10/2013	18:39:30	60.4
Average	1837 sampl	66.7
Test Run 4 End		

Test Run 5 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	10:00:39	59.48
10/11/2013	10:01:40	59.35
10/11/2013	10:02:40	59.64
10/11/2013	10:03:40	59.19
10/11/2013	10:04:40	59.7
10/11/2013	10:05:41	60.45
10/11/2013	10:06:41	60.54
10/11/2013	10:07:41	60.86
10/11/2013	10:08:40	61.28
10/11/2013	10:09:40	62.22
10/11/2013	10:10:40	62.62
10/11/2013	10:11:40	62.46
10/11/2013	10:12:40	62.22
10/11/2013	10:13:41	61.96
10/11/2013	10:14:41	61.71
10/11/2013	10:15:39	61.79
10/11/2013	10:16:40	61.65
10/11/2013	10:17:40	61.76
10/11/2013	10:18:40	61.82
10/11/2013	10:19:40	61.41
10/11/2013	10:20:41	60.91
10/11/2013	10:21:41	60.34
10/11/2013	10:22:41	60.35
10/11/2013	10:23:39	60.17
10/11/2013	10:24:40	60.48
10/11/2013	10:25:40	60.31
10/11/2013	10:26:40	60.03
10/11/2013	10:27:40	60.26
10/11/2013	10:28:41	60.17
10/11/2013	10:29:41	59.83
10/11/2013	10:30:41	59.58
10/11/2013	10:31:40	60.56
10/11/2013	10:32:40	60.96
10/11/2013	10:33:40	60.79
10/11/2013	10:34:40	61.26
10/11/2013	10:35:41	61.22
10/11/2013	10:36:41	61.09
10/11/2013	10:37:41	61.12
10/11/2013	10:38:39	61.86
10/11/2013	10:39:40	62.32
10/11/2013	10:40:40	62.49
10/11/2013	10:41:40	62.15
10/11/2013	10:42:41	62.22
10/11/2013	10:43:41	62.04
10/11/2013	10:44:41	61.73

10/11/2013	10:45:41	60.99
10/11/2013	10:46:40	61.3
10/11/2013	10:47:40	61.17
10/11/2013	10:48:40	62.35
10/11/2013	10:49:40	63.58
10/11/2013	10:50:41	63.57
10/11/2013	10:51:41	65.12
10/11/2013	10:52:41	67.32
10/11/2013	10:53:39	67.58
10/11/2013	10:54:40	67.4
10/11/2013	10:55:40	66.77
10/11/2013	10:56:40	66
10/11/2013	10:57:40	65.74
10/11/2013	10:58:41	64.85
10/11/2013	10:59:41	64.09
Average	1810 sampl	61.92
Test Run 5 End		

Test Run 6 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	11:37:39	62.85
10/11/2013	11:38:39	63.21
10/11/2013	11:39:40	63.49
10/11/2013	11:40:38	63.72
10/11/2013	11:41:38	64.5
10/11/2013	11:42:38	65.32
10/11/2013	11:43:39	66.16
10/11/2013	11:44:39	66.6
10/11/2013	11:45:39	66.81
10/11/2013	11:46:40	66.6
10/11/2013	11:47:38	64.85
10/11/2013	11:48:38	62.59
10/11/2013	11:49:38	60.21
10/11/2013	11:50:38	58.27
10/11/2013	11:51:39	56.95
10/11/2013	11:52:39	55.02
10/11/2013	11:53:39	53.86
10/11/2013	11:54:39	52.91
10/11/2013	11:55:40	52.4
10/11/2013	11:56:38	52.38
10/11/2013	11:57:38	52.86
10/11/2013	11:58:39	53.87
10/11/2013	11:59:39	54.56
10/11/2013	12:00:39	53.55
10/11/2013	12:01:39	52.72
10/11/2013	12:02:39	52.05
10/11/2013	12:03:40	51.53
10/11/2013	12:04:38	51.4
10/11/2013	12:05:38	52.07
10/11/2013	12:06:38	52.86
10/11/2013	12:07:39	53.12
10/11/2013	12:08:39	53.31
10/11/2013	12:09:39	52.77
10/11/2013	12:10:40	51.76
10/11/2013	12:11:40	51.02
10/11/2013	12:12:38	51.05
10/11/2013	12:13:38	52.13
10/11/2013	12:14:39	52.93
10/11/2013	12:15:39	53.34
10/11/2013	12:16:39	53.7
10/11/2013	12:17:39	53.91
10/11/2013	12:18:40	54.85
10/11/2013	12:19:38	55.39
10/11/2013	12:20:38	55.82
10/11/2013	12:21:38	55.66

10/11/2013	12:22:39	55.8
10/11/2013	12:23:39	56.58
10/11/2013	12:24:39	57.45
10/11/2013	12:25:40	58.57
10/11/2013	12:26:40	59.56
10/11/2013	12:27:38	60.26
10/11/2013	12:28:38	60.52
10/11/2013	12:29:39	60.23
10/11/2013	12:30:39	59.97
10/11/2013	12:31:39	59.98
10/11/2013	12:32:39	58.38
10/11/2013	12:33:40	57.52
10/11/2013	12:34:38	58.26
10/11/2013	12:35:38	59.53
10/11/2013	12:36:38	60.41
Average	1796 sampl	57.17
Test Run 6 End		

Test Run 7 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	13:43:41	29.28
10/11/2013	13:44:42	27.18
10/11/2013	13:45:42	25.85
10/11/2013	13:46:40	24.55
10/11/2013	13:47:40	23.31
10/11/2013	13:48:41	22.64
10/11/2013	13:49:41	22.37
10/11/2013	13:50:41	22.49
10/11/2013	13:51:42	22.37
10/11/2013	13:52:42	22.04
10/11/2013	13:53:40	22.25
10/11/2013	13:54:40	22.98
10/11/2013	13:55:41	22.9
10/11/2013	13:56:41	22.72
10/11/2013	13:57:41	23.05
10/11/2013	13:58:42	23.38
10/11/2013	13:59:42	23.44
10/11/2013	14:00:40	24.2
10/11/2013	14:01:40	24.19
10/11/2013	14:02:41	23.32
10/11/2013	14:03:41	22.78
10/11/2013	14:04:41	22.4
10/11/2013	14:05:41	22.24
10/11/2013	14:06:42	22.53
10/11/2013	14:07:40	22.54
10/11/2013	14:08:40	22
10/11/2013	14:09:40	21.36
10/11/2013	14:10:41	20.81
10/11/2013	14:11:41	20.6
10/11/2013	14:12:41	20.52
10/11/2013	14:13:41	20.67
10/11/2013	14:14:42	21.18
10/11/2013	14:15:40	22.48
10/11/2013	14:16:40	23.46
10/11/2013	14:17:41	23.6
10/11/2013	14:18:41	24.02
10/11/2013	14:19:41	24.31
10/11/2013	14:20:41	24.25
10/11/2013	14:21:42	24.44
10/11/2013	14:22:42	24.59
10/11/2013	14:23:40	24.59
10/11/2013	14:24:40	25.03
10/11/2013	14:25:40	25.21
10/11/2013	14:26:41	25.16
10/11/2013	14:27:41	25.61

10/11/2013	14:28:41	25.91
10/11/2013	14:29:42	24.74
10/11/2013	14:30:42	24.82
10/11/2013	14:31:40	24.18
10/11/2013	14:32:40	23.94
10/11/2013	14:33:41	24.63
10/11/2013	14:34:41	25.19
10/11/2013	14:35:41	25.92
10/11/2013	14:36:41	26.43
10/11/2013	14:37:42	25.26
10/11/2013	14:38:42	24.93
10/11/2013	14:39:40	25.61
10/11/2013	14:40:40	25.25
10/11/2013	14:41:41	24.92
10/11/2013	14:42:41	24.81
Average	1795 sampl	23.8
Test Run 7 End		

Test Run 8 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	15:08:58	20.89
10/11/2013	15:09:58	21.18
10/11/2013	15:10:56	21.36
10/11/2013	15:11:57	21.39
10/11/2013	15:12:57	21.49
10/11/2013	15:13:57	21.51
10/11/2013	15:14:58	21.66
10/11/2013	15:15:58	21.02
10/11/2013	15:16:58	20.12
10/11/2013	15:17:56	19.71
10/11/2013	15:18:57	19.67
10/11/2013	15:19:57	19.07
10/11/2013	15:20:57	19.24
10/11/2013	15:21:57	19.85
10/11/2013	15:22:58	20.21
10/11/2013	15:23:58	20.9
10/11/2013	15:24:56	21.72
10/11/2013	15:25:57	22.45
10/11/2013	15:26:57	23.3
10/11/2013	15:27:57	23.07
10/11/2013	15:28:57	22.47
10/11/2013	15:29:58	22.24
10/11/2013	15:30:58	22.14
10/11/2013	15:31:58	21.87
10/11/2013	15:32:56	22.09
10/11/2013	15:33:57	22.17
10/11/2013	15:34:57	22.55
10/11/2013	15:35:57	22.32
10/11/2013	15:36:57	21.72
10/11/2013	15:37:58	21.14
10/11/2013	15:38:58	21.1
10/11/2013	15:39:58	21.29
10/11/2013	15:40:56	21.44
10/11/2013	15:41:57	21.58
10/11/2013	15:42:57	22.64
10/11/2013	15:43:57	22.48
10/11/2013	15:44:57	22.65
10/11/2013	15:45:58	22.37
10/11/2013	15:46:58	22.73
10/11/2013	15:47:56	22.8
10/11/2013	15:48:57	22.34
10/11/2013	15:49:57	21.76
10/11/2013	15:50:57	21.83
10/11/2013	15:51:57	22.04
10/11/2013	15:52:58	22.15

10/11/2013	15:53:58	22.07
10/11/2013	15:54:58	22.66
10/11/2013	15:55:58	22.99
10/11/2013	15:56:57	22.84
10/11/2013	15:57:57	22.83
10/11/2013	15:58:57	22.2
10/11/2013	15:59:58	21.03
10/11/2013	16:00:58	19.77
10/11/2013	16:01:58	18.88
10/11/2013	16:02:56	18.32
10/11/2013	16:03:57	17.86
10/11/2013	16:04:57	18.62
10/11/2013	16:05:57	18.41
10/11/2013	16:06:57	18.6
10/11/2013	16:07:58	19.1
Average	1796 sampl	21.29
Test Run 8 End		

Test Run 9 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	16:29:59	22.84
10/11/2013	16:30:59	21.54
10/11/2013	16:31:59	21.11
10/11/2013	16:33:00	21.4
10/11/2013	16:34:00	21.21
10/11/2013	16:35:00	21.39
10/11/2013	16:36:00	21.79
10/11/2013	16:36:59	23.24
10/11/2013	16:37:59	23.79
10/11/2013	16:38:59	24.8
10/11/2013	16:39:59	25.11
10/11/2013	16:41:00	26.01
10/11/2013	16:42:00	28.05
10/11/2013	16:43:00	29.59
10/11/2013	16:44:00	29.65
10/11/2013	16:44:59	29.74
10/11/2013	16:45:59	29.86
10/11/2013	16:46:59	33.48
10/11/2013	16:48:00	32.59
10/11/2013	16:49:00	28.94
10/11/2013	16:49:59	26.37
10/11/2013	16:50:59	25.7
10/11/2013	16:51:59	24.69
10/11/2013	16:53:00	24.55
10/11/2013	16:54:00	24.78
10/11/2013	16:55:00	25.37
10/11/2013	16:55:59	26.6
10/11/2013	16:56:59	27.42
10/11/2013	16:57:59	26.35
10/11/2013	16:58:59	25.6
10/11/2013	17:00:00	25.52
10/11/2013	17:01:00	25.32
10/11/2013	17:02:00	24.67
10/11/2013	17:03:00	24.39
10/11/2013	17:04:01	24.2
10/11/2013	17:04:59	23.43
10/11/2013	17:05:59	22.29
10/11/2013	17:06:59	21.55
10/11/2013	17:08:00	21.18
10/11/2013	17:09:00	21.33
10/11/2013	17:10:00	21.67
10/11/2013	17:10:59	21.91
10/11/2013	17:11:59	22.59
10/11/2013	17:12:59	22.87
10/11/2013	17:14:00	23.27

10/11/2013	17:15:00	23.85
10/11/2013	17:16:00	23.83
10/11/2013	17:17:00	23.05
10/11/2013	17:17:59	23.11
10/11/2013	17:18:59	23.12
10/11/2013	17:19:59	24.45
10/11/2013	17:21:00	24.59
10/11/2013	17:22:00	24.41
10/11/2013	17:23:00	24.36
10/11/2013	17:24:00	25.25
10/11/2013	17:24:59	25.58
10/11/2013	17:25:59	26.03
10/11/2013	17:26:59	26.29
10/11/2013	17:27:59	26.55
10/11/2013	17:29:00	26.07
10/11/2013	17:30:00	25.36
10/11/2013	17:31:00	24.68
10/11/2013	17:32:00	24.5
10/11/2013	17:32:59	24.26
10/11/2013	17:33:59	24.15
Average	1951 sampl	24.82
Test Run 9 End		

Test Run 10 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	18:11:17	29.88
10/11/2013	18:12:18	33.18
10/11/2013	18:13:18	31
10/11/2013	18:14:18	22.29
10/11/2013	18:15:18	19.06
10/11/2013	18:16:19	19
10/11/2013	18:17:19	21.06
10/11/2013	18:18:19	23.21
10/11/2013	18:19:17	22.71
10/11/2013	18:20:18	23.92
10/11/2013	18:21:18	23.38
10/11/2013	18:22:18	22.46
10/11/2013	18:23:19	23.73
10/11/2013	18:24:19	27.16
10/11/2013	18:25:19	28.89
10/11/2013	18:26:17	27.17
10/11/2013	18:27:18	22.65
10/11/2013	18:28:18	22.36
10/11/2013	18:29:18	23.07
10/11/2013	18:30:18	23.39
10/11/2013	18:31:19	21.74
10/11/2013	18:32:19	21
10/11/2013	18:33:19	21.29
10/11/2013	18:34:17	20.98
10/11/2013	18:35:18	18.39
10/11/2013	18:36:18	18.16
10/11/2013	18:37:18	18.91
10/11/2013	18:38:19	19.32
10/11/2013	18:39:19	21.57
10/11/2013	18:40:19	25.3
10/11/2013	18:41:17	31.9
10/11/2013	18:42:18	38.29
10/11/2013	18:43:18	33.17
10/11/2013	18:44:18	31.99
10/11/2013	18:45:19	25.13
10/11/2013	18:46:19	21.93
10/11/2013	18:47:19	19.45
10/11/2013	18:48:19	19.52
10/11/2013	18:49:18	18.88
10/11/2013	18:50:18	20.12
10/11/2013	18:51:18	20.89
10/11/2013	18:52:18	21.09
10/11/2013	18:53:19	21.01
10/11/2013	18:54:19	19.4
10/11/2013	18:55:17	19.85

10/11/2013	18:56:18	24.65
10/11/2013	18:57:18	24.98
10/11/2013	18:58:18	22.99
10/11/2013	18:59:18	23.31
10/11/2013	19:00:19	25.22
10/11/2013	19:01:19	25.84
10/11/2013	19:02:19	27.93
10/11/2013	19:03:17	30.86
10/11/2013	19:04:18	37.73
10/11/2013	19:05:18	41.49
10/11/2013	19:06:18	33.42
10/11/2013	19:07:19	28.12
10/11/2013	19:08:19	24.42
10/11/2013	19:09:19	28.47
10/11/2013	19:10:17	32.11
10/11/2013	19:11:18	35.91
10/11/2013	19:12:18	31.9
Average	1881 sampl	25.19
Test Run 10 End		

Test Run 11 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	19:35:45	16.3
10/11/2013	19:36:45	16.9
10/11/2013	19:37:45	19.2
10/11/2013	19:38:46	19.43
10/11/2013	19:39:46	20.92
10/11/2013	19:40:46	21.44
10/11/2013	19:41:45	23.07
10/11/2013	19:42:45	23.32
10/11/2013	19:43:45	24.41
10/11/2013	19:44:46	25.71
10/11/2013	19:45:46	30.06
10/11/2013	19:46:46	36.61
10/11/2013	19:47:46	35.99
10/11/2013	19:48:46	29.55
10/11/2013	19:49:45	23.62
10/11/2013	19:50:45	23.25
10/11/2013	19:51:45	22.61
10/11/2013	19:52:45	23.8
10/11/2013	19:53:46	21.47
10/11/2013	19:54:46	20.75
10/11/2013	19:55:46	21.14
10/11/2013	19:56:46	22.12
10/11/2013	19:57:45	23.08
10/11/2013	19:58:45	22.57
10/11/2013	19:59:46	25.43
10/11/2013	20:00:46	26.18
10/11/2013	20:01:46	27.36
10/11/2013	20:02:46	26.43
10/11/2013	20:03:45	32.28
10/11/2013	20:04:45	29.23
10/11/2013	20:05:45	34.45
10/11/2013	20:06:45	34.13
10/11/2013	20:07:46	30.96
10/11/2013	20:08:46	30.2
10/11/2013	20:09:46	32.75
10/11/2013	20:10:47	36.19
10/11/2013	20:11:45	38.78
10/11/2013	20:12:45	37.58
10/11/2013	20:13:45	34.83
10/11/2013	20:14:46	30.77
10/11/2013	20:15:46	30.88
10/11/2013	20:16:46	31.74
10/11/2013	20:17:46	34.53
10/11/2013	20:18:45	42.51
10/11/2013	20:19:45	44.65

10/11/2013	20:20:45	35.45
10/11/2013	20:21:46	25.21
10/11/2013	20:22:46	23.77
10/11/2013	20:23:46	28.87
10/11/2013	20:24:46	36.75
10/11/2013	20:25:45	45.05
10/11/2013	20:26:45	45.64
10/11/2013	20:27:45	41.52
10/11/2013	20:28:45	35.53
10/11/2013	20:29:46	33.91
10/11/2013	20:30:46	34.59
10/11/2013	20:31:46	29.84
10/11/2013	20:32:46	31.48
10/11/2013	20:33:45	39.63
10/11/2013	20:34:45	36.38
Average	1794 sampl	29.72
Test Run 11 End		

Test Run 12 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	20:49:06	22.17
10/11/2013	20:50:04	21.67
10/11/2013	20:51:04	23.4
10/11/2013	20:52:05	24.29
10/11/2013	20:53:05	25.04
10/11/2013	20:54:05	26.33
10/11/2013	20:55:05	26.92
10/11/2013	20:56:06	25.87
10/11/2013	20:57:06	25.72
10/11/2013	20:58:04	25.14
10/11/2013	20:59:04	25.52
10/11/2013	21:00:05	25.37
10/11/2013	21:01:05	25.64
10/11/2013	21:02:05	26.15
10/11/2013	21:03:05	26.08
10/11/2013	21:04:06	24.52
10/11/2013	21:05:04	25.79
10/11/2013	21:06:04	26.55
10/11/2013	21:07:04	27.79
10/11/2013	21:08:05	28.72
10/11/2013	21:09:05	27.24
10/11/2013	21:10:05	30.06
10/11/2013	21:11:05	33.03
10/11/2013	21:12:06	28.99
10/11/2013	21:13:04	20.95
10/11/2013	21:14:04	19.34
10/11/2013	21:15:05	19.67
10/11/2013	21:16:05	21.55
10/11/2013	21:17:05	26.17
10/11/2013	21:18:05	34.11
10/11/2013	21:19:06	29.02
10/11/2013	21:20:06	23.47
10/11/2013	21:21:04	18.29
10/11/2013	21:22:04	20.47
10/11/2013	21:23:05	20.63
10/11/2013	21:24:05	18.82
10/11/2013	21:25:05	18.74
10/11/2013	21:26:06	17.07
10/11/2013	21:27:04	17.1
10/11/2013	21:28:04	18.57
10/11/2013	21:29:05	22.44
10/11/2013	21:30:05	23.51
10/11/2013	21:31:05	23.1
10/11/2013	21:32:05	23.66
10/11/2013	21:33:05	26.36

10/11/2013	21:34:06	29.16
10/11/2013	21:35:04	30.42
10/11/2013	21:36:04	24.58
10/11/2013	21:37:05	22.02
10/11/2013	21:38:05	21.27
10/11/2013	21:39:05	22.01
10/11/2013	21:40:05	21.7
10/11/2013	21:41:06	25.89
10/11/2013	21:42:06	27.16
10/11/2013	21:43:04	26.97
10/11/2013	21:44:04	27.62
10/11/2013	21:45:04	25.38
10/11/2013	21:46:05	22.73
10/11/2013	21:47:05	22.71
10/11/2013	21:48:05	24.06
Average	1802 samp	24.43
Test Run 12 End		

Test Run 13 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/12/2013	8:58:20	33.01
10/12/2013	8:59:20	33.09
10/12/2013	9:00:21	33.69
10/12/2013	9:01:21	33.38
10/12/2013	9:02:19	34.58
10/12/2013	9:03:19	34.24
10/12/2013	9:04:20	32.82
10/12/2013	9:05:20	31.76
10/12/2013	9:06:20	31.56
10/12/2013	9:07:20	32.43
10/12/2013	9:08:21	32.07
10/12/2013	9:09:21	33.62
10/12/2013	9:10:21	35.22
10/12/2013	9:11:19	35.73
10/12/2013	9:12:20	36.7
10/12/2013	9:13:20	38.36
10/12/2013	9:14:20	39.65
10/12/2013	9:15:20	36.74
10/12/2013	9:16:21	34.73
10/12/2013	9:17:21	37.06
10/12/2013	9:18:19	39.31
10/12/2013	9:19:19	40.7
10/12/2013	9:20:20	41.32
10/12/2013	9:21:20	42.72
10/12/2013	9:22:20	44.45
10/12/2013	9:23:21	41.77
10/12/2013	9:24:21	41.75
10/12/2013	9:25:19	40.84
10/12/2013	9:26:19	40.01
10/12/2013	9:27:20	39.81
10/12/2013	9:28:20	38.16
10/12/2013	9:29:20	36.14
10/12/2013	9:30:20	33.8
10/12/2013	9:31:21	42.88
10/12/2013	9:32:21	44.68
10/12/2013	9:33:19	48.06
10/12/2013	9:34:19	48.98
10/12/2013	9:35:20	49.89
10/12/2013	9:36:20	50.59
10/12/2013	9:37:20	48.17
10/12/2013	9:38:20	42.62
10/12/2013	9:39:21	41.05
10/12/2013	9:40:21	40.93
10/12/2013	9:41:19	38.08
10/12/2013	9:42:19	36.88

10/12/2013	9:43:20	38.28
10/12/2013	9:44:20	37.83
10/12/2013	9:45:20	38.96
10/12/2013	9:46:20	39.74
10/12/2013	9:47:21	39.65
10/12/2013	9:48:21	38.16
10/12/2013	9:49:19	36.49
10/12/2013	9:50:19	37.79
10/12/2013	9:51:20	38.86
10/12/2013	9:52:20	38.2
10/12/2013	9:53:20	39.36
10/12/2013	9:54:21	42.28
10/12/2013	9:55:21	42.37
10/12/2013	9:56:19	42.48
10/12/2013	9:57:19	42.15
10/12/2013	9:58:20	42.58
Average	1843 sampl	39.05
Test Run 13 End		

Test Run 14 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/12/2013	10:23:19	38.78
10/12/2013	10:24:19	38.95
10/12/2013	10:25:20	37.38
10/12/2013	10:26:20	35.26
10/12/2013	10:27:20	33.47
10/12/2013	10:28:21	33.54
10/12/2013	10:29:21	35.1
10/12/2013	10:30:19	36.39
10/12/2013	10:31:19	38.16
10/12/2013	10:32:20	37.83
10/12/2013	10:33:20	38.5
10/12/2013	10:34:20	39.8
10/12/2013	10:35:20	41.11
10/12/2013	10:36:20	43.31
10/12/2013	10:37:21	43.12
10/12/2013	10:38:19	41.6
10/12/2013	10:39:19	40.09
10/12/2013	10:40:20	41.76
10/12/2013	10:41:20	37.42
10/12/2013	10:42:20	35.32
10/12/2013	10:43:20	36.85
10/12/2013	10:44:21	37.03
10/12/2013	10:45:21	37.63
10/12/2013	10:46:19	37.23
10/12/2013	10:47:19	36.6
10/12/2013	10:48:20	36.58
10/12/2013	10:49:20	34.3
10/12/2013	10:50:20	32.95
10/12/2013	10:51:20	35.86
10/12/2013	10:52:21	40.36
10/12/2013	10:53:21	41.13
10/12/2013	10:54:19	40.92
10/12/2013	10:55:19	38.94
10/12/2013	10:56:20	35.9
10/12/2013	10:57:20	34.71
10/12/2013	10:58:20	35.12
10/12/2013	10:59:20	38.4
10/12/2013	11:00:21	38.46
10/12/2013	11:01:19	38.96
10/12/2013	11:02:19	39.11
10/12/2013	11:03:20	39.66
10/12/2013	11:04:20	37.43
10/12/2013	11:05:20	32.13
10/12/2013	11:06:20	25.88
10/12/2013	11:07:21	22.76

10/12/2013	11:08:19	20.44
10/12/2013	11:09:19	21.39
10/12/2013	11:10:20	19.1
10/12/2013	11:11:20	20.05
10/12/2013	11:12:20	19.67
10/12/2013	11:13:20	20.48
10/12/2013	11:14:21	23.27
10/12/2013	11:15:21	23.34
10/12/2013	11:16:19	22.56
10/12/2013	11:17:19	20.89
10/12/2013	11:18:20	21.23
10/12/2013	11:19:20	22.61
10/12/2013	11:20:20	24.32
10/12/2013	11:21:20	25.83
10/12/2013	11:22:21	25.38
Average	1802 sampl	33.29
Test Run 14 End		

Test Run 15 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/12/2013	11:41:41	42.04
10/12/2013	11:42:42	38.71
10/12/2013	11:43:42	37.78
10/12/2013	11:44:42	33.87
10/12/2013	11:45:42	33.86
10/12/2013	11:46:43	38.57
10/12/2013	11:47:43	38.29
10/12/2013	11:48:41	37.43
10/12/2013	11:49:41	35.42
10/12/2013	11:50:42	35.35
10/12/2013	11:51:42	36.29
10/12/2013	11:52:42	36.18
10/12/2013	11:53:42	39.17
10/12/2013	11:54:43	41.21
10/12/2013	11:55:43	45.09
10/12/2013	11:56:41	44.99
10/12/2013	11:57:42	42.66
10/12/2013	11:58:42	41.22
10/12/2013	11:59:42	40.64
10/12/2013	12:00:42	41.76
10/12/2013	12:01:43	41.25
10/12/2013	12:02:43	40.48
10/12/2013	12:03:41	40.5
10/12/2013	12:04:41	35.92
10/12/2013	12:05:42	39.32
10/12/2013	12:06:42	39.55
10/12/2013	12:07:42	37.98
10/12/2013	12:08:42	37.41
10/12/2013	12:09:43	34.56
10/12/2013	12:10:43	32.14
10/12/2013	12:11:41	30.17
10/12/2013	12:12:42	29.4
10/12/2013	12:13:42	31.84
10/12/2013	12:14:42	31.63
10/12/2013	12:15:42	30.68
10/12/2013	12:16:43	30.88
10/12/2013	12:17:43	31.21
10/12/2013	12:18:41	33.29
10/12/2013	12:19:41	35.08
10/12/2013	12:20:42	36.57
10/12/2013	12:21:42	34.06
10/12/2013	12:22:42	32.44
10/12/2013	12:23:43	31.77
10/12/2013	12:24:43	31.01
10/12/2013	12:25:41	31.56

10/12/2013	12:26:41	32.83
10/12/2013	12:27:42	31.92
10/12/2013	12:28:42	33.46
10/12/2013	12:29:42	33.76
10/12/2013	12:30:43	33.98
10/12/2013	12:31:43	33.51
10/12/2013	12:32:41	33.07
10/12/2013	12:33:41	32.11
10/12/2013	12:34:41	34.32
10/12/2013	12:35:42	32.87
10/12/2013	12:36:42	33.76
10/12/2013	12:37:42	35.71
10/12/2013	12:38:42	32.83
10/12/2013	12:39:43	31.48
10/12/2013	12:40:43	32.15
Average	1794 sampl	35.65
Test Run 15 End		

Test Run 1 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/12/2013	15:09:26	1001.1
10/12/2013	15:10:26	1022.4
10/12/2013	15:11:26	1009.4
10/12/2013	15:12:26	1027.4
10/12/2013	15:13:27	1045.1
10/12/2013	15:14:27	1073.3
10/12/2013	15:15:26	1039.6
10/12/2013	15:16:26	1038.3
10/12/2013	15:17:26	1049.6
10/12/2013	15:18:26	1074.6
10/12/2013	15:19:27	1072.1
10/12/2013	15:20:27	1010.8
10/12/2013	15:21:27	962.7
10/12/2013	15:22:25	922.6
10/12/2013	15:23:26	912.5
10/12/2013	15:24:26	885.5
10/12/2013	15:25:26	971
10/12/2013	15:26:27	1016
10/12/2013	15:27:27	1059.8
10/12/2013	15:28:27	1099.5
10/12/2013	15:29:25	1128.8
10/12/2013	15:30:26	1126.8
10/12/2013	15:31:26	1103.4
10/12/2013	15:32:26	1069.6
10/12/2013	15:33:27	1011.3
10/12/2013	15:34:27	1040.7
10/12/2013	15:35:27	1079.2
10/12/2013	15:36:25	1094
10/12/2013	15:37:26	1082.4
10/12/2013	15:38:26	1112.7
10/12/2013	15:39:26	1120.2
10/12/2013	15:40:26	1154.1
10/12/2013	15:41:27	1168.4
10/12/2013	15:42:27	1163.2
10/12/2013	15:43:27	1133.2
10/12/2013	15:44:26	1049.9
10/12/2013	15:45:26	1053.5
10/12/2013	15:46:26	1027
10/12/2013	15:47:26	1020.1
10/12/2013	15:48:27	1022.4
10/12/2013	15:49:27	1050
10/12/2013	15:50:27	1065.4
10/12/2013	15:51:25	1040.1
10/12/2013	15:52:26	1079.5
10/12/2013	15:53:26	1113.1

10/12/2013	15:54:26	1144
10/12/2013	15:55:26	1128.2
10/12/2013	15:56:27	1054
10/12/2013	15:57:27	993.8
10/12/2013	15:58:27	1039.7
10/12/2013	15:59:25	1073
10/12/2013	16:00:26	1061.5
10/12/2013	16:01:26	1101.2
10/12/2013	16:02:26	1085.7
10/12/2013	16:03:26	1125.9
10/12/2013	16:04:27	1169.1
10/12/2013	16:05:27	1190.6
10/12/2013	16:06:27	1218.4
10/12/2013	16:07:26	1252.7
10/12/2013	16:08:26	1293.9
Average	1811 sampl	1074.7
Test Run 1 End		

Test Run 2 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/12/2013	16:36:23	989.3
10/12/2013	16:37:21	1058.5
10/12/2013	16:38:22	1059.2
10/12/2013	16:39:22	1090.3
10/12/2013	16:40:22	1113.4
10/12/2013	16:41:23	1157.2
10/12/2013	16:42:23	1148.6
10/12/2013	16:43:23	1105.5
10/12/2013	16:44:21	1046.7
10/12/2013	16:45:22	1012.7
10/12/2013	16:46:22	968.8
10/12/2013	16:47:22	963.1
10/12/2013	16:48:22	949.2
10/12/2013	16:49:23	960.6
10/12/2013	16:50:23	959
10/12/2013	16:51:21	942.5
10/12/2013	16:52:22	962.3
10/12/2013	16:53:22	925.5
10/12/2013	16:54:22	960.7
10/12/2013	16:55:23	971.3
10/12/2013	16:56:23	990.3
10/12/2013	16:57:23	949.2
10/12/2013	16:58:21	891.5
10/12/2013	16:59:22	905.3
10/12/2013	17:00:22	914.1
10/12/2013	17:01:22	914.2
10/12/2013	17:02:23	926.1
10/12/2013	17:03:23	930.9
10/12/2013	17:04:23	895.7
10/12/2013	17:05:21	943.1
10/12/2013	17:06:22	943.9
10/12/2013	17:07:22	978.3
10/12/2013	17:08:22	940.6
10/12/2013	17:09:23	993.2
10/12/2013	17:10:23	996.5
10/12/2013	17:11:23	986.9
10/12/2013	17:12:21	952
10/12/2013	17:13:22	875.5
10/12/2013	17:14:22	916.5
10/12/2013	17:15:22	939.4
10/12/2013	17:16:23	930.8
10/12/2013	17:17:23	919.8
10/12/2013	17:18:23	938.6
10/12/2013	17:19:21	999.3
10/12/2013	17:20:22	986.2

10/12/2013	17:21:22	963
10/12/2013	17:22:22	910.9
10/12/2013	17:23:23	886.5
10/12/2013	17:24:23	873.2
10/12/2013	17:25:21	870.2
10/12/2013	17:26:21	876.3
10/12/2013	17:27:22	925.8
10/12/2013	17:28:22	911.6
10/12/2013	17:29:22	865.7
10/12/2013	17:30:22	850
10/12/2013	17:31:23	893.9
10/12/2013	17:32:23	913.1
10/12/2013	17:33:21	915.1
10/12/2013	17:34:21	918.1
10/12/2013	17:35:22	960.6
10/12/2013	17:36:22	942.2
Average	1824 sampl	957
Test Run 2 End		

Test Run 3 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/12/2013	18:00:49	1126.2
10/12/2013	18:01:49	1091.3
10/12/2013	18:02:49	1034.6
10/12/2013	18:03:49	996.3
10/12/2013	18:04:50	1063.4
10/12/2013	18:05:50	1027.2
10/12/2013	18:06:50	995.6
10/12/2013	18:07:48	1085.5
10/12/2013	18:08:49	1133.7
10/12/2013	18:09:49	1177.7
10/12/2013	18:10:49	1174.3
10/12/2013	18:11:50	1169.6
10/12/2013	18:12:50	1112.9
10/12/2013	18:13:50	1135.7
10/12/2013	18:14:50	1102.2
10/12/2013	18:15:49	1176.6
10/12/2013	18:16:49	1201.9
10/12/2013	18:17:49	1217
10/12/2013	18:18:49	1248
10/12/2013	18:19:50	1297.6
10/12/2013	18:20:50	1351.7
10/12/2013	18:21:50	1412.8
10/12/2013	18:22:49	1417.9
10/12/2013	18:23:49	1368.5
10/12/2013	18:24:49	1287.4
10/12/2013	18:25:49	1173.7
10/12/2013	18:26:50	1198.4
10/12/2013	18:27:50	1205.2
10/12/2013	18:28:50	1198.8
10/12/2013	18:29:50	1194.9
10/12/2013	18:30:49	1174.8
10/12/2013	18:31:49	1184.2
10/12/2013	18:32:49	1161.6
10/12/2013	18:33:50	1200.8
10/12/2013	18:34:50	1239.5
10/12/2013	18:35:50	1260.8
10/12/2013	18:36:50	1242.4
10/12/2013	18:37:49	1230.9
10/12/2013	18:38:49	1200.6
10/12/2013	18:39:49	1159
10/12/2013	18:40:49	1156.6
10/12/2013	18:41:50	1183.6
10/12/2013	18:42:50	1112.7
10/12/2013	18:43:50	1146.3
10/12/2013	18:44:48	1178.5

10/12/2013	18:45:49	1184.8
10/12/2013	18:46:49	1190.2
10/12/2013	18:47:49	1236.3
10/12/2013	18:48:50	1229.3
10/12/2013	18:49:50	1299.9
10/12/2013	18:50:50	1314.9
10/12/2013	18:51:48	1303.2
10/12/2013	18:52:49	1305.8
10/12/2013	18:53:49	1308.6
10/12/2013	18:54:49	1314
10/12/2013	18:55:50	1277
10/12/2013	18:56:50	1203.3
10/12/2013	18:57:50	1144.9
10/12/2013	18:58:48	1242.6
10/12/2013	18:59:49	1242.4
Average	1796 sampl	1200
Test Run 3 End		

Test Run 9 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/13/2013	9:22:03	71.7
10/13/2013	9:23:03	73.9
10/13/2013	9:24:04	76.1
10/13/2013	9:25:04	78.7
10/13/2013	9:26:04	80.4
10/13/2013	9:27:04	82.1
10/13/2013	9:28:05	83.8
10/13/2013	9:29:03	85.1
10/13/2013	9:30:03	85.8
10/13/2013	9:31:03	86.3
10/13/2013	9:32:04	86.9
10/13/2013	9:33:04	87.8
10/13/2013	9:34:04	88
10/13/2013	9:35:05	89.5
10/13/2013	9:36:03	87.7
10/13/2013	9:37:03	87
10/13/2013	9:38:03	86.1
10/13/2013	9:39:04	85.2
10/13/2013	9:40:04	84.8
10/13/2013	9:41:04	85.1
10/13/2013	9:42:04	85.9
10/13/2013	9:43:05	87.4
10/13/2013	9:44:03	88.9
10/13/2013	9:45:03	89.8
10/13/2013	9:46:03	90.7
10/13/2013	9:47:04	90.6
10/13/2013	9:48:04	90.8
10/13/2013	9:49:04	92.2
10/13/2013	9:50:05	93.7
10/13/2013	9:51:03	93.8
10/13/2013	9:52:03	94.6
10/13/2013	9:53:03	95.6
10/13/2013	9:54:04	96
10/13/2013	9:55:04	96.3
10/13/2013	9:56:04	97
10/13/2013	9:57:04	97.5
10/13/2013	9:58:05	98
10/13/2013	9:59:03	98.3
10/13/2013	10:00:03	99.7
10/13/2013	10:01:03	100.8
10/13/2013	10:02:04	101.7
10/13/2013	10:03:04	102.4
10/13/2013	10:04:04	103
10/13/2013	10:05:05	102.3
10/13/2013	10:06:03	101.1

10/13/2013	10:07:03	100
10/13/2013	10:08:03	98.6
10/13/2013	10:09:04	98.2
10/13/2013	10:10:04	98.4
10/13/2013	10:11:04	98.1
10/13/2013	10:12:04	97.6
10/13/2013	10:13:05	96.8
10/13/2013	10:14:03	95.4
10/13/2013	10:15:03	92.2
10/13/2013	10:16:03	91.5
10/13/2013	10:17:04	93.1
10/13/2013	10:18:04	94.6
10/13/2013	10:19:04	97.1
10/13/2013	10:20:04	97.7
10/13/2013	10:21:05	97.5
Average	1797 sampl	91.8
Test Run 9 End		

Test Run 10 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/13/2013	11:04:49	77.08
10/13/2013	11:05:50	78.11
10/13/2013	11:06:50	78.19
10/13/2013	11:07:50	77.63
10/13/2013	11:08:50	77.56
10/13/2013	11:09:51	77.71
10/13/2013	11:10:51	77.97
10/13/2013	11:11:49	77.89
10/13/2013	11:12:49	78.97
10/13/2013	11:13:50	79.14
10/13/2013	11:14:50	77.97
10/13/2013	11:15:51	76.86
10/13/2013	11:16:49	76.19
10/13/2013	11:17:49	76.58
10/13/2013	11:18:50	76.82
10/13/2013	11:19:50	77.53
10/13/2013	11:20:50	78.27
10/13/2013	11:21:50	79.01
10/13/2013	11:22:51	79.04
10/13/2013	11:23:51	78.95
10/13/2013	11:24:49	78.85
10/13/2013	11:25:50	78.45
10/13/2013	11:26:50	78.1
10/13/2013	11:27:50	78.55
10/13/2013	11:28:50	78.58
10/13/2013	11:29:51	78.39
10/13/2013	11:30:51	78.37
10/13/2013	11:31:49	79.42
10/13/2013	11:32:49	81.98
10/13/2013	11:33:50	84.04
10/13/2013	11:34:50	83.84
10/13/2013	11:35:50	83.55
10/13/2013	11:36:50	83.19
10/13/2013	11:37:51	82.62
10/13/2013	11:38:51	82.45
10/13/2013	11:39:49	82.09
10/13/2013	11:40:49	81.91
10/13/2013	11:41:50	81.54
10/13/2013	11:42:50	81.56
10/13/2013	11:43:50	82.21
10/13/2013	11:44:51	82.55
10/13/2013	11:45:51	82.6
10/13/2013	11:46:49	82.99
10/13/2013	11:47:49	83.33
10/13/2013	11:48:50	83.22

10/13/2013	11:49:50	83.17
10/13/2013	11:50:50	84.26
10/13/2013	11:51:50	86.33
10/13/2013	11:52:51	87.37
10/13/2013	11:53:51	85.99
10/13/2013	11:54:49	85.29
10/13/2013	11:55:49	85.22
10/13/2013	11:56:50	86.39
10/13/2013	11:57:50	86.43
10/13/2013	11:58:50	85.81
10/13/2013	11:59:50	86.1
10/13/2013	12:00:51	86.23
10/13/2013	12:01:51	84.93
10/13/2013	12:02:49	82.97
10/13/2013	12:03:50	82.23
10/13/2013	12:04:50	84.21
Average	1825 sampl	81.24
Test Run 10 End		

Test Run 11 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/13/2013	12:31:14	107.99
10/13/2013	12:32:14	108.6
10/13/2013	12:33:15	109.57
10/13/2013	12:34:15	112.47
10/13/2013	12:35:15	115.91

Pause

10/13/2013	12:36:15	115.09
10/13/2013	12:37:14	112.39
10/13/2013	12:38:14	111.26
10/13/2013	12:39:14	112.42
10/13/2013	12:40:14	113.56
10/13/2013	12:41:15	114.42
10/13/2013	12:42:15	113.98
10/13/2013	12:43:15	112.12
10/13/2013	12:44:15	110.5
10/13/2013	12:45:14	109.3
10/13/2013	12:46:14	108.63
10/13/2013	12:47:14	110.13
10/13/2013	12:48:14	112.11
10/13/2013	12:49:15	112.2
10/13/2013	12:50:15	111.62
10/13/2013	12:51:15	111.91

End Pause

10/13/2013	12:52:15	111.76
10/13/2013	12:53:14	110.85
10/13/2013	12:54:14	109.25
10/13/2013	12:55:14	107.32
10/13/2013	12:56:15	105.6
10/13/2013	12:57:15	105.51
10/13/2013	12:58:15	105.13
10/13/2013	12:59:15	103.83
10/13/2013	13:00:15	101.32
10/13/2013	13:01:14	100.13
10/13/2013	13:02:14	99.2
10/13/2013	13:03:14	99
10/13/2013	13:04:14	99.6
10/13/2013	13:05:15	100.72
10/13/2013	13:06:15	100.21
10/13/2013	13:07:15	99.39
10/13/2013	13:08:15	99
10/13/2013	13:09:14	98.91
10/13/2013	13:10:14	98.55
10/13/2013	13:11:14	99.06
10/13/2013	13:12:15	99.18
10/13/2013	13:13:15	99.24

10/13/2013	13:14:15	100.67
10/13/2013	13:15:15	101.29
10/13/2013	13:16:14	100.86
10/13/2013	13:17:14	100.04
10/13/2013	13:18:14	99.03
10/13/2013	13:19:14	99.26
10/13/2013	13:20:15	100.68
10/13/2013	13:21:15	100.36
10/13/2013	13:22:15	99.65
10/13/2013	13:23:15	98.28
10/13/2013	13:24:14	96.42
10/13/2013	13:25:14	96.23
10/13/2013	13:26:14	96.14
10/13/2013	13:27:14	94.87
10/13/2013	13:28:15	95.34
10/13/2013	13:29:15	94.94
10/13/2013	13:30:15	94.01
10/13/2013	13:31:14	92.64
10/13/2013	13:32:14	91.56
10/13/2013	13:33:14	89.78
10/13/2013	13:34:14	87.93
10/13/2013	13:35:15	86.12
10/13/2013	13:36:15	85.57
10/13/2013	13:37:15	85.8
10/13/2013	13:38:14	85.88
10/13/2013	13:39:14	85.76
10/13/2013	13:40:14	85.56
10/13/2013	13:41:14	85.49
10/13/2013	13:42:15	84.8
10/13/2013	13:43:15	84.44
10/13/2013	13:44:15	83.05
10/13/2013	13:45:15	81.96
10/13/2013	13:46:14	81
10/13/2013	13:47:14	81.22
Average	1833 sampl	97.19
Test Run 11 End		

Enviva - Wiggins
Run 1

Date: 10-Oct
Run Time: 0917-1017
(CEM Run Time Eastern)

Parameter	Symbol	Green Hammermill
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, \text{zero}}$	0.0
Low-Level Gas	$C_{v, \text{low}}$	27.99
Mid-Level Gas	$C_{v, \text{mid}}$	50
High-Level Gas	$C_{v, \text{high}}$	86.13
Calibration Span	CS	100

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, \text{zero}}$	0.0
Low-Level Gas	$C_{Dir, \text{low}}$	28.3
Mid-Level Gas	$C_{Dir, \text{mid}}$	50.8
High-Level Gas	$C_{Dir, \text{high}}$	86.5

0900

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	1.1
Mid-Level Gas	ACE_{mid}	1.6
High-Level Gas	ACE_{high}	0.4
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, \text{zero (pre)}}$	0
Final Zero	$C_{s, \text{zero (post)}}$	0.11
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, \text{up (pre)}}$	50.8
Final Upscale	$C_{v, \text{up (post)}}$	50.65

System Bias - Results (Percent)		
Zero (pre)	$SB_{i \text{ (zero)}}$	0.0
Zero (post)	$SB_{\text{final (zero)}}$	0.1
Upscale (pre)	$SB_{i \text{ (upscale)}}$	0.0
Upscale (post)	$SB_{\text{final (upscale)}}$	-0.1
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.1
Upscale	D_{upscale}	-0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	30.8
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	30.8

Enviva - Wiggins
Run 2

Date: 10-Oct
Run Time: 1036-1136

Parameter	Symbol	Green Hammermill
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.3
Mid-Level Gas	$C_{Dir, mid}$	50.8
High-Level Gas	$C_{Dir, high}$	86.5

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	1.1
Mid-Level Gas	ACE_{mid}	1.6
High-Level Gas	ACE_{high}	0.4
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.11
Final Zero	$C_{s, zero (post)}$	0.05
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.65
Final Upscale	$C_{v, up (post)}$	50.1

System Bias - Results (Percent)		
Zero (pre)	$SB_{i (zero)}$	0.1
Zero (post)	$SB_{final (zero)}$	0.1
Upscale (pre)	$SB_{i (upscale)}$	-0.1
Upscale (post)	$SB_{final (upscale)}$	-0.7
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	-0.1
Upscale	$D_{upscale}$	-0.5
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	32.23
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	32.2

Enviva - Wiggins
Run 3

Date: 10-Oct
Run Time: 1150-1250

Parameter	Symbol	Green Hammermill
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.3
Mid-Level Gas	$C_{Dir, mid}$	50.8
High-Level Gas	$C_{Dir, high}$	86.5

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	1.1
Mid-Level Gas	ACE_{mid}	1.6
High-Level Gas	ACE_{high}	0.4
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.05
Final Zero	$C_{s, zero (post)}$	0.1
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.1
Final Upscale	$C_{v, up (post)}$	49.8

System Bias - Results (Percent)		
Zero (pre)	$SB_{i (zero)}$	0.1
Zero (post)	$SB_{final (zero)}$	0.1
Upscale (pre)	$SB_{i (upscale)}$	-0.7
Upscale (post)	$SB_{final (upscale)}$	-1.0
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.1
Upscale	$D_{upscale}$	-0.3
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	26.38
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	26.4

Enviva - Wiggins
Run #7

Date: 11-Oct
Run Time: 1343-1443

Parameter	Symbol	Pellet Cooler 2
		THC
		(as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, \text{zero}}$	0.0
Low-Level Gas	$C_{v, \text{low}}$	27.99
Mid-Level Gas	$C_{v, \text{mid}}$	50
High-Level Gas	$C_{v, \text{high}}$	86.13
Calibration Span	CS	100

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, \text{zero}}$	0.0
Low-Level Gas	$C_{Dir, \text{low}}$	28.1
Mid-Level Gas	$C_{Dir, \text{mid}}$	51.1
High-Level Gas	$C_{Dir, \text{high}}$	86.15

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	2.2
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, \text{zero (pre)}}$	0.04
Final Zero	$C_{s, \text{zero (post)}}$	0.35
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, \text{up (pre)}}$	50.14
Final Upscale	$C_{v, \text{up (post)}}$	50.2

System Bias - Results (Percent)		
Zero (pre)	$SB_i (\text{zero})$	0.0
Zero (post)	$SB_{\text{final}} (\text{zero})$	0.3
Upscale (pre)	$SB_i (\text{upscale})$	-1.0
Upscale (post)	$SB_{\text{final}} (\text{upscale})$	-0.9
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.3
Upscale	D_{upscale}	0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	23.80
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	23.8

Enviva - Wiggins
Run #8

Date: 11-Oct
Run Time: 1508-1608

Parameter	Symbol	Pellet Cooler 2
		THC
		(as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	2.2
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.35
Final Zero	$C_{s, zero (post)}$	0.18
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.2
Final Upscale	$C_{v, up (post)}$	50.1

System Bias - Results (Percent)		
Zero (pre)	$SB_{i (zero)}$	0.3
Zero (post)	$SB_{final (zero)}$	0.1
Upscale (pre)	$SB_{i (upscale)}$	-0.9
Upscale (post)	$SB_{final (upscale)}$	-1.0
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	-0.2
Upscale	$D_{upscale}$	-0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	21.29
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	21.3

Enviva - Wiggins
Run #9

Date: 11-Oct
Run Time: 29-1729

Parameter	Symbol	Pellet Cooler 2
		THC
		(as C_3H_8)
		ppm _w

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	2.2
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.18
Final Zero	$C_{s, zero (post)}$	0.2
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.1
Final Upscale	$C_{v, up (post)}$	49.8

System Bias - Results (Percent)		
Zero (pre)	$SB_{i (zero)}$	0.1
Zero (post)	$SB_{final (zero)}$	0.2
Upscale (pre)	$SB_{i (upscale)}$	-1.0
Upscale (post)	$SB_{final (upscale)}$	-1.3
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.0
Upscale	$D_{upscale}$	-0.3
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	24.84
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	24.8

Enviva - Wiggins
Run #4

Date: 10-Oct
Run Time: 1738-1838

Parameter	Symbol	Dryer 1
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, \text{zero}}$	0.0
Low-Level Gas	$C_{v, \text{low}}$	27.99
Mid-Level Gas	$C_{v, \text{mid}}$	50
High-Level Gas	$C_{v, \text{high}}$	86.13
Calibration Span	CS	100

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, \text{zero}}$	0.0
Low-Level Gas	$C_{Dir, \text{low}}$	28.3
Mid-Level Gas	$C_{Dir, \text{mid}}$	50.8
High-Level Gas	$C_{Dir, \text{high}}$	86.5

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	1.1
Mid-Level Gas	ACE_{mid}	1.6
High-Level Gas	ACE_{high}	0.4
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, \text{zero (pre)}}$	0
Final Zero	$C_{s, \text{zero (post)}}$	0.85
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, \text{up (pre)}}$	50.8
Final Upscale	$C_{v, \text{up (post)}}$	50.9

System Bias - Results (Percent)		
Zero (pre)	$SB_{i(\text{zero})}$	0.0
Zero (post)	$SB_{final(\text{zero})}$	0.9
Upscale (pre)	$SB_{i(\text{upscale})}$	0.0
Upscale (post)	$SB_{final(\text{upscale})}$	0.1
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.9
Upscale	D_{upscale}	0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	66.70
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	66.7

Enviva - Wiggins
Run #5

Date: 11-Oct
Run Time: 1000-1100

Parameter	Symbol	Dryer 1
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, \text{zero}}$	0.0
Low-Level Gas	$C_{v, \text{low}}$	28.0
Mid-Level Gas	$C_{v, \text{mid}}$	50.0
High-Level Gas	$C_{v, \text{high}}$	86.1
Calibration Span	CS	100.0

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, \text{zero}}$	0.0
Low-Level Gas	$C_{Dir, \text{low}}$	28.1
Mid-Level Gas	$C_{Dir, \text{mid}}$	51.1
High-Level Gas	$C_{Dir, \text{high}}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	2.2
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, \text{zero (pre)}}$	0.85
Final Zero	$C_{s, \text{zero (post)}}$	0.15
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, \text{up (pre)}}$	50.9
Final Upscale	$C_{v, \text{up (post)}}$	50.5

System Bias - Results (Percent)		
Zero (pre)	$SB_{i \text{ (zero)}}$	0.8
Zero (post)	$SB_{\text{final (zero)}}$	0.1
Upscale (pre)	$SB_{i \text{ (upscale)}}$	-0.2
Upscale (post)	$SB_{\text{final (upscale)}}$	-0.6
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	-0.7
Upscale	D_{upscale}	-0.4
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	61.92
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	61.9

Enviva - Wiggins
Run #6

Date: 11-Oct
Run Time: 1137-1237

Parameter	Symbol	Dryer 1
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	2.2
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.15
Final Zero	$C_{s, zero (post)}$	0.1
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.5
Final Upscale	$C_{v, up (post)}$	50.14

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.1
Zero (post)	$SB_{final} (zero)$	0.1
Upscale (pre)	$SB_i (upscale)$	-0.6
Upscale (post)	$SB_{final} (upscale)$	-1.0
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	-0.1
Upscale	$D_{upscale}$	-0.4
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	57.17
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	57.2

Parameter	Symbol	Hammermill 2
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Calibration Standards

Zero Gas	$C_{v, zero}$	0.0
Low-Level Gas	$C_{v, low}$	27.99
Mid-Level Gas	$C_{v, mid}$	50
High-Level Gas	$C_{v, high}$	86.13
Calibration Span	CS	100

Analyzer Calibration Error - Instrument Response

Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.15

Analyzer Calibration Error - Results (Percent of Span)

Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	2.2
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response

Initial Zero	$C_{s, zero (pre)}$	0.2
Final Zero	$C_{s, zero (post)}$	0.08
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	49.8
Final Upscale	$C_{v, up (post)}$	50

System Bias - Results (Percent)

Zero (pre)	$SB_{i (zero)}$	0.2
Zero (post)	$SB_{final (zero)}$	0.0
Upscale (pre)	$SB_{i (upscale)}$	-1.3
Upscale (post)	$SB_{final (upscale)}$	-1.1
Specification	SB_{spec}	NA

System Drift - Results (Percent)

Zero	D_{zero}	-0.1
Upscale	$D_{upscale}$	0.2
Specification	D_{spec}	±3

Response Test - Results (seconds)

Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction

Raw Average	C_{ave}	25.19
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	25.2

Enviva - Wiggins
Run 11

Date: 11-Oct
Run Time: 1935-2035

Parameter	Symbol	Hammermill 2
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response

Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)

Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	2.2
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response

Initial Zero	$C_{s, zero (pre)}$	0.08
Final Zero	$C_{s, zero (post)}$	0.21
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50
Final Upscale	$C_{v, up (post)}$	49.85

System Bias - Results (Percent)

Zero (pre)	$SB_i (zero)$	0.0
Zero (post)	$SB_{final} (zero)$	0.2
Upscale (pre)	$SB_i (upscale)$	-1.1
Upscale (post)	$SB_{final} (upscale)$	-1.3
Specification	SB_{spec}	NA

System Drift - Results (Percent)

Zero	D_{zero}	0.1
Upscale	$D_{upscale}$	-0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)

Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction

Raw Average	C_{ave}	29.72
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	29.7

Enviva - Wiggins
Run 12

Date: 10/11/2013
Run Time: 2048-2148

Parameter	Symbol	Hammermill 2
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response

Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)

Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	2.2
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response

Initial Zero	$C_{s, zero (pre)}$	0.21
Final Zero	$C_{s, zero (post)}$	0.23
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	49.85
Final Upscale	$C_{v, up (post)}$	49.9

System Bias - Results (Percent)

Zero (pre)	$SB_i (zero)$	0.2
Zero (post)	$SB_{final} (zero)$	0.2
Upscale (pre)	$SB_i (upscale)$	-1.3
Upscale (post)	$SB_{final} (upscale)$	-1.2
Specification	SB_{spec}	NA

System Drift - Results (Percent)

Zero	D_{zero}	0.0
Upscale	$D_{upscale}$	0.0
Specification	D_{spec}	±3

Response Test - Results (seconds)

Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction

Raw Average	C_{ave}	24.43
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	24.4

Enviva - Wiggins
Run 13

Date: 12-Oct
Run Time: 0858-0958

Parameter	Symbol	Pellet Cooler 1
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, \text{zero}}$	0.0
Low-Level Gas	$C_{v, \text{low}}$	27.99
Mid-Level Gas	$C_{v, \text{mid}}$	50
High-Level Gas	$C_{v, \text{high}}$	86.13
Calibration Span	CS	100

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, \text{zero}}$	0.1
Low-Level Gas	$C_{Dir, \text{low}}$	28.1
Mid-Level Gas	$C_{Dir, \text{mid}}$	50.4
High-Level Gas	$C_{Dir, \text{high}}$	86.15

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.1
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	0.8
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, \text{zero (pre)}}$	0.1
Final Zero	$C_{s, \text{zero (post)}}$	0.35
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, \text{up (pre)}}$	50.4
Final Upscale	$C_{v, \text{up (post)}}$	50.3

System Bias - Results (Percent)		
Zero (pre)	$SB_i (\text{zero})$	0.0
Zero (post)	$SB_{\text{final}} (\text{zero})$	0.3
Upscale (pre)	$SB_i (\text{upscale})$	0.0
Upscale (post)	$SB_{\text{final}} (\text{upscale})$	-0.1
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.3
Upscale	D_{upscale}	-0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	39.05
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	39.1

Enviva - Wiggins
Run 14

Date: 12-Oct
Run Time: 1022-1122

Parameter	Symbol	Pellet Cooler 1
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.1
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	50.4
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.1
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	0.8
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.35
Final Zero	$C_{s, zero (post)}$	0.24
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.3
Final Upscale	$C_{v, up (post)}$	50.25

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.3
Zero (post)	$SB_{final} (zero)$	
Upscale (pre)	$SB_i (upscale)$	-0.1
Upscale (post)	$SB_{final} (upscale)$	
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	-0.1
Upscale	$D_{upscale}$	0.0
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	33.29
Bias Average - Zero	C_0	NA
Bias Average - Upscale	C_M	NA
Corrected Run Average	C_{Gas}	33.3

Enviva - Wiggins
Run 15

Date: 12-Oct
Run Time: 1141-124

Parameter	Symbol	Pellet Cooler 1
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.1
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	50.4
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.1
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	0.8
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.24
Final Zero	$C_{s, zero (post)}$	0.33
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.25
Final Upscale	$C_{v, up (post)}$	50.1

System Bias - Results (Percent)		
Zero (pre)	$SB_{i (zero)}$	0.2
Zero (post)	$SB_{final (zero)}$	0.3
Upscale (pre)	$SB_{i (upscale)}$	-0.1
Upscale (post)	$SB_{final (upscale)}$	-0.3
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.1
Upscale	$D_{upscale}$	-0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	35.65
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	35.7

Enviva - Wiggins
Run 16

Date: 12-Oct
Run Time: 1509-1609

Parameter	Symbol	Aspirator
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, \text{zero}}$	0.0
Low-Level Gas	$C_{v, \text{low}}$	258.1
Mid-Level Gas	$C_{v, \text{mid}}$	507.1
High-Level Gas	$C_{v, \text{high}}$	836.9
Calibration Span	CS	1000

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, \text{zero}}$	1.1
Low-Level Gas	$C_{Dir, \text{low}}$	260
Mid-Level Gas	$C_{Dir, \text{mid}}$	507
High-Level Gas	$C_{Dir, \text{high}}$	838.3

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.1
Low-Level Gas	ACE_{low}	0.7
Mid-Level Gas	ACE_{mid}	0.0
High-Level Gas	ACE_{high}	0.1
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, \text{zero (pre)}}$	1.1
Final Zero	$C_{s, \text{zero (post)}}$	2.4
Upscale Gas Standard	C_{MA}	836.9
Initial Upscale	$C_{v, \text{up (pre)}}$	838.3
Final Upscale	$C_{v, \text{up (post)}}$	837

System Bias - Results (Percent)		
Zero (pre)	$SB_i (\text{zero})$	0.0
Zero (post)	$SB_{\text{final}} (\text{zero})$	0.1
Upscale (pre)	$SB_i (\text{upscale})$	0.0
Upscale (post)	$SB_{\text{final}} (\text{upscale})$	-0.1
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.1
Upscale	D_{upscale}	-0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	1074.70
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	1074.7

Enviva - Wiggins
Run 17

Date: 12-Oct
Run Time: 1636-1736

Parameter	Symbol	Aspirator
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, \text{zero}}$	0.0
Low-Level Gas	$C_{v, \text{low}}$	258.1
Mid-Level Gas	$C_{v, \text{mid}}$	507.1
High-Level Gas	$C_{v, \text{high}}$	836.9
Calibration Span	CS	1000.0

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, \text{zero}}$	1.1
Low-Level Gas	$C_{Dir, \text{low}}$	260.0
Mid-Level Gas	$C_{Dir, \text{mid}}$	507.0
High-Level Gas	$C_{Dir, \text{high}}$	838.3

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.1
Low-Level Gas	ACE_{low}	0.7
Mid-Level Gas	ACE_{mid}	0.0
High-Level Gas	ACE_{high}	0.1
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, \text{zero (pre)}}$	2.40
Final Zero	$C_{s, \text{zero (post)}}$	1.4
Upscale Gas Standard	C_{MA}	836.9
Initial Upscale	$C_{v, \text{up (pre)}}$	837
Final Upscale	$C_{v, \text{up (post)}}$	837.5

System Bias - Results (Percent)		
Zero (pre)	$SB_i (\text{zero})$	0.1
Zero (post)	$SB_{final} (\text{zero})$	0.0
Upscale (pre)	$SB_i (\text{upscale})$	-0.1
Upscale (post)	$SB_{final} (\text{upscale})$	-0.1
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	-0.1
Upscale	D_{upscale}	0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	957.00
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	957.0

Enviva - Wiggins
Run 18

Date: 12-Oct
Run Time: 1800-1900

Parameter	Symbol	Aspirator
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response

Zero Gas	$C_{Dir, zero}$	1.1
Low-Level Gas	$C_{Dir, low}$	260.0
Mid-Level Gas	$C_{Dir, mid}$	507.0
High-Level Gas	$C_{Dir, high}$	838.3

Analyzer Calibration Error - Results (Percent of Span)

Zero Gas	ACE_{zero}	0.1
Low-Level Gas	ACE_{low}	0.7
Mid-Level Gas	ACE_{mid}	0.0
High-Level Gas	ACE_{high}	0.1
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response

Initial Zero	$C_{s, zero (pre)}$	1.40
Final Zero	$C_{s, zero (post)}$	2
Upscale Gas Standard	C_{MA}	836.9
Initial Upscale	$C_{v, up (pre)}$	837.5
Final Upscale	$C_{v, up (post)}$	835

System Bias - Results (Percent)

Zero (pre)	$SB_i (zero)$	0.0
Zero (post)	$SB_{final (zero)}$	0.1
Upscale (pre)	$SB_i (upscale)$	-0.1
Upscale (post)	$SB_{final (upscale)}$	-0.3
Specification	SB_{spec}	NA

System Drift - Results (Percent)

Zero	D_{zero}	0.1
Upscale	$D_{upscale}$	-0.3
Specification	D_{spec}	±3

Response Test - Results (seconds)

Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction

Raw Average	C_{ave}	1200.00
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	1200.0

Parameter	Symbol	Dryer 2	
		THC (as C ₃ H ₈)	
		ppm _w	

Analyzer Calibration Error - Calibration Standards			
Zero Gas	$C_{v, \text{zero}}$	0.0	0.0
Low-Level Gas	$C_{v, \text{low}}$	258.1	27.99
Mid-Level Gas	$C_{v, \text{mid}}$	507.1	50
High-Level Gas	$C_{v, \text{high}}$	836.9	86.13
Calibration Span	CS	1000	100

Analyzer Calibration Error - Instrument Response			
Zero Gas	$C_{Dir, \text{zero}}$	1.0	1.0
Low-Level Gas	$C_{Dir, \text{low}}$	259	28.4
Mid-Level Gas	$C_{Dir, \text{mid}}$	506.8	50.34
High-Level Gas	$C_{Dir, \text{high}}$	837.3	86.24

Analyzer Calibration Error - Results (Percent of Span)			
Zero Gas	ACE_{zero}	0.1	1.0
Low-Level Gas	ACE_{low}	0.3	1.5
Mid-Level Gas	ACE_{mid}	-0.1	0.7
High-Level Gas	ACE_{high}	0.0	0.1
Specification	ACE_{spec}	±5	±8

System Calibrations - Instrument Response			
Initial Zero	$C_{s, \text{zero (pre)}}$	1.0	1.0
Final Zero	$C_{s, \text{zero (post)}}$	1.6	1.6
Upscale Gas Standard	C_{MA}	507.1	50.0
Initial Upscale	$C_{v, \text{up (pre)}}$	506.8	50.34
Final Upscale	$C_{v, \text{up (post)}}$	504	50.6

System Bias - Results (Percent)			
Zero (pre)	$SB_i (\text{zero})$	0.0	0.0
Zero (post)	$SB_{\text{final (zero)}}$	0.1	0.6
Upscale (pre)	$SB_i (\text{upscale})$	0.0	0.0
Upscale (post)	$SB_{\text{final (upscale)}}$	-0.3	0.3
Specification	SB_{spec}	NA	NA

System Drift - Results (Percent)			
Zero	D_{zero}	0.1	0.6
Upscale	D_{upscale}	-0.3	0.3
Specification	D_{spec}	±3	±6

Response Test - Results (seconds)			
Upscale Test		NA	NA
Zero Test		NA	NA
Response Time		28	28

Calibration Correction			
Raw Average	C_{ave}	91.8	91.8
Bias Average - Zero	C_0	N/A	N/A
Bias Average - Upscale	C_M	N/A	N/A
Corrected Run Average	C_{Gas}	91.8	91.8

Enviva - Wiggins
Run 20

Date: 13-Oct
Run Time: 1104-1204

Parameter	Symbol	Dryer 2	
		THC (as C ₃ H ₈)	
		ppm _w	

Analyzer Calibration Error - Calibration Standards

Zero Gas	$C_{v, \text{zero}}$	0.0	0.0
Low-Level Gas	$C_{v, \text{low}}$	258.1	28.0
Mid-Level Gas	$C_{v, \text{mid}}$	507.1	50.0
High-Level Gas	$C_{v, \text{high}}$	836.9	86.1
Calibration Span	CS	1000.0	100.0

Analyzer Calibration Error - Instrument Response

Zero Gas	$C_{Dir, \text{zero}}$	1.0	1.0
Low-Level Gas	$C_{Dir, \text{low}}$	259.0	28.4
Mid-Level Gas	$C_{Dir, \text{mid}}$	506.8	50.3
High-Level Gas	$C_{Dir, \text{high}}$	837.3	86.2

Analyzer Calibration Error - Results (Percent of Span)

Zero Gas	ACE_{zero}	0.1	1.0
Low-Level Gas	ACE_{low}	0.3	1.5
Mid-Level Gas	ACE_{mid}	-0.1	0.7
High-Level Gas	ACE_{high}	0.0	0.1
Specification	ACE_{spec}	±5	±8

System Calibrations - Instrument Response

Initial Zero	$C_{s, \text{zero (pre)}}$	1.60	1.60
Final Zero	$C_{s, \text{zero (post)}}$	0.42	0.42
Upscale Gas Standard	C_{MA}	507.1	50.0
Initial Upscale	$C_{v, \text{up (pre)}}$	504	50.6
Final Upscale	$C_{v, \text{up (post)}}$	503	50.4

System Bias - Results (Percent)

Zero (pre)	$SB_{i \text{ (zero)}}$	0.1	0.6
Zero (post)	$SB_{\text{final (zero)}}$	-0.1	-0.6
Upscale (pre)	$SB_{i \text{ (upscale)}}$	-0.3	0.3
Upscale (post)	$SB_{\text{final (upscale)}}$	-0.4	0.1
Specification	SB_{spec}	NA	NA

System Drift - Results (Percent)

Zero	D_{zero}	-0.1	-1.2
Upscale	D_{upscale}	-0.1	-0.2
Specification	D_{spec}	±3	±3

Response Test - Results (seconds)

Upscale Test		NA	NA
Zero Test		NA	NA
Response Time		28	28

Calibration Correction

Raw Average	C_{ave}	81.2	81.2
Bias Average - Zero	C_0	N/A	N/A
Bias Average - Upscale	C_M	N/A	N/A
Corrected Run Average	C_{Gas}	81.2	81.2

Enviva - Wiggins
Run 21

Date: 13-Oct
Run Time: 1231-1347
Paused (1236-1252)

Parameter	Symbol	Dryer 2	
		THC (as C ₃ H ₈)	
		ppm _w	

Analyzer Calibration Error - Instrument Response			
Zero Gas	$C_{Dir, zero}$	1.0	1.00
Low-Level Gas	$C_{Dir, low}$	259.0	28.40
Mid-Level Gas	$C_{Dir, mid}$	506.8	50.34
High-Level Gas	$C_{Dir, high}$	837.3	86.24

Analyzer Calibration Error - Results (Percent of Span)			
Zero Gas	ACE_{zero}	0.1	1.0
Low-Level Gas	ACE_{low}	0.3	1.5
Mid-Level Gas	ACE_{mid}	-0.1	0.7
High-Level Gas	ACE_{high}	0.0	0.1
Specification	ACE_{spec}	±5	±8

System Calibrations - Instrument Response			
Initial Zero	$C_{s, zero (pre)}$	0.42	0.42
Final Zero	$C_{s, zero (post)}$	0.3	0.3
Upscale Gas Standard	C_{MA}	507.1	50.0
Initial Upscale	$C_{v, up (pre)}$	503	50.4
Final Upscale	$C_{v, up (post)}$	503.5	50.2

System Bias - Results (Percent)			
Zero (pre)	$SB_i (zero)$	-0.1	-0.6
Zero (post)	$SB_{final} (zero)$	-0.1	-0.7
Upscale (pre)	$SB_i (upscale)$	-0.4	0.1
Upscale (post)	$SB_{final} (upscale)$	-0.3	-0.1
Specification	SB_{spec}	NA	NA

System Drift - Results (Percent)			
Zero	D_{zero}	0.0	-0.1
Upscale	$D_{upscale}$	0.1	-0.2
Specification	D_{spec}	±3	±6

Response Test - Results (seconds)			
Upscale Test		NA	NA
Zero Test		NA	NA
Response Time		28	31

Calibration Correction			
Raw Average	C_{ave}	97.2	97.2
Bias Average - Zero	C_0	N/A	N/A
Bias Average - Upscale	C_M	N/A	N/A
Corrected Run Average	C_{Gas}	97.2	97.2

APPENDIX C

Method 320 Data

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	V0.62 13.10.18.12.58

Compound	Sample ID / Concentration (ppmv wet)					
	Data Runs					
	GMH Run 1	GMH Run 2	GMH Run 3	Dryer 1 Run 1	Dryer 1 Run 2	Dryer 1 Run 3
Acrolein	1.13 J	1.20 J	1.15 J	1.79 J	1.72 ND	1.72 ND
Formaldehyde	0.742	0.629	0.561	3.32	1.60	1.78
Methanol	0.508	0.460	0.376	2.52	1.70	1.59
Phenol	0.88 ND	0.88 ND	0.88 ND	2.04 ND	2.04 ND	2.04 ND
Propionaldehyde	0.234 ND	0.234 ND	0.251 J	0.644 J	0.714 J	0.505 J
acetaldehyde	0.756 J	0.721 J	0.723 J	1.27 ND	1.27 ND	1.27 ND
	Data Runs					
	Pellet Cooler 2 Run 1	Pellet Cooler 2 Run 2	Pellet Cooler 2 Run 3	Hammermill 2 Run 1	Hammermill 2 Run 2	Hammermill 2 Run 3
Acrolein	1.29 J	1.21 J	1.33 J	0.980 J	0.975 J	0.965 ND
Formaldehyde	1.07	0.663	1.84	1.04	1.14	1.11
Methanol	0.797	0.680 J	0.844	0.189 J	0.211 J	0.204 J
Phenol	1.08 ND	1.08 ND	1.08 ND	1.08 ND	1.08 ND	1.08 ND
Propionaldehyde	0.246 J	0.246 ND	0.359 J	0.233 J	0.243 J	0.263 J
acetaldehyde	0.864 J	0.825 J	0.786 J	0.715 J	0.710 J	0.707 ND
	Data Runs					
	Pellet Cooler 1 Run 1	Pellet Cooler 1 Run 2	Pellet Cooler 1 Run 3	Aspirator Run 1	Aspirator Run 2	Aspirator Run 3
Acrolein	0.976 J	1.02 J	1.35 J	3.16	3.12	2.25 J
Formaldehyde	1.44	1.25	1.26	1.05 ND	1.58 J	1.06 J
Methanol	0.537	0.327	0.351	8.30	8.90	8.16
Phenol	1.00 J	0.98 ND	0.98 ND	2.73 ND	2.73 ND	2.73 ND
Propionaldehyde	0.381 J	0.290 J	0.236 ND	3.00 ND	3.00 ND	3.00 ND
acetaldehyde	0.691 J	0.695 J	0.759 J	4.65	3.92 J	3.75
	Data Runs					
	Dryer 2 Run 1	Dryer 2 Run 2	Dryer 2 Run 3			
Acrolein	1.90 J	2.59	2.49			
Formaldehyde	6.40	6.58	6.76			
Methanol	18.8	10.2	10.8			
Phenol	2.78 ND	2.78 ND	2.78 ND			
Propionaldehyde	2.37	1.38	1.70			
acetaldehyde	0.967 J	3.28	1.02 J			

Company ACT
Analyst Initials CJT
Parameters EPA Method 320
Samples 21 Runs

Client # 1911
Job # 0913-111
PO # 3134 1911
Report Date V0.62 13.10.18.12.58

Minimum Detectable Concentration - Default

	GMH	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
	Run 1	1.13	0.502	0.742	0.0719	0.51	0.0912	0.88	0.44	0.234	0.120	0.756	0.371
	Run 2	1.20	0.474	0.629	0.0684	0.46	0.0935	0.88	0.44	0.234	0.118	0.721	0.351
	Run 3	1.15	0.480	0.561	0.0677	0.38	0.0913	0.88	0.45	0.251	0.113	0.723	0.355
Average SEC(ppm):		0.485		0.0693		0.0920		0.44		0.117		0.359	
MDC(ppm):		0.971		0.139		0.184		0.88		0.234		0.718	
Dryer 1													
	Run 1	1.79	0.917	3.32	0.131	2.52	0.296	2.04	1.00	0.644	0.239	1.270	0.679
	Run 2	1.72	0.850	1.60	0.126	1.70	0.293	2.04	1.07	0.714	0.227	1.270	0.628
	Run 3	1.72	0.812	1.78	0.120	1.59	0.287	2.04	0.99	0.505	0.213	1.270	0.598
Average SEC(ppm):		0.859		0.126		0.292		1.02		0.226		0.635	
MDC(ppm):		1.72		0.252		0.584		2.04		0.452		1.27	
Pellet Cooler 2													
	Run 1	1.29	0.496	1.07	0.0711	0.80	0.0813	1.08	0.54	0.246	0.125	0.864	0.370
	Run 2	1.21	0.497	0.663	0.0704	0.68	0.0823	1.08	0.54	0.246	0.120	0.825	0.370
	Run 3	1.33	0.507	1.84	0.0732	0.84	0.0844	1.09	0.55	0.359	0.124	0.786	0.378
Average SEC(ppm):		0.500		0.0716		0.0826		0.54		0.123		0.373	
MDC(ppm):		1.00		0.143		0.165		1.08		0.246		0.745	
Hammermill 2													
	Run 1	0.98	0.480	1.04	0.0677	0.19	0.0809	1.08	0.54	0.233	0.113	0.715	0.353
	Run 2	0.97	0.480	1.14	0.0682	0.21	0.0832	1.08	0.54	0.243	0.122	0.710	0.352
	Run 3	0.97	0.488	1.11	0.0675	0.20	0.0839	1.08	0.55	0.263	0.113	0.707	0.356
Average SEC(ppm):		0.483		0.0678		0.0826		0.54		0.116		0.354	
MDC(ppm):		0.965		0.136		0.165		1.08		0.232		0.707	
Pellet Cooler 1													
	Run 1	0.98	0.467	1.44	0.0646	0.54	0.0738	1.00	0.50	0.381	0.118	0.691	0.344
	Run 2	1.02	0.463	1.25	0.0635	0.33	0.0723	0.98	0.50	0.290	0.119	0.695	0.341
	Run 3	1.35	0.467	1.26	0.0647	0.35	0.0690	0.98	0.48	0.236	0.118	0.759	0.345
Average SEC(ppm):		0.466		0.0642		0.0717		0.49		0.118		0.343	
MDC(ppm):		0.931		0.128		0.143		0.98		0.236		0.686	
Aspirator													
	Run 1	3.16	0.827	1.055	0.535	8.30	0.244	2.73	1.15	3.00	1.53	4.65	0.616
	Run 2	3.12	0.808	1.58	0.467	8.90	0.256	2.73	1.60	3.00	1.35	3.92	0.602
	Run 3	2.25	0.916	1.063	0.580	8.16	0.265	2.73	1.34	3.00	1.62	3.75	0.681
Average SEC(ppm):		0.850		0.527		0.255		1.36		1.50		0.633	
MDC(ppm):		1.70		1.05		0.510		2.73		3.00		1.27	
Dryer 2													
	Run 1	1.90	0.631	6.40	0.108	18.8	0.539	2.78	1.29	2.37	0.222	0.967	0.472
	Run 2	2.59	0.617	6.58	0.105	10.2	0.549	2.78	1.55	1.38	0.260	3.28	0.457
	Run 3	2.49	0.633	6.76	0.112	10.8	0.531	2.78	1.33	1.70	0.263	1.02	0.473
Average SEC(ppm):		0.627		0.108		0.540		1.39		0.248		0.467	
MDC(ppm):		1.25		0.217		1.08		2.78		0.497		0.934	

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	VO.62 13.10.18.12.58

GMH Run 1															
Date	Method	Filename	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/10/2013 9:17	0913-111, A	13, 10, 10, 0917, 37, 936	1	1.58	0.517	0.846	0.0700	0.434	0.0900	0.88	0.43	0.234	0.114	0.718	0.383
10/10/2013 9:18	0913-111, A	13, 10, 10, 0918, 38, 786	1	0.971	0.472	0.708	0.0680	0.457	0.0880	0.88	0.43	0.234	0.112	0.718	0.346
10/10/2013 9:19	0913-111, A	13, 10, 10, 0919, 39, 506	1	0.971	0.504	0.778	0.0720	0.443	0.0920	0.88	0.43	0.234	0.115	0.718	0.373
10/10/2013 9:20	0913-111, A	13, 10, 10, 0920, 40, 336	1	0.971	0.464	0.696	0.0690	0.467	0.0860	0.88	0.44	0.234	0.111	0.718	0.345
10/10/2013 9:21	0913-111, A	13, 10, 10, 0921, 41, 006	1	1.59	0.483	0.633	0.0700	0.454	0.0920	0.88	0.43	0.234	0.114	0.993	0.365
10/10/2013 9:22	0913-111, A	13, 10, 10, 0922, 41, 806	1	0.971	0.493	0.708	0.0680	0.457	0.0880	0.88	0.44	0.234	0.114	0.718	0.360
10/10/2013 9:23	0913-111, A	13, 10, 10, 0923, 42, 538	1	0.971	0.464	0.614	0.0660	0.469	0.0880	0.88	0.44	0.234	0.111	0.718	0.341
10/10/2013 9:24	0913-111, A	13, 10, 10, 0924, 43, 348	1	1.15	0.462	0.696	0.0630	0.481	0.0900	0.88	0.44	0.234	0.111	0.718	0.336
10/10/2013 9:25	0913-111, A	13, 10, 10, 0925, 44, 128	1	0.971	0.465	0.696	0.0680	0.477	0.0900	0.88	0.43	0.234	0.110	0.718	0.347
10/10/2013 9:26	0913-111, A	13, 10, 10, 0926, 44, 818	1	0.971	0.498	0.782	0.0660	0.407	0.0870	0.88	0.44	0.234	0.115	0.750	0.375
10/10/2013 9:27	0913-111, A	13, 10, 10, 0927, 45, 818	1	0.971	0.459	0.759	0.0660	0.491	0.0870	0.88	0.44	0.234	0.108	0.718	0.335
10/10/2013 9:28	0913-111, A	13, 10, 10, 0928, 46, 429	1	1.16	0.499	0.820	0.0690	0.383	0.0890	0.88	0.44	0.234	0.116	0.718	0.370
10/10/2013 9:29	0913-111, A	13, 10, 10, 0929, 47, 159	1	1.61	0.471	0.784	0.0680	0.445	0.0870	0.88	0.43	0.234	0.113	0.718	0.348
10/10/2013 9:30	0913-111, A	13, 10, 10, 0930, 47, 959	1	0.971	0.454	0.803	0.0660	0.537	0.0880	0.88	0.44	0.234	0.111	0.718	0.332
10/10/2013 9:31	0913-111, A	13, 10, 10, 0931, 48, 709	1	0.971	0.477	0.775	0.0700	0.442	0.0910	0.88	0.44	0.234	0.118	0.718	0.353
10/10/2013 9:32	0913-111, A	13, 10, 10, 0932, 49, 519	1	0.971	0.460	0.746	0.0660	0.477	0.0910	0.88	0.44	0.234	0.113	0.718	0.348
10/10/2013 9:33	0913-111, A	13, 10, 10, 0933, 50, 289	1	0.971	0.491	0.723	0.0730	0.473	0.0890	0.88	0.44	0.234	0.118	0.718	0.357
10/10/2013 9:34	0913-111, A	13, 10, 10, 0934, 50, 859	1	0.971	0.491	0.731	0.0680	0.456	0.0910	0.88	0.44	0.234	0.117	0.718	0.360
10/10/2013 9:35	0913-111, A	13, 10, 10, 0935, 51, 689	1	0.971	0.469	0.739	0.0680	0.477	0.0870	0.88	0.44	0.234	0.112	0.718	0.349
10/10/2013 9:36	0913-111, A	13, 10, 10, 0936, 52, 439	1	0.971	0.483	0.650	0.0710	0.446	0.0890	0.88	0.44	0.234	0.117	0.718	0.359
10/10/2013 9:37	0913-111, A	13, 10, 10, 0937, 53, 149	1	1.32	0.497	0.751	0.0700	0.448	0.0910	0.88	0.44	0.234	0.116	0.718	0.373
10/10/2013 9:38	0913-111, A	13, 10, 10, 0938, 53, 929	1	0.971	0.467	0.668	0.0680	0.467	0.0890	0.88	0.44	0.234	0.115	0.718	0.345
10/10/2013 9:39	0913-111, A	13, 10, 10, 0939, 54, 720	1	0.971	0.483	0.800	0.0720	0.416	0.0930	0.88	0.44	0.234	0.118	0.718	0.354
10/10/2013 9:40	0913-111, A	13, 10, 10, 0940, 55, 430	1	0.971	0.487	0.703	0.0680	0.393	0.0910	0.88	0.44	0.234	0.117	0.718	0.357
10/10/2013 9:41	0913-111, A	13, 10, 10, 0941, 56, 230	1	0.971	0.504	0.775	0.0710	0.435	0.0870	0.88	0.44	0.234	0.118	0.718	0.370
10/10/2013 9:42	0913-111, A	13, 10, 10, 0942, 57, 010	1	1.10	0.501	0.613	0.0700	0.470	0.0910	0.88	0.44	0.234	0.117	0.718	0.367
10/10/2013 9:43	0913-111, A	13, 10, 10, 0943, 57, 650	1	0.971	0.473	0.697	0.0690	0.415	0.0910	0.88	0.44	0.234	0.112	0.718	0.347
10/10/2013 9:44	0913-111, A	13, 10, 10, 0944, 58, 440	1	0.971	0.477	0.736	0.0670	0.393	0.0910	0.88	0.44	0.234	0.113	0.718	0.349
10/10/2013 9:45	0913-111, A	13, 10, 10, 0945, 59, 220	1	0.971	0.482	0.634	0.0670	0.388	0.0910	0.88	0.44	0.234	0.109	0.718	0.355
10/10/2013 9:47	0913-111, A	13, 10, 10, 0947, 60, 000	1	1.48	0.477	0.644	0.0690	0.459	0.0890	0.88	0.44	0.234	0.116	0.742	0.355
10/10/2013 9:48	0913-111, A	13, 10, 10, 0948, 60, 730	1	0.971	0.461	0.774	0.0660	0.420	0.0880	0.88	0.44	0.234	0.112	0.718	0.337
10/10/2013 9:49	0913-111, A	13, 10, 10, 0949, 61, 480	1	1.29	0.487	0.773	0.0640	0.501	0.0910	0.88	0.44	0.234	0.112	0.718	0.359
10/10/2013 9:50	0913-111, A	13, 10, 10, 0950, 62, 280	1	0.971	0.483	0.721	0.0680	0.464	0.0910	0.88	0.44	0.234	0.115	0.718	0.353
10/10/2013 9:51	0913-111, A	13, 10, 10, 0951, 63, 020	1	0.971	0.476	0.710	0.0700	0.457	0.0870	0.88	0.44	0.234	0.117	0.718	0.363
10/10/2013 9:52	0913-111, A	13, 10, 10, 0952, 63, 761	1	0.971	0.489	0.683	0.0700	0.523	0.0880	0.88	0.44	0.234	0.119	0.735	0.364
10/10/2013 9:53	0913-111, A	13, 10, 10, 0953, 64, 581	1	0.971	0.500	0.789	0.0690	0.523	0.0880	0.88	0.44	0.234	0.118	0.718	0.368
10/10/2013 9:54	0913-111, A	13, 10, 10, 0954, 65, 281	1	0.971	0.455	0.737	0.0660	0.490	0.0900	0.88	0.44	0.234	0.114	0.740	0.339
10/10/2013 9:55	0913-111, A	13, 10, 10, 0955, 66, 091	1	1.41	0.469	0.869	0.0710	0.647	0.0950	0.88	0.44	0.234	0.118	0.718	0.351
10/10/2013 9:56	0913-111, A	13, 10, 10, 0956, 66, 811	1	0.971	0.513	0.980	0.0740	0.645	0.0910	0.88	0.44	0.234	0.124	0.718	0.382
10/10/2013 9:57	0913-111, A	13, 10, 10, 0957, 67, 611	1	1.30	0.482	0.870	0.0720	0.667	0.0960	0.88	0.44	0.234	0.122	0.990	0.356
10/10/2013 9:58	0913-111, A	13, 10, 10, 0958, 68, 331	1	0.971	0.488	0.920	0.0700	0.688	0.0950	0.88	0.44	0.234	0.117	0.947	0.366
10/10/2013 9:59	0913-111, A	13, 10, 10, 0959, 69, 071	1	1.42	0.496	0.677	0.0700	0.649	0.0930	0.88	0.44	0.234	0.119	0.872	0.364
10/10/2013 10:00	0913-111, A	13, 10, 10, 1000, 69, 811	1	0.971	0.492	0.821	0.0700	0.564	0.0920	0.88	0.44	0.234	0.117	0.747	0.360
10/10/2013 10:01	0913-111, A	13, 10, 10, 1001, 70, 015	1	1.62	0.494	0.864	0.0720	0.597	0.0930	0.88	0.44	0.234	0.123	0.718	0.376
10/10/2013 10:02	0913-111, A	13, 10, 10, 1002, 71, 391	1	0.971	0.487	0.650	0.0680	0.580	0.0920	0.88	0.44	0.234	0.114	0.866	0.363
10/10/2013 10:03	0913-111, A	13, 10, 10, 1003, 72, 111	1	1.80	0.503	0.846	0.0710	0.577	0.0930	0.88	0.44	0.234	0.118	0.718	0.368
10/10/2013 10:04	0913-111, A	13, 10, 10, 1004, 72, 832	1	0.978	0.474	0.794	0.0690	0.664	0.0920	0.88	0.44	0.234	0.118	0.718	0.356
10/10/2013 10:05	0913-111, A	13, 10, 10, 1005, 73, 642	1	1.21	0.489	0.819	0.0760	0.593	0.0890	0.88	0.44	0.234	0.124	0.718	0.364
10/10/2013 10:06	0913-111, A	13, 10, 10, 1006, 74, 372	1	0.971	0.476	0.718	0.0710	0.644	0.0930	0.88	0.44	0.234	0.118	0.718	0.353
10/10/2013 10:07	0913-111, A	13, 10, 10, 1007, 75, 182	1	1.07	0.497	0.769	0.0720	0.727	0.0910	0.88	0.44	0.234	0.125	0.718	0.367
10/10/2013 10:08	0913-111, A	13, 10, 10, 1008, 75, 892	1	1.28	0.512	0.804	0.0750	0.660	0.0950	0.88	0.44	0.234	0.124	0.718	0.383
10/10/2013 10:09	0913-111, A	13, 10, 10, 1009, 76, 712	1	1.61	0.551	0.828	0.0820	0.582	0.0910	0.88	0.44	0.234	0.133	0.718	0.406
10/10/2013 10:10	0913-111, A	13, 10, 10, 1010, 77, 422	1	0.986	0.559	0.706	0.0790	0.620	0.0940	0.88	0.44	0.234	0.133	0.718	0.417
10/10/2013 10:11	0913-111, A	13, 10, 10, 1011, 78, 172	1	1.39	0.537	0.667	0.0780	0.631	0.0920	0.88	0.44	0.234	0.134	0.900	0.395
10/10/2013 10:12	0913-111, A	13, 10, 10, 1012, 78, 922	1	0.971	0.535	0.703	0.0770	0.435	0.0950	0.88	0.43	0.234	0.130	1.28	0.393
10/10/2013 10:13	0913-111, A	13, 10, 10, 1013, 79, 722	1	1.48	0.582	0.825	0.0840	0.497	0.0970	0.88	0.43	0.234	0.139	1.05	0.429
10/10/2013 10:14	0913-111, A	13, 10, 10, 1014, 80, 442	1	0.999	0.682	0.594	0.0930	0.537	0.0950	0.88	0.43	0.234	0.155	0.718	0.495
10/10/2013 10:15	0913-111, A	13, 10, 10, 1015, 21, 272	1	1.71	0.651	0.563	0.0920	0.501	0.0970	0.88	0.43	0.234	0.150	0.718	0.477
10/10/2013 10:16	0913-111, A	13, 10, 10, 1016, 21, 893	1	0.971	0.705	0.431	0.0								

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	V0.62 13.10.18.12.58

Date	Method	Filename	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/10/2013 17:38	0913-111-A	13_10_10_1738_19_855	1	1.87	0.969	5.44	1.145	3.31	0.311	2.04	0.84	1.16	0.253	1.27	0.711	
10/10/2013 17:41	0913-111-A	13_10_10_1738_20_451	1	2.01	0.979	5.39	1.142	3.31	0.312	2.04	0.84	1.36	0.258	1.27	0.725	
10/10/2013 17:41	0913-111-A	13_10_10_1741_33_410	1	1.72	0.949	5.44	1.046	3.31	0.314	2.04	0.89	1.18	0.258	1.27	0.703	
10/10/2013 17:42	0913-111-A	13_10_10_1742_34_100	1	1.00	0.963	5.60	1.046	3.32	0.318	2.04	0.88	1.13	0.259	1.27	0.712	
10/10/2013 17:43	0913-111-A	13_10_10_1743_34_860	1	2.27	0.976	5.77	1.048	3.46	0.323	2.04	0.88	1.02	0.267	1.27	0.719	
10/10/2013 17:44	0913-111-A	13_10_10_1744_35_610	1	1.72	0.988	6.15	1.048	3.65	0.326	2.04	0.85	1.24	0.264	1.27	0.725	
10/10/2013 17:44	0913-111-A	13_10_10_1745_36_400	1	1.99	0.979	6.15	1.045	3.74	0.326	2.04	0.85	1.25	0.269	1.27	0.727	
10/10/2013 17:46	0913-111-A	13_10_10_1746_37_220	1	1.95	1.01	6.74	1.051	3.88	0.330	2.04	0.85	1.16	0.269	1.27	0.735	
10/10/2013 17:47	0913-111-A	13_10_10_1747_37_980	1	2.68	0.984	6.60	1.047	3.84	0.323	2.04	0.87	1.21	0.267	1.27	0.728	
10/10/2013 17:48	0913-111-A	13_10_10_1748_38_700	1	1.78	0.985	6.70	1.052	3.85	0.319	2.04	0.88	1.22	0.268	1.27	0.724	
10/10/2013 17:47	0913-111-A	13_10_10_1748_38_446	1	2.02	1.01	6.10	1.042	3.82	0.310	2.04	0.88	1.10	0.267	1.27	0.738	
10/10/2013 17:50	0913-111-A	13_10_10_1750_40_260	1	2.05	0.960	5.27	1.039	3.31	0.307	2.04	0.90	0.847	0.252	1.27	0.707	
10/10/2013 17:51	0913-111-A	13_10_10_1751_41_070	1	1.72	0.956	4.78	1.035	3.07	0.307	2.04	0.91	0.728	0.251	1.27	0.702	
10/10/2013 17:52	0913-111-A	13_10_10_1752_41_790	1	1.72	0.967	4.48	1.037	2.94	0.306	2.04	0.93	0.560	0.250	1.27	0.709	
10/10/2013 17:53	0913-111-A	13_10_10_1753_42_537	1	1.90	0.957	3.90	1.030	2.93	0.307	2.04	0.91	0.514	0.251	1.27	0.704	
10/10/2013 17:54	0913-111-A	13_10_10_1754_43_251	1	1.72	0.943	3.70	1.035	2.69	0.297	2.04	0.96	0.452	0.253	1.27	0.696	
10/10/2013 17:55	0913-111-A	13_10_10_1755_44_091	1	1.79	0.903	3.57	1.035	2.58	0.294	2.04	0.96	0.452	0.246	1.27	0.685	
10/10/2013 17:56	0913-111-A	13_10_10_1756_44_841	1	1.72	0.961	3.29	1.035	2.45	0.293	2.04	0.98	0.452	0.247	1.27	0.712	
10/10/2013 17:57	0913-111-A	13_10_10_1757_45_591	1	2.09	0.903	3.00	1.030	2.46	0.295	2.04	0.99	0.452	0.237	1.27	0.670	
10/10/2013 17:58	0913-111-A	13_10_10_1758_46_391	1	1.72	0.909	2.91	1.032	2.41	0.289	2.04	1.01	0.452	0.243	1.27	0.680	
10/10/2013 17:59	0913-111-A	13_10_10_1759_47_171	1	1.72	0.908	2.72	1.031	2.21	0.286	2.04	1.01	0.452	0.239	1.27	0.670	
10/10/2013 18:00	0913-111-A	13_10_10_1800_47_881	1	1.72	0.931	2.52	1.029	2.22	0.281	2.04	1.04	0.452	0.241	1.27	0.698	
10/10/2013 18:01	0913-111-A	13_10_10_1801_48_651	1	1.92	0.903	2.45	1.030	2.24	0.277	2.04	1.04	0.452	0.240	1.27	0.672	
10/10/2013 18:02	0913-111-A	13_10_10_1802_49_481	1	1.72	0.919	2.17	1.029	2.05	0.272	2.04	1.06	0.452	0.236	1.27	0.688	
10/10/2013 18:03	0913-111-A	13_10_10_1803_50_191	1	1.72	0.862	2.18	1.023	1.96	0.272	2.04	1.07	0.452	0.228	1.27	0.644	
10/10/2013 18:04	0913-111-A	13_10_10_1804_51_001	1	1.72	0.856	2.04	1.020	2.08	0.282	2.04	1.07	0.452	0.224	1.27	0.638	
10/10/2013 18:05	0913-111-A	13_10_10_1805_51_742	1	1.72	0.901	2.12	1.026	2.01	0.266	2.04	1.06	0.452	0.230	1.27	0.664	
10/10/2013 18:06	0913-111-A	13_10_10_1806_52_442	1	1.72	0.910	2.33	1.027	2.13	0.295	2.04	1.04	0.452	0.232	1.27	0.671	
10/10/2013 18:07	0913-111-A	13_10_10_1807_53_232	1	1.72	0.901	2.55	1.027	2.22	0.292	2.04	1.02	0.452	0.239	1.27	0.666	
10/10/2013 18:08	0913-111-A	13_10_10_1808_53_952	1	1.72	0.938	2.54	1.028	2.23	0.298	2.04	1.02	0.452	0.242	1.27	0.691	
10/10/2013 18:09	0913-111-A	13_10_10_1809_54_762	1	1.72	0.944	2.72	1.029	2.26	0.298	2.04	1.02	0.452	0.242	1.27	0.706	
10/10/2013 18:10	0913-111-A	13_10_10_1810_55_572	1	1.72	0.908	2.54	1.027	2.30	0.298	2.04	1.00	0.452	0.233	1.27	0.672	
10/10/2013 18:11	0913-111-A	13_10_10_1811_56_282	1	1.72	0.879	2.86	1.024	2.40	0.306	2.04	1.00	0.452	0.228	1.27	0.654	
10/10/2013 18:12	0913-111-A	13_10_10_1812_57_092	1	1.72	0.930	3.03	1.029	2.62	0.310	2.04	0.99	0.452	0.238	1.27	0.690	
10/10/2013 18:13	0913-111-A	13_10_10_1813_57_812	1	1.72	0.941	3.21	1.030	2.72	0.307	2.04	0.97	0.452	0.239	1.27	0.703	
10/10/2013 18:14	0913-111-A	13_10_10_1814_58_622	1	1.72	0.922	3.36	1.033	2.59	0.306	2.04	0.97	0.452	0.238	1.27	0.684	
10/10/2013 18:15	0913-111-A	13_10_10_1815_59_382	1	1.72	0.927	3.14	1.029	2.69	0.302	2.04	0.97	0.452	0.237	1.27	0.685	
10/10/2013 18:17	0913-111-A	13_10_10_1817_00_093	1	1.86	0.926	2.95	1.029	2.59	0.296	2.04	0.96	0.452	0.238	1.27	0.697	
10/10/2013 18:18	0913-111-A	13_10_10_1818_00_713	1	1.72	0.924	3.03	1.029	2.49	0.293	2.04	0.99	0.452	0.235	1.27	0.684	
10/10/2013 18:19	0913-111-A	13_10_10_1819_01_512	1	1.72	0.927	2.77	1.029	2.51	0.297	2.04	0.97	0.452	0.236	1.27	0.689	
10/10/2013 18:20	0913-111-A	13_10_10_1820_02_313	1	1.72	0.906	2.49	1.028	2.20	0.284	2.04	1.02	0.452	0.229	1.27	0.671	
10/10/2013 18:21	0913-111-A	13_10_10_1821_03_043	1	1.72	0.903	2.25	1.027	2.16	0.283	2.04	1.05	0.452	0.231	1.27	0.667	
10/10/2013 18:22	0913-111-A	13_10_10_1822_03_843	1	1.72	0.878	2.31	1.023	2.06	0.284	2.04	1.07	0.452	0.225	1.27	0.653	
10/10/2013 18:23	0913-111-A	13_10_10_1823_04_563	1	1.72	0.887	2.38	1.025	2.18	0.285	2.04	1.06	0.452	0.226	1.27	0.658	
10/10/2013 18:24	0913-111-A	13_10_10_1824_05_383	1	1.72	0.873	2.37	1.022	2.15	0.291	2.04	1.10	0.452	0.225	1.27	0.642	
10/10/2013 18:25	0913-111-A	13_10_10_1825_06_133	1	1.72	0.877	2.31	1.025	2.13	0.292	2.04	1.10	0.452	0.224	1.27	0.652	
10/10/2013 18:26	0913-111-A	13_10_10_1826_06_673	1	1.72	0.916	2.29	1.027	2.12	0.288	2.04	1.10	0.452	0.232	1.27	0.683	
10/10/2013 18:27	0913-111-A	13_10_10_1827_07_663	1	1.72	0.855	2.33	1.027	2.24	0.287	2.04	1.07	0.452	0.226	1.27	0.637	
10/10/2013 18:28	0913-111-A	13_10_10_1828_08_403	1	1.72	0.869	2.36	1.023	2.11	0.288	2.04	1.06	0.462	0.224	1.27	0.642	
10/10/2013 18:29	0913-111-A	13_10_10_1829_09_244	1	1.72	0.846	2.51	1.025	2.24	0.288	2.04	1.06	0.489	0.223	1.27	0.627	
10/10/2013 18:30	0913-111-A	13_10_10_1830_09_954	1	1.72	0.883	2.29	1.026	2.12	0.280	2.04	1.01	0.575	0.227	1.27	0.657	
10/10/2013 18:31	0913-111-A	13_10_10_1831_10_773	1	1.72	0.861	2.07	1.023	2.12	0.282	2.04	1.02	0.580	0.227	1.27	0.641	
10/10/2013 18:32	0913-111-A	13_10_10_1832_10_484	1	1.72	0.855	2.07	1.020	1.92	0.281	2.04	1.10	0.719	0.221	1.27	0.635	
10/10/2013 18:33	0913-111-A	13_10_10_1833_12_074	1	1.72	0.872	2.11	1.022	1.96	0.284	2.04	1.11	0.732	0.222	1.27	0.639	
10/10/2013 18:34	0913-111-A	13_10_10_1834_13_124	1	1.72	0.874	2.08	1.020	1.86	0.283	2.04	1.13	0.748	0.220	1.27	0.642	
10/10/2013 18:35	0913-111-A	13_10_10_1835_13_863	1	1.72	0.872	2.10	1.020	1.82	0.282	2.04	1.12	0.752	0.221	1.27	0.654	
10/10/2013 18:36	0913-111-A	13_10_10_1836_14_564	1	1.72	0.875	1.73	1.028	1.74	0.280	2.04	1.10	0.717	0.230	1.27	0.657	
10/10/2013 18:37	0913-111-A	13_10_10_1837_15_364	1	1.72	0.852	1.71	1.024	1.63	0.275	2.04	1.11	0.735	0.221	1.27	0.630	
10/10/2013 18:38	0913-111-A	13_10_10_1838_16_164	1	1.72	0.839	1.76	1.018	1.67	0.280	2.04	1.13	0.806	0.216	1.27	0.622	
Average Conc (ppm):				1	1.79	0.917	3.32	0.131	2.52	0.296	2.04	1.00	0.644	0.239	1.27	0.679

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	V0.62 13.10.18.12.58

Date	Method	Filename	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/11/2013 11:37	0913-111-A	13_10_11_1137_48_370	1	1.72	0.785	1.48	0.117	1.23	0.285	2.04	1.07	0.452	0.217	1.27	0.580	
10/11/2013 11:38	0913-111-A	13_10_11_1138_49_370	1	1.72	0.778	1.61	0.119	1.23	0.285	2.04	1.06	0.452	0.211	1.27	0.572	
10/11/2013 11:39	0913-111-A	13_10_11_1139_50_161	1	1.72	0.790	1.54	0.120	1.23	0.284	2.04	1.05	0.452	0.217	1.27	0.579	
10/11/2013 11:40	0913-111-A	13_10_11_1140_50_630	1	1.72	0.811	1.65	0.123	1.36	0.282	2.04	1.05	0.452	0.221	1.27	0.600	
10/11/2013 11:41	0913-111-A	13_10_11_1141_51_950	1	1.72	0.804	1.67	0.119	1.30	0.277	2.04	1.04	0.452	0.216	1.27	0.591	
10/11/2013 11:42	0913-111-A	13_10_11_1142_52_480	1	1.72	0.814	1.55	0.122	1.30	0.276	2.04	1.04	0.452	0.218	1.27	0.601	
10/11/2013 11:43	0913-111-A	13_10_11_1143_53_127	1	1.72	0.821	1.57	0.123	1.27	0.277	2.04	1.02	0.452	0.221	1.27	0.606	
10/11/2013 11:44	0913-111-A	13_10_11_1144_53_970	1	1.72	0.798	1.47	0.121	1.27	0.278	2.04	1.02	0.452	0.217	1.27	0.585	
10/11/2013 11:45	0913-111-A	13_10_11_1145_54_690	1	1.72	0.825	1.60	0.120	1.30	0.277	2.04	1.03	0.452	0.218	1.27	0.605	
10/11/2013 11:46	0913-111-A	13_10_11_1146_55_471	1	1.72	0.782	1.71	0.118	1.39	0.278	2.04	1.05	0.452	0.210	1.27	0.580	
10/11/2013 11:47	0913-111-A	13_10_11_1147_56_221	1	1.72	0.807	1.58	0.120	1.35	0.278	2.04	1.04	0.452	0.212	1.27	0.589	
10/11/2013 11:48	0913-111-A	13_10_11_1148_57_04	1	1.72	0.839	1.67	0.120	1.44	0.280	2.04	1.07	0.452	0.212	1.27	0.618	
10/11/2013 11:49	0913-111-A	13_10_11_1149_57_761	1	1.72	0.782	1.69	0.116	1.55	0.279	2.04	1.02	0.464	0.203	1.27	0.581	
10/11/2013 11:50	0913-111-A	13_10_11_1150_58_531	1	1.72	0.803	1.55	0.119	1.52	0.276	2.04	1.02	0.452	0.206	1.27	0.595	
10/11/2013 11:51	0913-111-A	13_10_11_1151_59_131	1	1.72	0.808	1.60	0.119	1.55	0.277	2.04	1.03	0.452	0.208	1.27	0.595	
10/11/2013 11:52	0913-111-A	13_10_11_1152_59_90	1	1.72	0.801	1.61	0.119	1.52	0.280	2.04	1.02	0.452	0.208	1.27	0.591	
10/11/2013 11:53	0913-111-A	13_10_11_1154_00_611	1	1.72	0.781	1.61	0.120	1.58	0.288	2.04	0.99	0.452	0.204	1.27	0.574	
10/11/2013 11:54	0913-111-A	13_10_11_1155_01_421	1	1.72	0.864	1.72	0.120	1.63	0.290	2.04	0.98	0.452	0.209	1.27	0.635	
10/11/2013 11:55	0913-111-A	13_10_11_1156_02_101	1	1.72	0.812	1.74	0.123	1.65	0.286	2.04	0.97	0.452	0.209	1.27	0.602	
10/11/2013 11:57	0913-111-A	13_10_11_1157_03_02	1	1.72	0.809	1.72	0.117	1.67	0.285	2.04	0.99	0.463	0.205	1.27	0.589	
10/11/2013 11:58	0913-111-A	13_10_11_1158_03_661	1	1.72	0.776	1.56	0.116	1.67	0.282	2.04	0.99	0.562	0.201	1.27	0.574	
10/11/2013 11:59	0913-111-A	13_10_11_1159_04_382	1	1.72	0.805	1.70	0.126	1.60	0.281	2.04	0.99	0.576	0.213	1.27	0.603	
10/11/2013 12:00	0913-111-A	13_10_11_1200_05_122	1	1.72	0.838	1.68	0.123	1.62	0.287	2.04	0.99	0.452	0.212	1.27	0.616	
10/11/2013 12:01	0913-111-A	13_10_11_1201_05_832	1	1.72	0.775	1.72	0.116	1.67	0.286	2.04	1.01	0.452	0.201	1.27	0.572	
10/11/2013 12:02	0913-111-A	13_10_11_1202_06_592	1	1.72	0.812	1.59	0.119	1.57	0.277	2.04	1.00	0.452	0.208	1.27	0.599	
10/11/2013 12:03	0913-111-A	13_10_11_1203_07_332	1	1.72	0.799	1.64	0.122	1.61	0.284	2.04	1.01	0.452	0.206	1.27	0.594	
10/11/2013 12:04	0913-111-A	13_10_11_1204_08_092	1	1.72	0.823	1.64	0.120	1.59	0.286	2.04	1.01	0.625	0.208	1.27	0.605	
10/11/2013 12:05	0913-111-A	13_10_11_1205_08_912	1	1.72	0.835	1.78	0.116	1.63	0.284	2.04	0.99	0.533	0.208	1.27	0.615	
10/11/2013 12:06	0913-111-A	13_10_11_1206_08_585	1	1.72	0.819	1.71	0.119	1.59	0.288	2.04	0.99	0.526	0.208	1.27	0.597	
10/11/2013 12:07	0913-111-A	13_10_11_1207_10_432	1	1.72	0.827	1.81	0.123	1.67	0.290	2.04	0.97	0.491	0.215	1.27	0.610	
10/11/2013 12:08	0913-111-A	13_10_11_1208_11_142	1	1.72	0.789	1.70	0.116	1.62	0.282	2.04	0.98	0.452	0.204	1.27	0.581	
10/11/2013 12:09	0913-111-A	13_10_11_1209_11_902	1	1.72	0.817	1.76	0.115	1.62	0.285	2.04	0.99	0.508	0.200	1.27	0.598	
10/11/2013 12:10	0913-111-A	13_10_11_1210_12_712	1	1.72	0.800	1.72	0.117	1.62	0.280	2.04	1.00	0.452	0.207	1.27	0.599	
10/11/2013 12:11	0913-111-A	13_10_11_1211_13_142	1	1.72	0.806	1.71	0.118	1.60	0.285	2.04	0.99	0.452	0.206	1.27	0.595	
10/11/2013 12:12	0913-111-A	13_10_11_1212_14_173	1	1.72	0.782	1.74	0.121	1.63	0.286	2.04	1.00	0.452	0.209	1.27	0.577	
10/11/2013 12:13	0913-111-A	13_10_11_1213_14_893	1	1.72	0.806	1.53	0.118	1.67	0.284	2.04	1.00	0.452	0.206	1.27	0.595	
10/11/2013 12:14	0913-111-A	13_10_11_1214_15_705	1	1.72	0.828	1.69	0.119	1.62	0.288	2.04	0.99	0.452	0.215	1.27	0.602	
10/11/2013 12:15	0913-111-A	13_10_11_1215_16_453	1	1.72	0.801	1.73	0.118	1.59	0.282	2.04	0.99	0.474	0.207	1.27	0.591	
10/11/2013 12:16	0913-111-A	13_10_11_1216_17_183	1	1.72	0.830	1.78	0.122	1.62	0.287	2.04	0.98	0.474	0.215	1.27	0.607	
10/11/2013 12:17	0913-111-A	13_10_11_1217_18_003	1	1.72	0.803	1.84	0.119	1.61	0.292	2.04	0.97	0.452	0.209	1.27	0.590	
10/11/2013 12:18	0913-111-A	13_10_11_1218_18_713	1	1.72	0.769	1.85	0.119	1.68	0.287	2.04	0.97	0.555	0.208	1.27	0.567	
10/11/2013 12:19	0913-111-A	13_10_11_1219_19_492	1	1.72	0.801	1.80	0.121	1.68	0.285	2.04	0.98	0.452	0.216	1.27	0.580	
10/11/2013 12:20	0913-111-A	13_10_11_1220_20_233	1	1.72	0.801	1.88	0.121	1.64	0.287	2.04	0.98	0.452	0.213	1.27	0.588	
10/11/2013 12:21	0913-111-A	13_10_11_1221_20_953	1	1.72	0.816	1.74	0.119	1.59	0.286	2.04	0.98	0.532	0.212	1.27	0.604	
10/11/2013 12:22	0913-111-A	13_10_11_1222_21_693	1	1.72	0.801	2.02	0.119	1.68	0.291	2.04	0.98	0.509	0.212	1.27	0.592	
10/11/2013 12:23	0913-111-A	13_10_11_1223_22_456	1	1.72	0.825	1.90	0.121	1.62	0.285	2.04	0.98	0.452	0.221	1.27	0.614	
10/11/2013 12:24	0913-111-A	13_10_11_1224_23_184	1	1.72	0.825	1.88	0.122	1.72	0.296	2.04	0.96	0.633	0.217	1.27	0.611	
10/11/2013 12:25	0913-111-A	13_10_11_1225_23_994	1	1.72	0.845	1.97	0.121	1.77	0.293	2.04	0.97	0.614	0.220	1.27	0.627	
10/11/2013 12:26	0913-111-A	13_10_11_1226_24_704	1	1.72	0.826	2.00	0.121	1.71	0.307	2.04	0.96	0.544	0.221	1.27	0.611	
10/11/2013 12:27	0913-111-A	13_10_11_1227_25_512	1	1.72	0.839	1.98	0.121	1.77	0.317	2.04	0.97	0.648	0.219	1.27	0.630	
10/11/2013 12:28	0913-111-A	13_10_11_1228_26_234	1	1.72	0.830	2.21	0.123	1.84	0.305	2.04	0.92	0.586	0.219	1.27	0.615	
10/11/2013 12:29	0913-111-A	13_10_11_1229_27_024	1	1.72	0.833	2.20	0.125	1.91	0.301	2.04	0.94	0.796	0.225	1.27	0.615	
10/11/2013 12:30	0913-111-A	13_10_11_1230_27_370	1	1.72	0.811	2.19	0.123	1.86	0.294	2.04	0.95	0.577	0.219	1.27	0.607	
10/11/2013 12:31	0913-111-A	13_10_11_1232_38_340	1	1.72	0.820	1.94	0.123	1.73	0.286	2.04	0.95	0.654	0.220	1.27	0.605	
10/11/2013 12:33	0913-111-A	13_10_11_1233_39_140	1	1.72	0.818	2.02	0.123	1.81	0.293	2.04	0.97	0.516	0.217	1.27	0.602	
10/11/2013 12:34	0913-111-A	13_10_11_1234_39_730	1	1.72	0.839	2.14	0.123	1.84	0.300	2.04	0.94	0.607	0.224	1.27	0.617	
10/11/2013 12:35	0913-111-A	13_10_11_1235_40_510	1	1.72	0.851	2.37	0.122	1.82	0.305	2.04	0.93	0.635	0.223	1.27	0.627	
10/11/2013 12:36	0913-111-A	13_10_11_1236_41_230	1	1.72	0.826	2.68	0.124	2.06	0.312	2.04	0.92	0.648	0.226	1.27	0.606	
Average Conc. (ppm):				1	1.72	0.812	1.78	0.120	1.59	0.287	2.04	0.99	0.505	0.213	1.27	0.598

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	VO.62 13.10.18.12.58

Pellet Cooler 2 Run 1

Date	Method	Filename	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/11/2013 13:44	0913-111, A	13, 10, 11, 1344, 00_484	1	1.00	0.514	1.46	0.0740	0.972	0.0810	1.08	0.54	0.246	0.127	1.07	0.386
10/11/2013 13:45	0913-111, A	13, 10, 11, 1345, 01_204	1	1.21	0.477	1.41	0.0700	0.939	0.0810	1.08	0.53	0.246	0.126	1.10	0.362
10/11/2013 13:46	0913-111, A	13, 10, 11, 1346, 02_004	1	1.38	0.509	1.09	0.0710	0.876	0.0810	1.09	0.53	0.246	0.124	1.10	0.384
10/11/2013 13:47	0913-111, A	13, 10, 11, 1347, 02_754	1	1.00	0.492	1.15	0.0710	0.801	0.0790	1.08	0.53	0.246	0.122	0.812	0.367
10/11/2013 13:48	0913-111, A	13, 10, 11, 1348, 03_454	1	1.39	0.518	1.03	0.0690	0.829	0.0820	1.08	0.53	0.246	0.123	0.745	0.381
10/11/2013 13:49	0913-111, A	13, 10, 11, 1349, 04_244	1	1.06	0.453	1.02	0.0690	0.798	0.0790	1.08	0.54	0.246	0.117	0.878	0.338
10/11/2013 13:50	0913-111, A	13, 10, 11, 1350, 05_064	1	1.47	0.480	1.00	0.0700	0.818	0.0820	1.08	0.54	0.246	0.119	0.745	0.355
10/11/2013 13:51	0913-111, A	13, 10, 11, 1351, 05_795	1	1.69	0.503	1.05	0.0750	0.826	0.0830	1.08	0.54	0.246	0.126	0.745	0.381
10/11/2013 13:52	0913-111, A	13, 10, 11, 1352, 06_545	1	2.23	0.464	0.964	0.0750	0.730	0.0800	1.08	0.53	0.246	0.124	1.12	0.353
10/11/2013 13:53	0913-111, A	13, 10, 11, 1353, 07_335	1	1.00	0.521	1.10	0.0740	0.859	0.0800	1.08	0.53	0.246	0.128	0.819	0.386
10/11/2013 13:54	0913-111, A	13, 10, 11, 1354, 08_045	1	1.00	0.498	1.02	0.0680	0.823	0.0830	1.08	0.54	0.246	0.121	0.884	0.368
10/11/2013 13:55	0913-111, A	13, 10, 11, 1355, 08_815	1	2.04	0.513	1.06	0.0750	0.829	0.0800	1.08	0.54	0.246	0.128	0.937	0.392
10/11/2013 13:56	0913-111, A	13, 10, 11, 1356, 09_515	1	1.85	0.514	1.06	0.0750	0.861	0.0800	1.08	0.53	0.246	0.127	0.874	0.384
10/11/2013 13:57	0913-111, A	13, 10, 11, 1357, 10_335	1	1.12	0.488	1.15	0.0660	0.904	0.0840	1.08	0.54	0.246	0.116	0.784	0.360
10/11/2013 13:58	0913-111, A	13, 10, 11, 1358, 11_105	1	1.00	0.487	1.12	0.0700	0.817	0.0820	1.08	0.54	0.246	0.122	1.02	0.360
10/11/2013 13:59	0913-111, A	13, 10, 11, 1359, 11_825	1	1.00	0.480	1.11	0.0730	0.851	0.0830	1.08	0.53	0.246	0.124	1.23	0.358
10/11/2013 14:00	0913-111, A	13, 10, 11, 1400, 12_475	1	1.18	0.488	1.01	0.0700	0.854	0.0830	1.08	0.54	0.246	0.124	1.19	0.363
10/11/2013 14:01	0913-111, A	13, 10, 11, 1401, 13_185	1	1.00	0.514	1.08	0.0720	0.822	0.0770	1.08	0.53	0.246	0.124	0.745	0.381
10/11/2013 14:02	0913-111, A	13, 10, 11, 1402, 13_945	1	1.42	0.493	1.05	0.0730	0.833	0.0800	1.08	0.53	0.246	0.122	0.862	0.368
10/11/2013 14:03	0913-111, A	13, 10, 11, 1403, 14_706	1	1.36	0.505	1.03	0.0690	0.804	0.0790	1.08	0.53	0.246	0.122	0.745	0.377
10/11/2013 14:04	0913-111, A	13, 10, 11, 1404, 15_456	1	1.18	0.484	1.18	0.0690	0.787	0.0810	1.08	0.54	0.246	0.124	0.869	0.366
10/11/2013 14:05	0913-111, A	13, 10, 11, 1405, 16_186	1	1.00	0.489	1.11	0.0680	0.832	0.0810	1.08	0.54	0.246	0.121	0.745	0.368
10/11/2013 14:06	0913-111, A	13, 10, 11, 1406, 16_946	1	1.11	0.527	1.01	0.0670	0.828	0.0800	1.08	0.54	0.246	0.124	0.765	0.390
10/11/2013 14:07	0913-111, A	13, 10, 11, 1407, 17_746	1	1.00	0.486	1.11	0.0690	0.796	0.0810	1.08	0.53	0.246	0.121	0.917	0.371
10/11/2013 14:08	0913-111, A	13, 10, 11, 1408, 18_506	1	1.28	0.491	1.10	0.0700	0.797	0.0790	1.08	0.53	0.246	0.122	0.875	0.365
10/11/2013 14:09	0913-111, A	13, 10, 11, 1409, 19_206	1	1.00	0.486	1.06	0.0710	0.804	0.0790	1.08	0.53	0.246	0.123	0.745	0.368
10/11/2013 14:10	0913-111, A	13, 10, 11, 1410, 20_016	1	1.06	0.496	1.05	0.0680	0.853	0.0790	1.08	0.53	0.246	0.122	1.05	0.377
10/11/2013 14:11	0913-111, A	13, 10, 11, 1411, 20_696	1	1.24	0.504	1.04	0.0710	0.818	0.0790	1.08	0.53	0.246	0.125	1.25	0.376
10/11/2013 14:12	0913-111, A	13, 10, 11, 1412, 21_506	1	1.11	0.489	1.10	0.0680	0.905	0.0770	1.08	0.53	0.246	0.123	1.06	0.363
10/11/2013 14:13	0913-111, A	13, 10, 11, 1413, 22_276	1	1.23	0.489	1.06	0.0720	0.778	0.0790	1.08	0.53	0.246	0.124	0.959	0.367
10/11/2013 14:14	0913-111, A	13, 10, 11, 1414, 22_977	1	1.14	0.476	1.17	0.0730	0.810	0.0810	1.08	0.54	0.246	0.123	0.745	0.361
10/11/2013 14:15	0913-111, A	13, 10, 11, 1415, 23_697	1	1.13	0.488	0.926	0.0730	0.808	0.0800	1.08	0.54	0.246	0.125	0.745	0.367
10/11/2013 14:16	0913-111, A	13, 10, 11, 1416, 24_517	1	1.50	0.503	1.06	0.0710	0.831	0.0830	1.08	0.54	0.246	0.127	0.947	0.370
10/11/2013 14:17	0913-111, A	13, 10, 11, 1417, 25_267	1	1.00	0.504	1.14	0.0700	0.791	0.0790	1.08	0.54	0.246	0.122	0.887	0.371
10/11/2013 14:18	0913-111, A	13, 10, 11, 1418, 25_987	1	1.27	0.515	1.15	0.0710	0.820	0.0810	1.08	0.54	0.246	0.125	0.745	0.380
10/11/2013 14:19	0913-111, A	13, 10, 11, 1419, 26_687	1	1.72	0.503	1.07	0.0700	0.766	0.0810	1.08	0.54	0.246	0.125	0.745	0.371
10/11/2013 14:20	0913-111, A	13, 10, 11, 1420, 27_457	1	1.45	0.468	1.11	0.0720	0.824	0.0820	1.08	0.54	0.246	0.125	1.13	0.350
10/11/2013 14:21	0913-111, A	13, 10, 11, 1421, 28_207	1	1.09	0.495	1.04	0.0710	0.744	0.0800	1.08	0.54	0.246	0.124	0.745	0.363
10/11/2013 14:22	0913-111, A	13, 10, 11, 1422, 28_967	1	1.40	0.499	1.09	0.0710	0.679	0.0840	1.08	0.54	0.252	0.128	0.745	0.369
10/11/2013 14:23	0913-111, A	13, 10, 11, 1423, 29_697	1	1.80	0.513	1.12	0.0710	0.798	0.0820	1.08	0.54	0.246	0.125	0.905	0.382
10/11/2013 14:24	0913-111, A	13, 10, 11, 1424, 30_467	1	1.46	0.492	1.11	0.0700	0.785	0.0820	1.08	0.54	0.246	0.124	0.928	0.369
10/11/2013 14:25	0913-111, A	13, 10, 11, 1425, 31_177	1	1.00	0.488	1.09	0.0680	0.824	0.0830	1.08	0.54	0.246	0.124	0.901	0.361
10/11/2013 14:26	0913-111, A	13, 10, 11, 1426, 31_988	1	1.62	0.517	1.12	0.0740	0.781	0.0820	1.08	0.54	0.246	0.129	0.946	0.380
10/11/2013 14:27	0913-111, A	13, 10, 11, 1427, 32_717	1	1.00	0.462	1.07	0.0700	0.751	0.0820	1.08	0.54	0.246	0.128	0.745	0.374
10/11/2013 14:28	0913-111, A	13, 10, 11, 1428, 33_468	1	1.94	0.493	1.07	0.0700	0.752	0.0810	1.08	0.54	0.246	0.128	0.745	0.366
10/11/2013 14:29	0913-111, A	13, 10, 11, 1429, 34_178	1	1.00	0.513	1.02	0.0720	0.778	0.0840	1.08	0.54	0.246	0.127	0.745	0.380
10/11/2013 14:30	0913-111, A	13, 10, 11, 1430, 35_028	1	1.00	0.518	0.998	0.0750	0.794	0.0830	1.08	0.54	0.246	0.129	0.996	0.380
10/11/2013 14:31	0913-111, A	13, 10, 11, 1431, 36_267	1	1.56	0.487	1.04	0.0740	0.788	0.0830	1.08	0.54	0.246	0.128	0.745	0.376
10/11/2013 14:32	0913-111, A	13, 10, 11, 1432, 36_498	1	1.19	0.506	1.04	0.0730	0.760	0.0820	1.08	0.54	0.246	0.128	0.745	0.379
10/11/2013 14:33	0913-111, A	13, 10, 11, 1433, 37_208	1	1.00	0.487	1.06	0.0730	0.774	0.0830	1.08	0.54	0.246	0.127	0.760	0.368
10/11/2013 14:34	0913-111, A	13, 10, 11, 1434, 37_918	1	1.06	0.496	1.14	0.0700	0.750	0.0830	1.08	0.54	0.246	0.126	0.788	0.374
10/11/2013 14:35	0913-111, A	13, 10, 11, 1435, 38_748	1	1.00	0.467	1.06	0.0670	0.796	0.0840	1.08	0.55	0.246	0.122	0.745	0.349
10/11/2013 14:36	0913-111, A	13, 10, 11, 1436, 39_488	1	1.43	0.483	1.08	0.0690	0.736	0.0840	1.08	0.55	0.246	0.124	0.780	0.360
10/11/2013 14:37	0913-111, A	13, 10, 11, 1437, 40_168	1	1.85	0.508	1.00	0.0730	0.722	0.0850	1.08	0.55	0.246	0.128	0.745	0.374
10/11/2013 14:38	0913-111, A	13, 10, 11, 1438, 40_969	1	1.55	0.494	0.950	0.0740	0.789	0.0840	1.08	0.55	0.246	0.128	0.784	0.372
10/11/2013 14:39	0913-111, A	13, 10, 11, 1439, 41_669	1	1.00	0.513	1.05	0.0750	0.750	0.0860	1.08	0.55	0.246	0.131	0.745	0.379
10/11/2013 14:40	0913-111, A	13, 10, 11, 1440, 42_449	1	1.56	0.487	1.12	0.0720	0.710	0.0870	1.08	0.55	0.246	0.128	0.745	0.382
10/11/2013 14:41	0913-111, A	13, 10, 11, 1441, 43_159	1	1.17	0.522	1.12	0.0730	0.768	0.0860	1.08	0.55	0.246	0.132	0.745	0.386
10/11/2013 14:42	0913-111, A	13, 10, 11, 1442, 43_779	1	1.00	0.517	0.993	0.0710	0.760	0.0860	1.08	0.55	0.246	0.127	0.745	0.381
10/11/2013 14:43	0913-111, A	13, 10, 11, 1443, 44_609	1	1.44	0.475	0.493	0.068								

Pellet Cooler 2 Run 2

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	VO.62 13.10.18.12.58

Pellet Cooler 2 Run 3

Date	Method	Filename	DF	Acroline (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/11/2013 16:29	0913-111	A 13.10.11.1629.02.222	1	1.41	0.500	1.27	0.0750	0.793	0.0840	1.08	0.55	0.246	0.125	0.989	0.379	
10/11/2013 16:30	0913-111	A 13.10.11.1630.02.872	1	1.08	0.520	1.12	0.0740	0.741	0.0840	1.08	0.55	0.246	0.125	0.787	0.385	
10/11/2013 16:31	0913-111	A 13.10.11.1631.03.632	1	1.13	0.505	0.925	0.0710	0.715	0.0850	1.08	0.55	0.246	0.119	1.25	0.372	
10/11/2013 16:32	0913-111	A 13.10.11.1632.04.442	1	1.00	0.521	1.10	0.0720	0.688	0.0820	1.08	0.55	0.246	0.123	1.18	0.385	
10/11/2013 16:33	0913-111	A 13.10.11.1633.05.202	1	1.11	0.507	1.07	0.0730	0.780	0.0840	1.08	0.55	0.246	0.118	0.745	0.384	
10/11/2013 16:34	0913-111	A 13.10.11.1634.05.962	1	1.25	0.512	1.11	0.0690	0.837	0.0870	1.08	0.55	0.246	0.117	1.02	0.379	
10/11/2013 16:35	0913-111	A 13.10.11.1635.06.772	1	1.27	0.525	1.12	0.0730	0.837	0.0860	1.08	0.55	0.246	0.125	0.991	0.388	
10/11/2013 16:36	0913-111	A 13.10.11.1636.07.512	1	1.00	0.524	1.20	0.0760	0.931	0.0840	1.08	0.55	0.246	0.124	0.745	0.395	
10/11/2013 16:37	0913-111	A 13.10.11.1637.08.223	1	1.00	0.528	1.19	0.0760	0.867	0.0880	1.08	0.56	0.246	0.127	0.745	0.393	
10/11/2013 16:38	0913-111	A 13.10.11.1638.08.953	1	1.67	0.504	1.20	0.0780	0.906	0.0860	1.08	0.56	0.246	0.129	1.16	0.377	
10/11/2013 16:39	0913-111	A 13.10.11.1639.09.743	1	1.00	0.532	1.28	0.0740	0.932	0.0870	1.08	0.56	0.246	0.125	0.745	0.390	
10/11/2013 16:40	0913-111	A 13.10.11.1640.10.493	1	1.00	0.536	1.34	0.0770	0.956	0.0870	1.08	0.56	0.246	0.129	0.745	0.394	
10/11/2013 16:41	0913-111	A 13.10.11.1641.11.243	1	1.10	0.505	1.31	0.0720	0.940	0.0880	1.08	0.56	0.246	0.122	0.745	0.372	
10/11/2013 16:42	0913-111	A 13.10.11.1642.12.003	1	1.05	0.482	1.31	0.0690	0.921	0.0880	1.08	0.56	0.246	0.121	0.922	0.362	
10/11/2013 16:43	0913-111	A 13.10.11.1643.12.743	1	1.49	0.519	1.42	0.0730	0.948	0.0870	1.08	0.56	0.246	0.129	0.746	0.387	
10/11/2013 16:44	0913-111	A 13.10.11.1644.13.493	1	1.52	0.519	1.30	0.0740	0.951	0.0850	1.08	0.56	0.246	0.129	0.745	0.388	
10/11/2013 16:45	0913-111	A 13.10.11.1645.14.293	1	2.25	0.539	3.47	0.0800	1.675	0.0870	1.49	0.57	1.49	0.143	0.745	0.403	
10/11/2013 16:46	0913-111	A 13.10.11.1646.15.003	1	2.60	0.502	3.49	0.0810	1.271	0.0870	1.14	0.56	1.16	0.139	0.745	0.372	
10/11/2013 16:47	0913-111	A 13.10.11.1647.15.783	1	2.07	0.525	2.98	0.0800	1.030	0.0880	1.08	0.56	0.670	0.136	0.745	0.390	
10/11/2013 16:48	0913-111	A 13.10.11.1648.16.503	1	1.17	0.504	2.40	0.0760	0.875	0.0860	1.08	0.56	0.621	0.131	0.745	0.371	
10/11/2013 16:49	0913-111	A 13.10.11.1649.17.254	1	1.44	0.509	2.21	0.0760	0.739	0.0830	1.08	0.55	0.485	0.129	0.745	0.378	
10/11/2013 16:50	0913-111	A 13.10.11.1650.17.954	1	1.22	0.521	2.09	0.0720	0.746	0.0850	1.08	0.56	0.404	0.124	0.745	0.384	
10/11/2013 16:51	0913-111	A 13.10.11.1651.18.704	1	1.05	0.503	2.16	0.0770	0.833	0.0860	1.08	0.56	0.347	0.125	0.745	0.379	
10/11/2013 16:52	0913-111	A 13.10.11.1652.19.514	1	1.67	0.515	2.13	0.0750	0.842	0.0880	1.08	0.56	0.424	0.125	0.745	0.389	
10/11/2013 16:53	0913-111	A 13.10.11.1653.20.254	1	1.18	0.528	2.14	0.0770	0.888	0.0860	1.08	0.56	0.259	0.129	0.745	0.385	
10/11/2013 16:54	0913-111	A 13.10.11.1654.20.974	1	1.00	0.496	2.22	0.0780	0.804	0.0840	1.08	0.56	0.309	0.126	0.745	0.380	
10/11/2013 16:55	0913-111	A 13.10.11.1655.21.734	1	1.00	0.521	2.23	0.0750	0.784	0.0880	1.08	0.56	0.338	0.127	0.745	0.390	
10/11/2013 16:56	0913-111	A 13.10.11.1656.22.484	1	1.79	0.517	2.23	0.0730	0.820	0.0840	1.08	0.55	0.618	0.128	0.745	0.385	
10/11/2013 16:57	0913-111	A 13.10.11.1657.23.244	1	1.00	0.521	2.01	0.0750	0.967	0.0830	1.08	0.55	0.447	0.127	0.745	0.382	
10/11/2013 16:58	0913-111	A 13.10.11.1658.24.014	1	1.43	0.494	2.09	0.0720	0.753	0.0840	1.08	0.55	0.384	0.125	0.745	0.376	
10/11/2013 16:59	0913-111	A 13.10.11.1659.24.714	1	1.44	0.527	2.01	0.0720	0.783	0.0840	1.08	0.55	0.434	0.127	0.745	0.388	
10/11/2013 17:00	0913-111	A 13.10.11.1700.25.504	1	1.00	0.521	2.05	0.0760	0.806	0.0840	1.08	0.55	0.460	0.128	0.745	0.393	
10/11/2013 17:01	0913-111	A 13.10.11.1701.26.275	1	1.46	0.530	1.98	0.0740	0.722	0.0830	1.08	0.55	0.463	0.125	0.745	0.392	
10/11/2013 17:02	0913-111	A 13.10.11.1702.27.015	1	0.92	0.496	1.94	0.0690	0.790	0.0840	1.08	0.55	0.344	0.120	0.745	0.371	
10/11/2013 17:03	0913-111	A 13.10.11.1703.27.725	1	1.50	0.504	1.90	0.0750	0.764	0.0850	1.08	0.55	0.268	0.126	0.745	0.375	
10/11/2013 17:04	0913-111	A 13.10.11.1704.28.495	1	1.37	0.488	1.78	0.0730	0.737	0.0850	1.08	0.55	0.380	0.122	0.745	0.364	
10/11/2013 17:05	0913-111	A 13.10.11.1705.29.235	1	1.64	0.497	1.88	0.0720	0.809	0.0820	1.08	0.55	0.246	0.121	0.745	0.364	
10/11/2013 17:06	0913-111	A 13.10.11.1706.30.015	1	1.24	0.491	1.92	0.0710	0.776	0.0820	1.08	0.55	0.313	0.119	0.761	0.370	
10/11/2013 17:07	0913-111	A 13.10.11.1707.30.725	1	1.00	0.524	1.92	0.0730	0.803	0.0840	1.08	0.55	0.323	0.120	0.745	0.390	
10/11/2013 17:08	0913-111	A 13.10.11.1708.31.445	1	1.00	0.502	1.92	0.0710	0.728	0.0830	1.08	0.55	0.391	0.116	0.745	0.376	
10/11/2013 17:09	0913-111	A 13.10.11.1709.32.195	1	2.23	0.512	1.90	0.0720	0.804	0.0800	1.08	0.55	0.386	0.122	0.745	0.381	
10/11/2013 17:10	0913-111	A 13.10.11.1710.33.005	1	1.31	0.486	1.97	0.0720	0.773	0.0840	1.08	0.54	0.413	0.120	0.745	0.367	
10/11/2013 17:11	0913-111	A 13.10.11.1711.33.755	1	1.00	0.506	1.88	0.0710	0.831	0.0820	1.08	0.55	0.424	0.119	0.745	0.376	
10/11/2013 17:12	0913-111	A 13.10.11.1712.34.465	1	1.00	0.505	1.96	0.0780	0.738	0.0840	1.08	0.55	0.330	0.123	0.862	0.386	
10/11/2013 17:13	0913-111	A 13.10.11.1713.35.276	1	1.00	0.500	2.00	0.0710	0.907	0.0810	1.08	0.55	0.293	0.123	0.745	0.379	
10/11/2013 17:14	0913-111	A 13.10.11.1714.35.986	1	1.38	0.473	1.83	0.0720	0.748	0.0840	1.08	0.55	0.246	0.121	0.745	0.353	
10/11/2013 17:15	0913-111	A 13.10.11.1715.36.786	1	1.31	0.511	1.91	0.0710	0.731	0.0840	1.08	0.55	0.343	0.121	0.745	0.374	
10/11/2013 17:16	0913-111	A 13.10.11.1716.37.496	1	1.00	0.489	1.88	0.0680	0.776	0.0800	1.08	0.55	0.246	0.122	0.745	0.359	
10/11/2013 17:17	0913-111	A 13.10.11.1717.38.286	1	1.29	0.469	1.87	0.0680	0.840	0.0850	1.08	0.55	0.323	0.121	0.745	0.349	
10/11/2013 17:18	0913-111	A 13.10.11.1718.38.976	1	1.51	0.474	1.78	0.0710	0.830	0.0820	1.08	0.55	0.246	0.123	0.745	0.351	
10/11/2013 17:19	0913-111	A 13.10.11.1719.39.786	1	1.22	0.511	1.79	0.0700	0.870	0.0840	1.08	0.55	0.285	0.120	0.745	0.378	
10/11/2013 17:20	0913-111	A 13.10.11.1720.40.566	1	1.17	0.487	1.92	0.0710	0.727	0.0820	1.08	0.55	0.291	0.120	0.745	0.369	
10/11/2013 17:21	0913-111	A 13.10.11.1721.41.276	1	1.00	0.507	1.97	0.0690	0.785	0.0820	1.08	0.55	0.257	0.119	0.745	0.379	
10/11/2013 17:22	0913-111	A 13.10.11.1722.41.986	1	1.00	0.519	1.95	0.0720	0.778	0.0810	1.08	0.54	0.246	0.127	0.745	0.381	
10/11/2013 17:23	0913-111	A 13.10.11.1723.42.806	1	1.00	0.487	1.85	0.0710	0.879	0.0840	1.08	0.54	0.326	0.122	0.745	0.367	
10/11/2013 17:24	0913-111	A 13.10.11.1724.43.527	1	1.00	0.492	1.96	0.0720	0.858	0.0840	1.08	0.55	0.246	0.123	0.745	0.367	
10/11/2013 17:25	0913-111	A 13.10.11.1725.44.267	1	1.00	0.500	1.93	0.0690	0.854	0.0840	1.08	0.55	0.403	0.125	0.745	0.376	
10/11/2013 17:26	0913-111	A 13.10.11.1726.44.997	1	2.21	0.497	2.04	0.0710	0.849	0.0830	1.08	0.55	0.283	0.124	0.745	0.375	
10/11/2013 17:27	0913-111	A 13.10.11.1727.45.747	1	1.92	0.492	1.89	0.0720	0.869	0.0830	1.08	0.55	0.246	0.121	0.745	0.367	
10/11/2013 17:28	0913-111	A 13.10.11.1728.46.477	1	1.20	0.490	1.80	0.0750	0.814	0.0820	1.08	0.55	0.246	0.122	0.787	0.367	
10/11/2013 17:29	0913-111	A 13.10.11.1729.47.307	1	1.25	0.504	1.95	0.0720	0.843	0.0820	1.08	0.55	0.302	0.124	0.745	0.380	
Average Conc. (ppm):				1	1.33	0.507	1.84	0.0732	0.844	0.0844	1.09	0.55	0.359	0.124	0.786	0.378

Hammermill 2 Run 1

Date	Method	Filename	DF	Acroline (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)</
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Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	VO.62 13.10.18.12.58

Hammermill 2 Run 2

Date	Method	Filename	DF	Acroline (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/11/2013 19:35	0913-111	A 13.10.11.1935_01_714	1	1.03	0.455	0.387	0.0660	0.165	0.0760	1.08	0.52	0.232	0.107	0.707	0.335
10/11/2013 19:36	0913-111	A 13.10.11.1936_02_534	1	0.965	0.465	0.476	0.0620	0.184	0.0770	1.08	0.52	0.232	0.104	0.707	0.343
10/11/2013 19:37	0913-111	A 13.10.11.1937_03_254	1	0.965	0.466	0.584	0.0660	0.165	0.0770	1.08	0.52	0.232	0.107	0.707	0.343
10/11/2013 19:38	0913-111	A 13.10.11.1938_03_964	1	0.965	0.470	0.688	0.0660	0.165	0.0800	1.08	0.53	0.232	0.110	0.707	0.348
10/11/2013 19:39	0913-111	A 13.10.11.1939_04_744	1	0.965	0.468	0.608	0.0660	0.203	0.0810	1.08	0.53	0.232	0.108	0.731	0.346
10/11/2013 19:40	0913-111	A 13.10.11.1940_05_514	1	0.965	0.483	0.569	0.0660	0.165	0.0800	1.08	0.54	0.232	0.109	0.707	0.360
10/11/2013 19:41	0913-111	A 13.10.11.1941_06_114	1	0.965	0.470	0.705	0.0620	0.168	0.0850	1.08	0.55	0.232	0.105	0.707	0.343
10/11/2013 19:42	0913-111	A 13.10.11.1942_06_924	1	0.965	0.504	0.659	0.0670	0.169	0.0830	1.08	0.55	0.232	0.114	0.707	0.369
10/11/2013 19:43	0913-111	A 13.10.11.1943_07_674	1	0.965	0.502	0.739	0.0700	0.180	0.0860	1.08	0.55	0.232	0.117	0.707	0.369
10/11/2013 19:44	0913-111	A 13.10.11.1944_08_385	1	0.965	0.467	0.816	0.0680	0.184	0.0850	1.08	0.55	0.232	0.114	0.707	0.355
10/11/2013 19:45	0913-111	A 13.10.11.1945_09_195	1	0.965	0.496	0.955	0.0730	0.189	0.0880	1.08	0.56	0.232	0.123	0.707	0.366
10/11/2013 19:46	0913-111	A 13.10.11.1946_09_915	1	0.965	0.512	1.22	0.0740	0.178	0.0880	1.08	0.57	0.232	0.127	0.707	0.375
10/11/2013 19:47	0913-111	A 13.10.11.1947_10_665	1	0.965	0.505	1.29	0.0720	0.175	0.0860	1.08	0.56	0.232	0.122	0.707	0.372
10/11/2013 19:48	0913-111	A 13.10.11.1948_11_485	1	0.965	0.487	1.11	0.0670	0.165	0.0830	1.08	0.55	0.232	0.113	0.707	0.357
10/11/2013 19:49	0913-111	A 13.10.11.1949_12_195	1	0.965	0.492	1.06	0.0700	0.165	0.0840	1.08	0.55	0.292	0.114	0.707	0.359
10/11/2013 19:50	0913-111	A 13.10.11.1950_12_945	1	0.965	0.480	1.14	0.0660	0.165	0.0840	1.08	0.55	0.232	0.107	0.707	0.337
10/11/2013 19:51	0913-111	A 13.10.11.1951_13_755	1	0.965	0.462	1.17	0.0650	0.165	0.0830	1.08	0.55	0.271	0.106	0.707	0.339
10/11/2013 19:52	0913-111	A 13.10.11.1952_14_475	1	0.965	0.501	1.09	0.0680	0.165	0.0840	1.08	0.55	0.232	0.114	0.707	0.363
10/11/2013 19:53	0913-111	A 13.10.11.1953_15_195	1	0.965	0.453	0.918	0.0660	0.165	0.0820	1.08	0.55	0.238	0.109	0.707	0.338
10/11/2013 19:54	0913-111	A 13.10.11.1954_16_015	1	1.16	0.466	0.745	0.0620	0.165	0.0840	1.08	0.55	0.236	0.110	0.707	0.342
10/11/2013 19:55	0913-111	A 13.10.11.1955_16_735	1	0.965	0.464	0.645	0.0670	0.186	0.0830	1.08	0.55	0.274	0.109	0.707	0.352
10/11/2013 19:56	0913-111	A 13.10.11.1956_17_546	1	0.965	0.477	0.739	0.0700	0.167	0.0870	1.08	0.55	0.232	0.114	0.707	0.351
10/11/2013 19:57	0913-111	A 13.10.11.1957_18_266	1	0.965	0.484	0.834	0.0700	0.165	0.0830	1.08	0.55	0.232	0.114	0.707	0.355
10/11/2013 19:58	0913-111	A 13.10.11.1958_18_986	1	0.965	0.497	0.781	0.0660	0.197	0.0890	1.08	0.56	0.303	0.114	0.707	0.361
10/11/2013 19:59	0913-111	A 13.10.11.1959_19_796	1	0.965	0.495	0.968	0.0700	0.165	0.0870	1.08	0.56	0.232	0.116	0.707	0.364
10/11/2013 20:00	0913-111	A 13.10.11.2000_20_526	1	0.965	0.485	1.18	0.0670	0.235	0.0830	1.08	0.55	0.232	0.115	0.707	0.358
10/11/2013 20:01	0913-111	A 13.10.11.2001_21_306	1	0.965	0.486	0.996	0.0660	0.282	0.0820	1.08	0.55	0.232	0.114	0.707	0.365
10/11/2013 20:02	0913-111	A 13.10.11.2002_22_056	1	0.965	0.470	1.20	0.0710	0.297	0.0870	1.08	0.56	0.232	0.117	0.707	0.346
10/11/2013 20:03	0913-111	A 13.10.11.2003_22_766	1	0.965	0.503	1.15	0.0730	0.266	0.0870	1.08	0.56	0.232	0.120	0.707	0.362
10/11/2013 20:04	0913-111	A 13.10.11.2004_23_566	1	0.965	0.470	1.52	0.0720	0.287	0.0860	1.08	0.52	0.232	0.126	0.707	0.362
10/11/2013 20:05	0913-111	A 13.10.11.2005_24_316	1	0.965	0.499	1.31	0.0720	0.247	0.0900	1.08	0.56	0.232	0.121	0.707	0.366
10/11/2013 20:06	0913-111	A 13.10.11.2006_25_026	1	0.965	0.479	1.24	0.0670	0.289	0.0850	1.08	0.55	0.232	0.116	0.707	0.351
10/11/2013 20:07	0913-111	A 13.10.11.2007_25_847	1	0.965	0.471	1.50	0.0680	0.281	0.0840	1.08	0.55	0.290	0.113	0.707	0.340
10/11/2013 20:08	0913-111	A 13.10.11.2008_26_547	1	1.29	0.496	1.77	0.0700	0.381	0.0840	1.08	0.55	0.232	0.121	0.707	0.363
10/11/2013 20:09	0913-111	A 13.10.11.2009_27_247	1	0.965	0.479	1.60	0.0690	0.323	0.0850	1.08	0.56	0.232	0.117	0.707	0.348
10/11/2013 20:10	0913-111	A 13.10.11.2010_28_067	1	0.965	0.515	2.01	0.0720	0.308	0.0860	1.08	0.56	0.232	0.127	0.846	0.373
10/11/2013 20:11	0913-111	A 13.10.11.2011_28_787	1	0.965	0.467	2.07	0.0680	0.287	0.0880	1.08	0.55	0.383	0.118	0.707	0.342
10/11/2013 20:12	0913-111	A 13.10.11.2012_29_547	1	0.965	0.517	1.95	0.0710	0.254	0.0860	1.08	0.55	0.371	0.121	0.707	0.378
10/11/2013 20:13	0913-111	A 13.10.11.2013_30_317	1	0.965	0.479	1.47	0.0700	0.285	0.0860	1.08	0.55	0.232	0.119	0.707	0.352
10/11/2013 20:14	0913-111	A 13.10.11.2014_31_027	1	0.965	0.486	1.48	0.0700	0.165	0.0830	1.08	0.55	0.341	0.117	0.707	0.352
10/11/2013 20:15	0913-111	A 13.10.11.2015_31_827	1	0.965	0.502	1.42	0.0710	0.200	0.0840	1.08	0.55	0.232	0.117	0.707	0.366
10/11/2013 20:16	0913-111	A 13.10.11.2016_32_537	1	0.965	0.474	1.60	0.0660	0.218	0.0860	1.08	0.55	0.232	0.115	0.707	0.349
10/11/2013 20:17	0913-111	A 13.10.11.2017_33_357	1	0.965	0.473	1.54	0.0690	0.244	0.0860	1.08	0.56	0.232	0.120	0.707	0.345
10/11/2013 20:18	0913-111	A 13.10.11.2018_34_067	1	0.965	0.483	1.79	0.0720	0.207	0.0840	1.08	0.55	0.232	0.118	0.707	0.353
10/11/2013 20:19	0913-111	A 13.10.11.2019_34_828	1	0.965	0.441	1.32	0.0570	0.231	0.0810	1.08	0.54	0.232	0.103	0.707	0.319
10/11/2013 20:20	0913-111	A 13.10.11.2020_35_678	1	0.965	0.409	0.893	0.0620	0.237	0.0790	1.08	0.53	0.232	0.100	0.707	0.303
10/11/2013 20:21	0913-111	A 13.10.11.2021_36_418	1	0.965	0.433	0.987	0.0620	0.202	0.0750	1.08	0.53	0.232	0.103	0.707	0.318
10/11/2013 20:22	0913-111	A 13.10.11.2022_37_128	1	0.965	0.461	1.19	0.0620	0.227	0.0830	1.08	0.54	0.232	0.107	0.707	0.355
10/11/2013 20:23	0913-111	A 13.10.11.2023_37_728	1	0.965	0.479	1.36	0.0660	0.198	0.0870	1.08	0.56	0.232	0.119	0.707	0.351
10/11/2013 20:24	0913-111	A 13.10.11.2024_38_578	1	0.965	0.483	1.45	0.0680	0.184	0.0860	1.08	0.56	0.232	0.124	0.707	0.352
10/11/2013 20:25	0913-111	A 13.10.11.2025_39_308	1	0.965	0.491	1.36	0.0700	0.239	0.0850	1.08	0.56	0.232	0.121	0.707	0.360
10/11/2013 20:26	0913-111	A 13.10.11.2026_40_038	1	0.965	0.466	1.27	0.0680	0.182	0.0850	1.08	0.56	0.232	0.116	0.707	0.341
10/11/2013 20:27	0913-111	A 13.10.11.2027_40_768	1	0.965	0.484	1.15	0.0670	0.191	0.0860	1.08	0.55	0.232	0.115	0.707	0.356
10/11/2013 20:28	0913-111	A 13.10.11.2028_41_548	1	0.965	0.493	1.23	0.0660	0.243	0.0850	1.08	0.55	0.232	0.114	0.707	0.359
10/11/2013 20:29	0913-111	A 13.10.11.2029_42_348	1	0.965	0.477	0.973	0.0670	0.171	0.0860	1.08	0.55	0.232	0.113	0.707	0.350
10/11/2013 20:30	0913-111	A 13.10.11.2030_43_068	1	0.965	0.474	0.997	0.0660	0.165	0.0850	1.08	0.55	0.232	0.111	0.707	0.344
10/11/2013 20:31	0913-111	A 13.10.11.2031_43_869	1	0.965	0.485	0.903	0.0660	0.201	0.0840	1.08	0.55	0.232	0.114	0.707	0.354
10/11/2013 20:32	0913-111	A 13.10.11.2032_44_619	1	0.965	0.493	1.57	0.0710	0.253	0.0850	1.08	0.56	0.232	0.122	0.707	0.360
10/11/2013 20:33	0913-111	A 13.10.11.2033_45_359	1	0.965	0.463	1.44	0.0670	0.165	0.0840	1.08	0.55	0.232	0.111	0.707	0.342
10/11/2013 20:34	0913-111	A 13.10.11.2034_46_079	1	0.965	0.450	0.598	0.0670	0.165	0.0680	1.08	0.46	0.232	0.172	0.707	0.331
10/11/2013 20:35	0913-111	A 13.10.11.2035_46_799	1	0.965	0.515	0.136	0.100	0.							

Hammermill 2 Run 3

Date	Method
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Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	VO.62 13.10.18.12.58

Pellet Cooler 1 Run 1

Date	Method	Filename	DF	Acroline (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/12/2013 8:58	0913-111, A	13, 10, 12, 0858_54, 250	1	0.931	0.473	1.38	0.0630	0.373	0.0710	0.98	0.49	0.236	0.114	0.686	0.343
10/12/2013 8:59	0913-111, A	13, 10, 12, 0859_55, 060	1	0.931	0.451	1.43	0.0630	0.416	0.0730	0.98	0.49	0.297	0.113	0.686	0.332
10/12/2013 9:00	0913-111, A	13, 10, 12, 0900_55, 760	1	0.931	0.473	1.46	0.0650	0.440	0.0700	0.98	0.49	0.291	0.120	0.686	0.353
10/12/2013 9:01	0913-111, A	13, 10, 12, 0901_56, 540	1	0.931	0.443	1.56	0.0630	0.413	0.0710	0.98	0.49	0.337	0.114	0.686	0.327
10/12/2013 9:02	0913-111, A	13, 10, 12, 0902_57, 240	1	1.05	0.458	1.42	0.0670	0.487	0.0710	0.98	0.49	0.293	0.115	0.686	0.344
10/12/2013 9:03	0913-111, A	13, 10, 12, 0903_58, 000	1	0.931	0.447	1.38	0.0610	0.431	0.0700	0.98	0.49	0.236	0.109	0.686	0.328
10/12/2013 9:04	0913-111, A	13, 10, 12, 0904_58, 810	1	0.931	0.487	1.32	0.0660	0.495	0.0740	0.98	0.49	0.337	0.116	0.686	0.352
10/12/2013 9:05	0913-111, A	13, 10, 12, 0905_59, 520	1	1.20	0.480	1.26	0.0650	0.496	0.0700	0.98	0.49	0.236	0.116	0.686	0.351
10/12/2013 9:07	0913-111, A	13, 10, 12, 0907_00, 280	1	0.931	0.462	1.41	0.0670	0.543	0.0710	0.98	0.49	0.236	0.119	0.686	0.339
10/12/2013 9:08	0913-111, A	13, 10, 12, 0908_01, 061	1	0.931	0.477	1.50	0.0680	0.496	0.0700	0.98	0.50	0.340	0.116	0.686	0.352
10/12/2013 9:09	0913-111, A	13, 10, 12, 0909_01, 771	1	0.931	0.449	1.53	0.0590	0.483	0.0700	0.98	0.50	0.373	0.112	0.686	0.330
10/12/2013 9:10	0913-111, A	13, 10, 12, 0910_02, 601	1	0.931	0.449	1.50	0.0610	0.450	0.0720	0.98	0.50	0.236	0.114	0.686	0.320
10/12/2013 9:11	0913-111, A	13, 10, 12, 0911_03, 351	1	0.931	0.460	1.49	0.0630	0.502	0.0740	0.98	0.50	0.236	0.111	0.686	0.335
10/12/2013 9:12	0913-111, A	13, 10, 12, 0912_04, 061	1	0.931	0.461	1.45	0.0640	0.553	0.0740	0.98	0.50	0.236	0.115	0.686	0.337
10/12/2013 9:13	0913-111, A	13, 10, 12, 0913_04, 821	1	0.931	0.456	1.51	0.0650	0.543	0.0740	0.98	0.50	0.344	0.115	0.686	0.338
10/12/2013 9:14	0913-111, A	13, 10, 12, 0914_05, 631	1	1.19	0.466	1.48	0.0630	0.513	0.0750	0.98	0.50	0.306	0.115	0.686	0.344
10/12/2013 9:15	0913-111, A	13, 10, 12, 0915_06, 381	1	0.931	0.477	1.43	0.0640	0.522	0.0720	0.98	0.50	0.442	0.115	0.686	0.353
10/12/2013 9:16	0913-111, A	13, 10, 12, 0916_06, 991	1	0.931	0.459	1.47	0.0640	0.464	0.0710	0.98	0.50	0.425	0.114	0.686	0.337
10/12/2013 9:17	0913-111, A	13, 10, 12, 0917_07, 721	1	0.931	0.443	1.52	0.0700	0.624	0.0720	0.98	0.50	0.242	0.122	0.686	0.320
10/12/2013 9:18	0913-111, A	13, 10, 12, 0918_08, 531	1	0.931	0.470	1.47	0.0660	0.615	0.0720	0.98	0.51	0.257	0.117	0.686	0.345
10/12/2013 9:19	0913-111, A	13, 10, 12, 0919_09, 252	1	0.931	0.485	1.69	0.0640	0.591	0.0740	0.98	0.51	0.527	0.119	0.686	0.352
10/12/2013 9:20	0913-111, A	13, 10, 12, 0920_09, 962	1	0.931	0.473	1.50	0.0650	0.545	0.0740	0.98	0.51	0.342	0.122	0.686	0.343
10/12/2013 9:21	0913-111, A	13, 10, 12, 0921_10, 712	1	0.931	0.490	1.63	0.0620	0.634	0.0770	0.98	0.51	0.497	0.117	0.686	0.354
10/12/2013 9:22	0913-111, A	13, 10, 12, 0922_11, 562	1	0.931	0.487	1.54	0.0700	0.574	0.0750	0.98	0.51	0.356	0.123	0.686	0.368
10/12/2013 9:23	0913-111, A	13, 10, 12, 0923_12, 282	1	0.931	0.461	1.52	0.0610	0.620	0.0750	0.98	0.51	0.525	0.114	0.686	0.340
10/12/2013 9:24	0913-111, A	13, 10, 12, 0924_12, 982	1	1.31	0.472	1.51	0.0640	0.608	0.0730	0.98	0.51	0.505	0.120	0.686	0.344
10/12/2013 9:25	0913-111, A	13, 10, 12, 0925_13, 802	1	0.931	0.471	1.50	0.0670	0.601	0.0760	0.98	0.51	0.292	0.118	0.686	0.348
10/12/2013 9:26	0913-111, A	13, 10, 12, 0926_14, 512	1	1.14	0.468	1.44	0.0680	0.691	0.0760	0.98	0.51	0.291	0.121	0.686	0.340
10/12/2013 9:27	0913-111, A	13, 10, 12, 0927_15, 282	1	0.931	0.471	1.41	0.0640	0.516	0.0740	0.98	0.51	0.320	0.113	0.686	0.345
10/12/2013 9:28	0913-111, A	13, 10, 12, 0928_15, 992	1	0.931	0.457	1.51	0.0630	0.548	0.0750	0.98	0.51	0.326	0.117	0.686	0.333
10/12/2013 9:29	0913-111, A	13, 10, 12, 0929_16, 802	1	0.931	0.486	1.43	0.0660	0.505	0.0760	0.98	0.51	0.391	0.117	0.686	0.353
10/12/2013 9:30	0913-111, A	13, 10, 12, 0930_17, 552	1	0.931	0.475	1.50	0.0670	0.570	0.0750	0.98	0.51	0.236	0.122	0.686	0.355
10/12/2013 9:31	0913-111, A	13, 10, 12, 0931_18, 263	1	0.931	0.487	1.54	0.0660	0.600	0.0740	0.98	0.51	0.412	0.124	0.686	0.358
10/12/2013 9:32	0913-111, A	13, 10, 12, 0932_19, 013	1	0.931	0.471	1.39	0.0660	0.511	0.0750	0.98	0.51	0.348	0.124	0.686	0.351
10/12/2013 9:33	0913-111, A	13, 10, 12, 0933_19, 773	1	0.931	0.483	1.63	0.0650	0.620	0.0750	0.98	0.51	0.520	0.124	0.686	0.361
10/12/2013 9:34	0913-111, A	13, 10, 12, 0934_20, 553	1	0.931	0.465	1.51	0.0660	0.585	0.0770	0.98	0.52	0.476	0.123	0.686	0.340
10/12/2013 9:35	0913-111, A	13, 10, 12, 0935_21, 313	1	1.44	0.491	1.53	0.0690	0.690	0.0760	0.98	0.51	0.475	0.131	0.686	0.358
10/12/2013 9:36	0913-111, A	13, 10, 12, 0936_22, 033	1	1.06	0.466	1.49	0.0620	0.596	0.0800	0.98	0.51	0.642	0.122	0.686	0.342
10/12/2013 9:37	0913-111, A	13, 10, 12, 0937_22, 823	1	0.931	0.481	1.42	0.0670	0.561	0.0760	0.98	0.51	0.370	0.121	0.686	0.346
10/12/2013 9:38	0913-111, A	13, 10, 12, 0938_23, 533	1	0.931	0.478	1.39	0.0630	0.543	0.0780	0.99	0.51	0.519	0.118	0.686	0.346
10/12/2013 9:39	0913-111, A	13, 10, 12, 0939_24, 263	1	0.931	0.469	1.38	0.0640	0.609	0.0770	1.02	0.51	0.450	0.115	0.686	0.348
10/12/2013 9:40	0913-111, A	13, 10, 12, 0940_25, 023	1	1.13	0.476	1.39	0.0620	0.507	0.0740	1.03	0.51	0.558	0.118	0.686	0.346
10/12/2013 9:41	0913-111, A	13, 10, 12, 0941_25, 743	1	0.931	0.468	1.27	0.0630	0.612	0.0720	0.98	0.51	0.236	0.114	0.686	0.344
10/12/2013 9:42	0913-111, A	13, 10, 12, 0942_26, 543	1	0.931	0.475	1.37	0.0640	0.510	0.0760	0.98	0.51	0.480	0.118	0.686	0.351
10/12/2013 9:43	0913-111, A	13, 10, 12, 0943_27, 234	1	0.931	0.448	1.37	0.0660	0.502	0.0720	1.00	0.50	0.439	0.114	0.686	0.328
10/12/2013 9:44	0913-111, A	13, 10, 12, 0944_27, 984	1	0.931	0.464	1.48	0.0660	0.512	0.0710	0.98	0.51	0.486	0.118	0.686	0.343
10/12/2013 9:45	0913-111, A	13, 10, 12, 0945_28, 774	1	0.931	0.428	1.37	0.0610	0.502	0.0740	0.99	0.50	0.423	0.110	0.686	0.324
10/12/2013 9:46	0913-111, A	13, 10, 12, 0946_29, 534	1	0.931	0.487	1.30	0.0680	0.516	0.0730	1.05	0.51	0.351	0.121	0.686	0.337
10/12/2013 9:47	0913-111, A	13, 10, 12, 0947_30, 304	1	0.931	0.472	1.32	0.0640	0.497	0.0750	1.05	0.51	0.241	0.116	0.686	0.344
10/12/2013 9:48	0913-111, A	13, 10, 12, 0948_30, 974	1	1.12	0.487	1.27	0.0640	0.502	0.0750	1.03	0.51	0.405	0.117	0.686	0.359
10/12/2013 9:49	0913-111, A	13, 10, 12, 0949_31, 774	1	1.09	0.461	1.47	0.0600	0.528	0.0730	1.08	0.51	0.525	0.113	0.686	0.335
10/12/2013 9:50	0913-111, A	13, 10, 12, 0950_32, 484	1	0.931	0.453	1.26	0.0650	0.505	0.0750	1.06	0.51	0.348	0.117	0.686	0.329
10/12/2013 9:51	0913-111, A	13, 10, 12, 0951_33, 294	1	0.931	0.471	1.34	0.0680	0.571	0.0720	1.09	0.51	0.361	0.117	0.686	0.351
10/12/2013 9:52	0913-111, A	13, 10, 12, 0952_34, 074	1	1.20	0.470	1.30	0.0610	0.563	0.0730	1.09	0.51	0.402	0.120	0.686	0.346
10/12/2013 9:53	0913-111, A	13, 10, 12, 0953_34, 794	1	0.931	0.463	1.37	0.0630	0.527	0.0740	1.02	0.51	0.565	0.118	0.686	0.343
10/12/2013 9:54	0913-111, A	13, 10, 12, 0954_35, 514	1	0.931	0.477	1.37	0.0690	0.563	0.0720	1.03	0.51	0.236	0.123	0.686	0.352
10/12/2013 9:55	0913-111, A	13, 10, 12, 0955_36, 235	1	0.931	0.459	1.41	0.0630	0.538	0.0730	1.07	0.51	0.465	0.116	0.686	0.337
10/12/2013 9:56	0913-111, A	13, 10, 12, 0956_36, 955	1	0.931	0.446	1.33	0.0620	0.538	0.0760	1.09	0.51	0.573	0.115	0.686	0.328
10/12/2013 9:57	0913-111, A	13, 10, 12, 0957_37, 745	1	0.931	0.464	1.46	0.0640	0.523	0.0750	1.08	0.51	0.516	0.119	0.686	0.345
10/12/2013 9:58	0913-111, A	13, 10, 12, 0958_38, 355	1	0.931	0.450	1.36	0.0650	0.534							

Pellet Cooler 1 Run 2

Company	CJT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	VO.62 13.10.18.12.58

Pellet Cooler 1 Run 3

Date	Method	Filename	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/12/2013 11:41	0913-111, A	13, 10, 12, 1141, 54, 484	1	0.967	0.465	1.43	0.0640	0.316	0.0690	0.98	0.48	0.236	0.118	0.686	0.340	
10/12/2013 11:42	0913-111, A	13, 10, 12, 1142, 55, 194	1	0.931	0.471	1.18	0.0630	0.282	0.0710	0.98	0.48	0.236	0.114	0.905	0.345	
10/12/2013 11:43	0913-111, A	13, 10, 12, 1143, 56, 874	1	1.57	0.480	1.15	0.0600	0.327	0.0690	0.98	0.47	0.236	0.119	0.844	0.352	
10/12/2013 11:44	0913-111, A	13, 10, 12, 1144, 56, 674	1	1.69	0.446	1.19	0.0670	0.311	0.0700	0.98	0.48	0.236	0.120	0.686	0.329	
10/12/2013 11:45	0913-111, A	13, 10, 12, 1145, 57, 474	1	1.18	0.455	1.29	0.0630	0.402	0.0710	0.98	0.48	0.236	0.117	0.686	0.337	
10/12/2013 11:46	0913-111, A	13, 10, 12, 1146, 58, 174	1	1.31	0.467	1.15	0.0650	0.472	0.0720	0.98	0.48	0.236	0.119	0.686	0.348	
10/12/2013 11:47	0913-111, A	13, 10, 12, 1147, 58, 354	1	1.52	0.453	1.23	0.0630	0.368	0.0690	0.98	0.48	0.236	0.119	0.686	0.336	
10/12/2013 11:48	0913-111, A	13, 10, 12, 1148, 59, 814	1	1.10	0.447	1.38	0.0650	0.333	0.0710	0.98	0.48	0.236	0.118	0.686	0.333	
10/12/2013 11:50	0913-111, A	13, 10, 12, 1150, 00, 524	1	1.41	0.478	1.43	0.0620	0.400	0.0690	0.98	0.48	0.236	0.121	1.13	0.351	
10/12/2013 11:51	0913-111, A	13, 10, 12, 1151, 01, 374	1	1.64	0.467	1.33	0.0670	0.385	0.0670	0.98	0.48	0.236	0.118	0.686	0.347	
10/12/2013 11:52	0913-111, A	13, 10, 12, 1152, 02, 144	1	1.21	0.466	1.35	0.0650	0.361	0.0680	0.98	0.48	0.236	0.119	0.686	0.344	
10/12/2013 11:53	0913-111, A	13, 10, 12, 1153, 02, 904	1	1.13	0.475	1.40	0.0680	0.294	0.0700	0.98	0.48	0.236	0.127	0.686	0.353	
10/12/2013 11:54	0913-111, A	13, 10, 12, 1154, 03, 615	1	1.22	0.476	1.53	0.0680	0.449	0.0710	0.98	0.49	0.236	0.129	0.978	0.348	
10/12/2013 11:55	0913-111, A	13, 10, 12, 1155, 04, 415	1	1.43	0.472	1.51	0.0690	0.366	0.0730	0.98	0.48	0.236	0.126	0.686	0.341	
10/12/2013 11:56	0913-111, A	13, 10, 12, 1156, 05, 115	1	1.14	0.462	1.36	0.0670	0.419	0.0700	0.98	0.48	0.236	0.122	0.686	0.345	
10/12/2013 11:57	0913-111, A	13, 10, 12, 1157, 05, 325	1	0.932	0.444	1.41	0.0650	0.344	0.0700	0.98	0.48	0.236	0.119	0.686	0.330	
10/12/2013 11:58	0913-111, A	13, 10, 12, 1158, 06, 635	1	1.06	0.481	1.36	0.0620	0.274	0.0690	0.98	0.48	0.236	0.123	0.998	0.351	
10/12/2013 11:59	0913-111, A	13, 10, 12, 1159, 07, 345	1	0.931	0.461	1.32	0.0650	0.336	0.0690	0.98	0.48	0.236	0.126	0.857	0.343	
10/12/2013 12:00	0913-111, A	13, 10, 12, 1200, 08, 135	1	2.15	0.484	1.38	0.0680	0.316	0.0680	0.98	0.48	0.236	0.124	0.686	0.358	
10/12/2013 12:01	0913-111, A	13, 10, 12, 1201, 08, 905	1	1.29	0.452	1.45	0.0640	0.327	0.0730	0.98	0.48	0.236	0.118	0.686	0.335	
10/12/2013 12:02	0913-111, A	13, 10, 12, 1202, 09, 625	1	1.70	0.444	1.33	0.0660	0.304	0.0690	0.98	0.48	0.236	0.117	0.686	0.327	
10/12/2013 12:03	0913-111, A	13, 10, 12, 1203, 10, 385	1	1.24	0.434	1.22	0.0600	0.353	0.0680	0.98	0.48	0.236	0.114	0.686	0.323	
10/12/2013 12:04	0913-111, A	13, 10, 12, 1204, 11, 135	1	0.931	0.458	1.37	0.0650	0.304	0.0700	0.98	0.48	0.236	0.117	0.709	0.335	
10/12/2013 12:05	0913-111, A	13, 10, 12, 1205, 11, 785	1	2.02	0.471	1.33	0.0650	0.375	0.0710	0.98	0.48	0.236	0.123	1.10	0.345	
10/12/2013 12:06	0913-111, A	13, 10, 12, 1206, 12, 506	1	1.21	0.436	1.30	0.0620	0.389	0.0690	0.98	0.48	0.236	0.114	0.686	0.321	
10/12/2013 12:07	0913-111, A	13, 10, 12, 1207, 13, 246	1	0.931	0.485	1.44	0.0650	0.369	0.0680	0.98	0.48	0.236	0.118	0.686	0.354	
10/12/2013 12:08	0913-111, A	13, 10, 12, 1208, 13, 996	1	0.969	0.470	1.26	0.0680	0.316	0.0680	0.98	0.48	0.236	0.118	0.686	0.343	
10/12/2013 12:09	0913-111, A	13, 10, 12, 1209, 14, 766	1	1.21	0.447	1.21	0.0570	0.308	0.0680	0.98	0.48	0.236	0.114	0.780	0.331	
10/12/2013 12:10	0913-111, A	13, 10, 12, 1210, 15, 476	1	2.17	0.465	1.12	0.0630	0.315	0.0690	0.98	0.47	0.236	0.116	0.686	0.353	
10/12/2013 12:11	0913-111, A	13, 10, 12, 1211, 16, 216	1	1.08	0.471	1.15	0.0660	0.340	0.0670	0.98	0.47	0.236	0.115	0.686	0.350	
10/12/2013 12:12	0913-111, A	13, 10, 12, 1212, 16, 976	1	0.931	0.437	1.05	0.0620	0.356	0.0700	0.98	0.47	0.236	0.110	0.882	0.317	
10/12/2013 12:13	0913-111, A	13, 10, 12, 1213, 17, 736	1	0.931	0.447	1.12	0.0680	0.289	0.0670	0.98	0.47	0.236	0.116	0.874	0.331	
10/12/2013 12:14	0913-111, A	13, 10, 12, 1214, 18, 466	1	2.48	0.475	1.17	0.0660	0.253	0.0690	0.98	0.47	0.236	0.117	0.686	0.357	
10/12/2013 12:15	0913-111, A	13, 10, 12, 1215, 19, 276	1	1.74	0.455	1.13	0.0650	0.351	0.0670	0.98	0.47	0.236	0.116	0.686	0.334	
10/12/2013 12:16	0913-111, A	13, 10, 12, 1216, 19, 854	1	0.479	0.421	1.21	0.0700	0.294	0.0670	0.98	0.47	0.236	0.119	0.686	0.354	
10/12/2013 12:17	0913-111, A	13, 10, 12, 1217, 20, 746	1	1.29	0.468	1.19	0.0650	0.286	0.0700	0.98	0.48	0.236	0.118	1.06	0.349	
10/12/2013 12:18	0913-111, A	13, 10, 12, 1218, 21, 457	1	0.931	0.483	1.29	0.0630	0.375	0.0700	0.98	0.48	0.236	0.101	0.351	0.351	
10/12/2013 12:19	0913-111, A	13, 10, 12, 1219, 22, 227	1	1.31	0.491	1.24	0.0630	0.368	0.0670	0.98	0.47	0.236	0.116	0.686	0.363	
10/12/2013 12:20	0913-111, A	13, 10, 12, 1220, 23, 037	1	1.56	0.461	1.21	0.0650	0.408	0.0690	0.98	0.47	0.236	0.116	0.753	0.342	
10/12/2013 12:21	0913-111, A	13, 10, 12, 1221, 23, 767	1	0.931	0.478	1.32	0.0620	0.342	0.0670	0.98	0.47	0.236	0.114	0.775	0.350	
10/12/2013 12:22	0913-111, A	13, 10, 12, 1222, 24, 527	1	1.59	0.481	1.24	0.0680	0.333	0.0690	0.98	0.47	0.236	0.120	0.686	0.366	
10/12/2013 12:23	0913-111, A	13, 10, 12, 1223, 25, 227	1	0.931	0.477	1.07	0.0650	0.349	0.0650	0.98	0.47	0.236	0.119	0.743	0.346	
10/12/2013 12:24	0913-111, A	13, 10, 12, 1224, 25, 967	1	1.50	0.467	1.21	0.0630	0.453	0.0670	0.98	0.47	0.236	0.117	0.734	0.355	
10/12/2013 12:25	0913-111, A	13, 10, 12, 1225, 26, 397	1	1.09	0.456	1.23	0.0630	0.463	0.0690	0.98	0.47	0.236	0.116	0.686	0.341	
10/12/2013 12:26	0913-111, A	13, 10, 12, 1226, 27, 507	1	1.14	0.478	1.23	0.0680	0.390	0.0690	0.98	0.47	0.236	0.119	0.686	0.355	
10/12/2013 12:27	0913-111, A	13, 10, 12, 1227, 28, 287	1	1.80	0.477	1.11	0.0640	0.418	0.0680	0.98	0.47	0.236	0.116	0.759	0.350	
10/12/2013 12:28	0913-111, A	13, 10, 12, 1228, 29, 047	1	1.83	0.475	1.18	0.0650	0.456	0.0680	0.98	0.47	0.236	0.118	0.686	0.348	
10/12/2013 12:29	0913-111, A	13, 10, 12, 1229, 29, 767	1	1.30	0.474	1.20	0.0660	0.411	0.0690	0.98	0.47	0.236	0.115	0.790	0.350	
10/12/2013 12:30	0913-111, A	13, 10, 12, 1230, 30, 476	1	1.42	0.468	1.22	0.0640	0.308	0.0700	0.98	0.47	0.236	0.113	0.686	0.344	
10/12/2013 12:31	0913-111, A	13, 10, 12, 1231, 31, 268	1	1.20	0.471	1.20	0.0690	0.362	0.0680	0.98	0.47	0.236	0.119	0.765	0.355	
10/12/2013 12:32	0913-111, A	13, 10, 12, 1232, 31, 988	1	1.31	0.464	1.17	0.0620	0.328	0.0680	0.98	0.47	0.236	0.117	0.718	0.348	
10/12/2013 12:33	0913-111, A	13, 10, 12, 1233, 32, 748	1	1.21	0.464	1.26	0.0600	0.339	0.0680	0.98	0.47	0.236	0.113	0.686	0.338	
10/12/2013 12:34	0913-111, A	13, 10, 12, 1234, 33, 468	1	1.11	0.468	1.22	0.0670	0.327	0.0670	0.98	0.47	0.236	0.118	0.686	0.344	
10/12/2013 12:35	0913-111, A	13, 10, 12, 1235, 34, 248	1	1.26	0.462	1.22	0.0630	0.414	0.0700	0.98	0.47	0.236	0.117	1.07	0.344	
10/12/2013 12:36	0913-111, A	13, 10, 12, 1236, 35, 008	1	1.59	0.482	1.26	0.0650	0.370	0.0700	0.98	0.47	0.236	0.116	0.777	0.351	
10/12/2013 12:38	0913-111, A	13, 10, 12, 1238, 49, 630	1	2.01	0.489	1.29	0.0650	0.306	0.0660	0.98	0.47	0.236	0.118	0.686	0.366	
10/12/2013 12:39	0913-111, A	13, 10, 12, 1239, 50, 430	1	2.18	0.465	1.10	0.0620	0.347	0.0700	0.98	0.47	0.236	0.111	0.686	0.346	
10/12/2013 12:40	0913-111, A	13, 10, 12, 1240, 51, 220	1	0.931	0.461	1.18	0.0630	0.289	0.0680	0.98	0.47	0.236	0.116	0.686	0.345	
10/12/2013 12:41	0913-111, A	13, 10, 12, 1241, 51, 930	1	1.45	0.482	1.03	0.0670	0.350	0.0740	0.98	0.47	0.236	0.118	0.832	0.351	
Average Conc. (ppm):				1	1.35	0.467	1.26	0.0647	0.351	0.0690	0.98	0.48	0.236	0.118	0.759	0.345

Aspirator Run 1

Date	Method	Filename	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde
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Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	V0.62 13.10.18.12.58

Aspirator Run 2													
Date	Method	Filename	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)
10/12/2013 16:36	0913-111, A	13_10_12_1636_22_016	1	2.99	0.831	1.26	0.505	8.21	0.237	2.73	1.31	3.00	1.47
10/12/2013 16:37	0913-111, A	13_10_12_1637_22_786	1	3.74	0.820	1.54	0.511	8.34	0.282	2.73	1.64	3.00	1.45
10/12/2013 16:38	0913-111, A	13_10_12_1638_23_596	1	2.83	0.843	1.44	0.553	8.87	0.299	2.73	1.43	3.00	1.56
10/12/2013 16:39	0913-111, A	13_10_12_1639_24_356	1	3.46	0.860	1.49	0.557	8.84	0.303	2.73	1.50	3.00	1.57
10/12/2013 16:40	0913-111, A	13_10_12_1640_25_056	1	3.59	0.838	1.41	0.559	8.50	0.256	2.73	1.31	3.00	1.60
10/12/2013 16:41	0913-111, A	13_10_12_1641_25_866	1	3.44	0.843	1.29	0.538	8.45	0.250	2.73	1.31	3.00	1.55
10/12/2013 16:42	0913-111, A	13_10_12_1642_26_526	1	2.96	0.785	1.36	0.502	8.81	0.287	2.73	1.38	3.00	1.44
10/12/2013 16:43	0913-111, A	13_10_12_1643_27_336	1	2.73	0.787	1.45	0.494	8.65	0.270	2.73	1.81	3.00	1.38
10/12/2013 16:44	0913-111, A	13_10_12_1644_28_086	1	3.31	0.817	1.50	0.478	8.56	0.271	2.73	1.78	3.00	1.36
10/12/2013 16:45	0913-111, A	13_10_12_1645_28_826	1	2.82	0.785	1.69	0.469	8.67	0.272	2.73	1.69	3.00	1.35
10/12/2013 16:46	0913-111, A	13_10_12_1646_29_536	1	2.91	0.795	1.55	0.479	8.99	0.292	2.73	1.60	3.00	1.37
10/12/2013 16:47	0913-111, A	13_10_12_1647_30_356	1	3.94	0.795	1.64	0.471	8.91	0.265	2.73	1.54	3.00	1.34
10/12/2013 16:48	0913-111, A	13_10_12_1648_31_017	1	4.04	0.764	1.47	0.467	8.86	0.267	2.73	1.46	3.00	1.33
10/12/2013 16:49	0913-111, A	13_10_12_1649_31_837	1	2.86	0.770	1.43	0.465	8.94	0.262	2.73	1.47	3.00	1.30
10/12/2013 16:50	0913-111, A	13_10_12_1650_32_607	1	3.01	0.803	1.46	0.466	9.04	0.262	2.73	1.55	3.00	1.33
10/12/2013 16:51	0913-111, A	13_10_12_1651_33_377	1	2.63	0.782	1.61	0.458	8.96	0.250	2.73	2.12	3.00	1.31
10/12/2013 16:52	0913-111, A	13_10_12_1652_33_977	1	3.25	0.810	1.63	0.462	9.03	0.254	2.73	1.93	3.00	1.33
10/12/2013 16:53	0913-111, A	13_10_12_1653_34_767	1	3.79	0.798	1.59	0.468	9.20	0.266	2.73	1.83	3.00	1.33
10/12/2013 16:54	0913-111, A	13_10_12_1654_35_477	1	3.78	0.797	1.52	0.481	9.20	0.263	2.73	1.92	3.00	1.35
10/12/2013 16:55	0913-111, A	13_10_12_1655_36_207	1	3.31	0.775	1.67	0.458	8.96	0.254	2.73	1.82	3.00	1.30
10/12/2013 16:56	0913-111, A	13_10_12_1656_36_947	1	3.44	0.780	1.50	0.458	9.07	0.256	2.73	1.64	3.00	1.28
10/12/2013 16:57	0913-111, A	13_10_12_1657_37_757	1	3.00	0.766	1.39	0.447	9.14	0.261	2.73	1.42	3.00	1.20
10/12/2013 16:58	0913-111, A	13_10_12_1658_38_477	1	4.04	0.786	1.32	0.450	9.13	0.261	2.73	1.35	3.00	1.28
10/12/2013 16:59	0913-111, A	13_10_12_1659_39_217	1	3.22	0.792	1.32	0.441	9.08	0.270	2.73	1.28	3.00	1.28
10/12/2013 17:00	0913-111, A	13_10_12_1700_40_018	1	2.87	0.787	1.37	0.448	8.89	0.215	2.73	1.27	3.00	1.32
10/12/2013 17:01	0913-111, A	13_10_12_1701_40_728	1	2.87	0.851	1.47	0.451	9.13	0.273	2.73	1.49	3.00	1.29
10/12/2013 17:02	0913-111, A	13_10_12_1702_41_438	1	2.97	0.779	1.65	0.451	9.18	0.252	2.73	1.67	3.00	1.29
10/12/2013 17:03	0913-111, A	13_10_12_1703_42_208	1	3.09	0.814	1.71	0.459	9.05	0.257	2.73	1.69	3.00	1.31
10/12/2013 17:04	0913-111, A	13_10_12_1704_42_928	1	3.58	0.811	1.46	0.464	8.45	0.221	2.73	1.33	3.00	1.36
10/12/2013 17:05	0913-111, A	13_10_12_1705_43_758	1	2.95	0.817	1.54	0.471	8.13	0.268	2.73	1.37	3.00	1.35
10/12/2013 17:06	0913-111, A	13_10_12_1706_44_458	1	3.01	0.782	1.63	0.477	8.01	0.269	2.73	1.41	3.00	1.36
10/12/2013 17:07	0913-111, A	13_10_12_1707_45_208	1	3.91	0.800	1.57	0.489	8.57	0.230	2.73	1.46	3.00	1.40
10/12/2013 17:08	0913-111, A	13_10_12_1708_46_018	1	3.00	0.803	1.52	0.481	8.99	0.265	2.73	1.48	3.00	1.36
10/12/2013 17:09	0913-111, A	13_10_12_1709_46_738	1	2.61	0.787	1.66	0.461	8.09	0.257	2.73	1.73	3.00	1.33
10/12/2013 17:10	0913-111, A	13_10_12_1710_47_448	1	2.65	0.784	1.87	0.442	8.68	0.243	2.73	1.99	3.00	1.26
10/12/2013 17:11	0913-111, A	13_10_12_1711_48_248	1	3.22	0.776	1.67	0.441	9.04	0.255	2.73	1.67	3.00	1.27
10/12/2013 17:12	0913-111, A	13_10_12_1712_48_989	1	3.03	0.828	1.75	0.447	9.29	0.263	2.73	1.58	3.00	1.29
10/12/2013 17:13	0913-111, A	13_10_12_1713_49_799	1	3.28	0.802	1.76	0.455	9.21	0.259	2.73	1.50	3.00	1.30
10/12/2013 17:14	0913-111, A	13_10_12_1714_50_539	1	3.59	0.772	1.72	0.450	9.23	0.246	2.73	1.46	3.00	1.31
10/12/2013 17:15	0913-111, A	13_10_12_1715_51_279	1	2.99	0.794	1.68	0.464	8.99	0.265	2.73	1.47	3.00	1.33
10/12/2013 17:16	0913-111, A	13_10_12_1716_51_999	1	3.88	0.820	1.52	0.472	8.83	0.267	2.73	1.44	3.00	1.34
10/12/2013 17:17	0913-111, A	13_10_12_1717_52_749	1	2.71	0.839	1.78	0.480	8.84	0.270	2.73	1.59	3.00	1.38
10/12/2013 17:18	0913-111, A	13_10_12_1718_53_549	1	3.25	0.828	1.78	0.481	8.89	0.247	2.73	2.10	3.00	1.37
10/12/2013 17:19	0913-111, A	13_10_12_1719_54_259	1	2.95	0.804	1.62	0.455	8.94	0.241	2.73	2.41	3.00	1.28
10/12/2013 17:20	0913-111, A	13_10_12_1720_55_079	1	2.67	0.829	2.03	0.454	8.09	0.255	2.73	1.99	3.00	1.29
10/12/2013 17:21	0913-111, A	13_10_12_1721_55_909	1	2.49	0.800	1.80	0.427	9.19	0.257	2.73	1.60	3.00	1.26
10/12/2013 17:22	0913-111, A	13_10_12_1722_56_659	1	2.88	0.787	1.57	0.433	9.28	0.258	2.73	1.45	3.00	1.23
10/12/2013 17:23	0913-111, A	13_10_12_1723_57_409	1	2.15	0.763	1.68	0.417	9.16	0.251	2.73	1.38	3.00	1.21
10/12/2013 17:24	0913-111, A	13_10_12_1724_58_220	1	3.23	0.784	1.53	0.445	9.46	0.257	2.73	1.41	3.00	1.27
10/12/2013 17:25	0913-111, A	13_10_12_1725_58_940	1	2.76	0.795	1.71	0.444	9.36	0.251	2.73	1.54	3.00	1.27
10/12/2013 17:26	0913-111, A	13_10_12_1726_59_780	1	3.25	0.778	1.79	0.428	8.94	0.236	2.73	1.92	3.00	1.24
10/12/2013 17:27	0913-111, A	13_10_12_1728_00_500	1	2.96	0.759	2.03	0.414	8.98	0.225	2.73	2.41	3.00	1.18
10/12/2013 17:28	0913-111, A	13_10_12_1729_01_300	1	3.24	0.822	1.64	0.434	9.24	0.243	2.73	1.61	3.00	1.24
10/12/2013 17:30	0913-111, A	13_10_12_1730_02_020	1	1.92	0.796	1.45	0.447	9.16	0.257	2.73	1.30	3.00	1.30
10/12/2013 17:31	0913-111, A	13_10_12_1731_02_780	1	2.36	0.812	1.29	0.455	8.71	0.213	2.73	1.29	3.00	1.33
10/12/2013 17:32	0913-111, A	13_10_12_1732_03_490	1	3.07	0.798	1.43	0.462	9.13	0.259	2.73	1.44	3.00	1.32
10/12/2013 17:33	0913-111, A	13_10_12_1733_04_240	1	3.74	0.788	1.49	0.459	8.96	0.256	2.73	1.42	3.00	1.38
10/12/2013 17:34	0913-111, A	13_10_12_1734_04_920	1	3.29	0.835	1.53	0.457	8.92	0.254	2.73	1.62	3.00	1.31
10/12/2013 17:35	0913-111, A	13_10_12_1735_05_660	1	2.95	0.815	1.88	0.448	8.75	0.232	2.73	2.24	3.00	1.25
10/12/2013 17:36	0913-111, A	13_10_12_1736_06_381	1	3.24	1.19	1.05	0.523	6.25	0.181	2.73	1.31	3.00	2.17
Average Conc. (ppm):				1	3.12	0.808	1.58	0.467	8.90	0.256	2.73	1.60	3.00
												1.35	3.92
													0.602

Aspirator Run 3																
Date	Method	Filename	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/12/2013 18:00	0913-111, A	13_10_12_1800_36_741	1	2.53	0.845	1.05	0.520	7.94	0.225	2.73	1.17	3.00	1.48	3.73	0.627	
10/12/2013 18:01	0913-111, A	13_10_12_1801_37_551	1	2.85	0.859	1.05	0.504	8.15	0.224	2.73	1.03	3.00	1.45	3.61	0.631	
10/12/2013 18:02	0913-111, A	13_10_12_1802_38_261	1	2.74	0.806	1.05	0.500	8.25	0.222	2.73	1.04	3.00	1.43	3.76	0.598	
10/12/2013 18:03	0913-111, A	13_10_12_1803_39_032	1	2.31	0.839	1.05	0.516	8.47	0.221	2.73	1.11	3.00	1.46	3.64	0.618	
10/12/2013 18:04	0913-111, A	13_10_12_1804_39_742	1	2.64	0.821	1.05	0.499	8.29	0.262	2.73	1.57	3.00	1.40	3.74	0.610	
10/12/2013 18:05	0913-111, A	13_10_12_1805_40_552	1	2.05	0.846	1.21	0.471	8.30	0.236	2.73	2.36	3.00	1.34	3.76	0.628	
10/12/2013 18:06	0913-111, A	13_10_12_1806_41_282	1	2.63	0.847	1.05	0.536	8.46	0.232	2.73	1.01	3.00	1.51	3.55	0.626	
10/12/2013 18:07	0913-111, A	13_10_12_1807_42_072	1	3.16	0.853	1.05	0.552	8.43	0.238	2.73	0.90	3.00	1.55	4.14	0.630	
10/12/2013 18:08	0913-111, A	13_10_12_1808_42_782	1	2.65	0.877	1.05	0.577	8.27	0.240	2.73	0.95	3.00	1.60	3.68	0.647	
10/12/2013 18:09	0913-111, A	13_10_12_1809_43_546	1	2.55	0.869	1.05	0.546	8.16	0.237	2.73	1.55	3.00	1.54	3.27	0.645	
10/12/2013 18:10	0913-111, A	13_10_12_1810_44_292	1	2.46	0.890	1.05	0.566	8.77	0.242	2.73	1.34	3.00	1.59	3.72	0.666	
10/12/2013 18:11	0913-111, A	13_10_12_1811_45_102	1	1.83	0.903	1.05	0.549	8.25	0.281	2.73	1.42	3.00	1.53	3.76	0.668	
10/12/2013 18:12	0913-111, A	13_10_12_1812_45_862	1	2.76	0.873	1.05	0.547	7.68	0.232	2.73	1.36	3.00	1.52	3.90	0.652	
10/12/2013 18:13	0913-111, A	13_10_12_1813_46_573	1	2.04	0.862	1.05	0.553	8.26	0.236	2.73	1.55	3.00	1.56	3.27	0.648	
10/12/2013 18:14	0913-111, A	13_10_12_1814_47_372	1	2.76	0.910	1.05	0.553	8.24	0.282	2.73	1.52	3.00	1.55	2.82	0.677	
10/12/2013 18:15	0913-111, A	13_10_12_1815_48_083	1	1.70	0.868	1.44	0.552	7.88	0.255	2.73	2.54	3.00	1.54	3.04	0.649	
10/12/2013 18:16	0913-111, A	13_10_12_1816_48_803	1	2.64	0.918	1.05	0.588	8.24	0.296	2.73	1.41	3.00	1.62	4.29	0.681	
10/12/2013 18:17	0913-111, A	13_10_12_1817_49_463	1	1.70	0.860	1.05	0.573	8.29	0.287	2.73	1.94	3.00	1.54	3.18	0.686	
10/12/2013 18:18	0913-111, A	13_10_12_1818_50_243	1	2.71	0.916	1.05	0.674	7.79	0.259	2.73	1.09	3.00	1.80	4.82	0.678	
10/12/2013 18:19	0913-111, A	13_10_12_1819_51_043	1	1.85	0.962	1.05	0.693	7.90	0.272	2.73	1.05	3.00	1.85	4.30	0.712	
10/12/2013 18:20	0913-111, A	13_10_12_1820_51_843	1	3.36	0.965	1.05	0.714	8.11	0.274	2.73	1.04	3.00	1.91	4.45	0.719	
10/12/2013 18:21	0913-111, A	13_10_12_1821_51_513	1	1.07	0.927	1.01	0.717	8.10	0.277	2.73	1.12	3.00	1.88	3.76	0.743	
10/12/2013 18:22	0913-111, A	13_10_12_1822_53_283	1	2.04	0.910	1.05	0.645	8.00	0.265	2.73	1.29	3.00	1.82	4.52	0.744	
10/12/2013 18:23	0913-111, A	13_10_12_1823_54_043	1	2.09	0.916	1.05	0.608	7.83	0.256	2.73	1.27	3.00	1.72	4.06	0.788	
10/12/2013 18:24	0913-111, A	13_10_12_1824_54_743	1	2.62	0.898	1.05	0.579	7.90	0.245	2.73	1.33	3.00	1.65	4.14	0.673	
10/12/2013 18:25	0913-111, A	13_10_12_1825_55_553	1	1.90	0.978	1.05	0.628	7.93	0.248	2.73	1.29	3.00	1.62	4.03	0.733	
10/12/2013 18:26	0913-111, A	13_10_12_1826_56_303	1	2.17	0.922	1.05	0.576	7.83	0.245	2.73	1.25	3.00	1.63	3.72	0.688	
10/12/2013 18:27	0913-111, A	13_10_12_1827_57_024	1	1.83	0.913	1.05	0.573	7.82	0.243	2.73	1.26	3.00	1.60	3.01	0.677	
10/12/2013 18:28	0913-111, A	13_10_12_1828_57_854	1	3.23	0.912	1.05	0.570	7.82	0.243	2.73	1.30	3.00	1.61	3.48	0.679	
10/12/2013 18:29	0913-111, A	13_10_12_1829_58_599	1	1.91	0.910	1.05	0.570	7.82	0.245	2.73	1.27	3.00	1.60	3.56	0.681	
10/12/2013 18:30	0913-111, A	13_10_12_1830_59_364	1	1.92	0.905	1.05	0.573	7.88	0.243	2.73	1.32	3.00	1.60	3.62	0.673	
10/12/2013 18:32	0913-111, A	13_10_12_1832_00_094	1	1.97	0.945	1.05	0.583	8.01	0.251	2.73	1.32	3.00	1.63	3.59	0.694	
10/12/2013 18:33	0913-111, A	13_10_12_1833_00_814	1	3.01	0.930	1.05	0.578	7.86	0.249	2.73	1.41	3.00	1.63	3.82	0.699	
10/12/2013 18:35	0913-111, A	13_10_12_1834_01_607	1	0.95	0.955	1.05	0.585	8.07	0.259	2.73	1.39	3.00	1.62	3.22	0.708	
10/12/2013 18:36	0913-111, A	13_10_12_1835_02_364	1	2.65	0.950	1.05	0.600	8.30	0.302	2.73	1.38	3.00	1.67	3.73	0.702	
10/12/2013 18:37	0913-111, A	13_10_12_1836_03_104	1	1.70	0.956	1.05	0.601	8.38	0.301	2.73	1.45	3.00	1.68	4.20	0.710	
10/12/2013 18:38	0913-111, A	13_10_12_1837_03_864	1	2.73	0.935	1.05	0.600	8.50	0.303	2.73	1.37	3.00	1.67	3.97	0.697	
10/12/2013 18:39	0913-111, A	13_10_12_1838_04_589	1	1.92	0.921	1.05	0.585	8.55	0.295	2.73	1.35	3.00	1.65	3.54	0.692	
10/12/2013 18:39	0913-111, A	13_10_12_1839_05_385	1	1.80	0.918	1.05	0.551	8.72	0.286	2.73	1.33	3.00	1.54	3.24	0.688	
10/12/2013 18:40	0913-111, A	13_10_12_1840_06_145	1	2.24	0.887	1.05	0.554	8.13	0.250	2.73	1.37	3.00	1.58	3.52	0.666	
10/12/2013 18:41	0913-111, A	13_10_12_1841_06_875	1	1.90	0.927	1.05	0.567	8.01	0.251	2.73	1.35	3.00	1.59	3.09	0.689	
10/12/2013 18:42	0913-111, A	13_10_12_1842_07_650	1	2.22	0.909	1.05	0.569	8.29	0.286	2.73	1.37	3.00	1.53	3.87	0.674	
10/12/2013 18:43	0913-111, A	13_10_12_1843_08_395	1	2.19	0.902	1.05	0.559	7.89	0.250	2.73	1.33	3.00	1.59	3.13	0.672	
10/12/2013 18:44	0913-111, A	13_10_12_1844_09_185	1	1.77	0.920	1.05	0.557	7.77	0.250	2.73	1.36	3.00	1.58	3.91	0.683	
10/12/2013 18:45	0913-111, A	13_10_12_1845_09_885	1	2.01	0.897	1.05	0.573	8.09	0.287	2.73	1.34	3.00	1.58	3.49	0.670	
10/12/2013 18:46	0913-111, A	13_10_12_1846_10_684	1	2.54	0.940	1.05	0.584	8.16	0.285	2.73	1.36	3.00	1.59	3.65	0.685	
10/12/2013 18:47	0913-111, A	13_10_12_1847_11_395	1	2.64	0.940	1.05	0.601	7.76	0.260	2.73	1.39	3.00	1.70	4.17	0.700	
10/12/2013 18:48	0913-111, A	13_10_12_1848_12_195	1	2.89	0.949	1.05	0.611	8.32	0.314	2.73	1.40	3.00	1.73	3.15	0.707	
10/12/2013 18:49	0913-111, A	13_10_12_1849_12_955	1	2.48	0.966	1.05	0.629	8.53	0.319	2.73	1.59	3.00	1.74	3.57	0.725	
10/12/2013 18:50	0913-111, A	13_10_12_1850_13_715	1	1.01	0.923	1.05	0.628	8.78	0.318	2.73	1.52	3.00	1.73	3.42	0.742	
10/12/2013 18:51	0913-111, A	13_10_12_1851_14_456	1	1.70	0.951	1.05	0.616	8.50	0.315	2.73	1.50	3.00	1.73	3.98	0.707	
10/12/2013 18:52	0913-111, A	13_10_12_1852_15_206	1	2.31	0.977	1.05	0.623	8.60	0.317	2.73	1.52	3.00	1.76	3.99	0.729	
10/12/2013 18:53	0913-111, A	13_10_12_1853_15_926	1	1.76	0.971	1.05	0.621	8.65	0.321	2.73	1.46	3.00	1.73	3.82	0.741	
10/12/2013 18:54	0913-111, A	13_10_12_1854_16_748	1	0.99	0.971	1.05	0.618	8.54	0.315	2.73	1.51	3.00	1.74	3.76	0.74	
10/12/2013 18:55	0913-111, A	13_10_12_1855_17_456	1	1.83	0.925	1.05	0.585	7.89	0.284	2.73	1.34	3.00	1.67	3.95	0.687	
10/12/2013 18:56	0913-111, A	13_10_12_1856_18_246	1	1.70	0.915	1.05	0.558	7.68	0.260	2.73	1.32	3.00	1.56	3.37	0.688	
10/12/2013 18:57	0913-111, A	13_10_12_1857_19_986	1	1.71	0.924	1.05	0.577	8.80	0.306	2.73	1.42	3.00	1.60	4.13	0.692	
10/12/2013 18:58	0913-111, A	13_10_12_1858_19_739	1	0.94	0.933	1.05	0.599	8.83	0.313	2.73	1.42	3.00	1.65	3.86	0.697	
10/12/2013 18:59	0913-111, A	13_10_12_1859_20_336	1	1.70	0.920	1.05	0.567	9.14	0.251	2.73	1.28	3.00	1.62	4.06	0.684	
10/12/2013 19:00	0913-111, A	13_10_12_1900_21_086	1	1.70	0.864	1.05	0.537	8.41	0.240	2.73	1.32	3.00	1.53	3.51	0.649	
Average Conc. (ppm):				1	2.25	0.916	1.06	0.580	8.16	0.255	2.73	1.34	3.00	1.62	3.75	0.681

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	VO.62 13.10.18.12.58

Dryer 2 Run 1																
Date	Method	Filename	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/13/2013 9:21	0913-111, A	13_10_13_0921_40_932	1	2.53	0.630	5.62	0.101	17.3	0.524	2.78	0.07	1.37	0.203	1.48	0.474	
10/13/2013 9:22	0913-111, A	13_10_13_0922_41_572	1	1.61	0.616	6.08	0.103	18.4	0.551	2.78	0.08	1.70	0.199	0.985	0.455	
10/13/2013 9:23	0913-111, A	13_10_13_0923_41_392	1	2.02	0.641	6.63	0.108	18.8	0.561	2.78	0.08	1.69	0.207	1.39	0.480	
10/13/2013 9:24	0913-111, A	13_10_13_0924_42_103	1	1.25	0.634	6.81	0.106	18.9	0.556	2.78	0.07	1.88	0.213	1.17	0.472	
10/13/2013 9:25	0913-111, A	13_10_13_0925_42_893	1	1.84	0.630	7.02	0.104	19.1	0.559	2.78	0.08	1.97	0.210	0.934	0.466	
10/13/2013 9:26	0913-111, A	13_10_13_0926_43_653	1	2.09	0.648	7.27	0.109	19.3	0.565	2.78	0.07	2.02	0.216	1.24	0.486	
10/13/2013 9:27	0913-111, A	13_10_13_0927_44_353	1	1.59	0.652	7.16	0.111	19.5	0.556	2.78	0.08	2.34	0.216	0.934	0.484	
10/13/2013 9:28	0913-111, A	13_10_13_0928_45_093	1	1.92	0.648	7.07	0.108	19.8	0.550	2.78	0.08	2.23	0.214	0.934	0.485	
10/13/2013 9:29	0913-111, A	13_10_13_0929_45_913	1	2.06	0.610	6.71	0.104	19.9	0.545	2.78	0.07	2.22	0.208	1.13	0.453	
10/13/2013 9:30	0913-111, A	13_10_13_0930_46_663	1	1.25	0.620	6.81	0.108	20.0	0.544	2.78	0.08	2.28	0.210	0.934	0.461	
10/13/2013 9:31	0913-111, A	13_10_13_0931_47_433	1	1.25	0.652	6.61	0.107	20.2	0.542	2.78	0.08	2.27	0.213	0.934	0.486	
10/13/2013 9:32	0913-111, A	13_10_13_0932_48_143	1	1.54	0.631	6.32	0.105	20.2	0.544	2.78	1.97	1.92	0.211	0.945	0.472	
10/13/2013 9:33	0913-111, A	13_10_13_0933_48_863	1	1.93	0.639	6.25	0.106	20.2	0.539	2.78	1.93	2.33	0.212	0.934	0.478	
10/13/2013 9:34	0913-111, A	13_10_13_0934_49_573	1	1.25	0.625	5.96	0.109	20.5	0.547	2.78	1.81	2.36	0.215	0.934	0.465	
10/13/2013 9:35	0913-111, A	13_10_13_0935_50_263	1	1.95	0.617	5.68	0.104	20.3	0.529	2.78	1.72	2.12	0.207	0.934	0.457	
10/13/2013 9:36	0913-111, A	13_10_13_0936_51_104	1	2.84	0.624	5.68	0.107	19.9	0.523	2.78	1.71	2.23	0.211	0.934	0.467	
10/13/2013 9:37	0913-111, A	13_10_13_0937_51_824	1	1.88	0.617	5.55	0.101	19.3	0.509	2.78	1.60	2.16	0.207	0.934	0.460	
10/13/2013 9:38	0913-111, A	13_10_13_0938_52_634	1	1.86	0.614	5.38	0.104	18.8	0.513	2.78	1.62	2.11	0.206	0.934	0.457	
10/13/2013 9:39	0913-111, A	13_10_13_0939_53_384	1	1.45	0.624	5.46	0.101	19.1	0.516	2.78	1.59	2.26	0.209	0.934	0.462	
10/13/2013 9:40	0913-111, A	13_10_13_0940_54_084	1	1.63	0.644	5.40	0.104	19.9	0.517	2.78	1.49	2.30	0.216	0.934	0.479	
10/13/2013 9:41	0913-111, A	13_10_13_0941_54_884	1	2.02	0.611	5.47	0.108	20.4	0.517	2.78	1.58	2.20	0.216	0.934	0.455	
10/13/2013 9:42	0913-111, A	13_10_13_0942_55_604	1	1.97	0.624	5.40	0.107	20.9	0.511	2.78	1.61	2.26	0.213	0.934	0.465	
10/13/2013 9:43	0913-111, A	13_10_13_0943_56_414	1	2.27	0.601	5.23	0.104	21.1	0.513	2.78	1.57	2.09	0.213	0.934	0.449	
10/13/2013 9:44	0913-111, A	13_10_13_0944_57_124	1	1.69	0.614	5.28	0.111	21.2	0.507	2.78	1.55	2.02	0.219	0.934	0.464	
10/13/2013 9:45	0913-111, A	13_10_13_0945_57_864	1	1.67	0.627	5.10	0.105	21.1	0.509	2.78	1.53	2.13	0.213	0.934	0.466	
10/13/2013 9:46	0913-111, A	13_10_13_0946_58_664	1	1.91	0.621	5.13	0.106	21.4	0.514	2.78	1.46	2.32	0.215	0.934	0.462	
10/13/2013 9:47	0913-111, A	13_10_13_0947_59_355	1	1.42	0.595	5.45	0.108	21.7	0.521	2.78	1.53	2.19	0.216	0.934	0.448	
10/13/2013 9:49	0913-111, A	13_10_13_0949_00_105	1	1.86	0.641	5.46	0.110	21.5	0.510	2.78	1.51	2.23	0.220	0.934	0.479	
10/13/2013 9:50	0913-111, A	13_10_13_0950_00_875	1	1.25	0.630	5.56	0.107	21.4	0.517	2.78	1.54	2.22	0.218	0.934	0.465	
10/13/2013 9:51	0913-111, A	13_10_13_0951_01_625	1	1.89	0.645	5.83	0.116	21.6	0.536	2.78	1.39	2.25	0.224	0.934	0.485	
10/13/2013 9:52	0913-111, A	13_10_13_0952_02_335	1	1.62	0.635	6.10	0.109	21.9	0.541	2.78	1.51	2.48	0.225	0.934	0.472	
10/13/2013 9:53	0913-111, A	13_10_13_0953_03_175	1	1.66	0.625	5.99	0.109	21.6	0.539	2.78	1.51	2.37	0.220	0.934	0.466	
10/13/2013 9:54	0913-111, A	13_10_13_0954_03_855	1	1.93	0.623	5.89	0.110	21.9	0.541	2.78	1.54	2.49	0.224	0.934	0.464	
10/13/2013 9:55	0913-111, A	13_10_13_0955_04_565	1	2.47	0.633	6.09	0.110	21.8	0.540	2.78	1.64	2.52	0.222	0.934	0.474	
10/13/2013 9:56	0913-111, A	13_10_13_0956_05_405	1	1.19	0.619	6.11	0.111	21.9	0.539	2.78	1.59	2.68	0.221	0.934	0.467	
10/13/2013 9:57	0913-111, A	13_10_13_0957_06_075	1	1.81	0.614	6.23	0.112	21.9	0.543	2.78	1.58	2.57	0.226	0.934	0.460	
10/13/2013 9:58	0913-111, A	13_10_13_0958_06_845	1	1.40	0.650	6.62	0.113	22.1	0.556	2.78	1.64	2.70	0.229	0.934	0.483	
10/13/2013 9:59	0913-111, A	13_10_13_0959_07_685	1	1.79	0.616	6.83	0.113	22.1	0.565	2.78	1.65	2.62	0.230	0.934	0.467	
10/13/2013 10:00	0913-111, A	13_10_13_1000_08_486	1	1.25	0.640	6.83	0.109	22.1	0.561	2.78	1.64	2.62	0.224	0.934	0.482	
10/13/2013 10:01	0913-111, A	13_10_13_1001_09_226	1	1.28	0.649	7.05	0.110	21.8	0.555	2.78	1.67	2.78	0.234	0.934	0.481	
10/13/2013 10:02	0913-111, A	13_10_13_1002_09_906	1	2.18	0.629	6.90	0.114	21.5	0.548	2.78	1.63	2.82	0.232	0.934	0.473	
10/13/2013 10:03	0913-111, A	13_10_13_1003_10_696	1	2.08	0.678	6.91	0.118	21.2	0.543	2.78	1.54	2.87	0.239	0.934	0.507	
10/13/2013 10:04	0913-111, A	13_10_13_1004_11_436	1	2.56	0.639	6.24	0.114	20.9	0.528	2.78	1.49	2.62	0.231	0.934	0.482	
10/13/2013 10:05	0913-111, A	13_10_13_1005_12_186	1	1.61	0.623	5.90	0.107	20.5	0.525	2.78	1.62	2.66	0.235	0.934	0.464	
10/13/2013 10:06	0913-111, A	13_10_13_1006_12_966	1	2.39	0.625	6.04	0.109	19.6	0.533	2.78	1.54	2.66	0.233	0.934	0.468	
10/13/2013 10:07	0913-111, A	13_10_13_1007_13_776	1	1.78	0.625	6.36	0.111	18.8	0.542	2.78	1.62	2.53	0.228	0.934	0.472	
10/13/2013 10:08	0913-111, A	13_10_13_1008_14_516	1	2.53	0.642	6.82	0.106	17.6	0.550	2.78	1.55	2.58	0.229	0.934	0.480	
10/13/2013 10:09	0913-111, A	13_10_13_1009_15_276	1	2.29	0.634	7.03	0.111	16.5	0.550	2.78	1.51	2.55	0.231	0.934	0.479	
10/13/2013 10:10	0913-111, A	13_10_13_1010_15_986	1	1.44	0.650	7.05	0.111	15.3	0.549	2.78	1.57	2.40	0.228	0.934	0.494	
10/13/2013 10:11	0913-111, A	13_10_13_1011_16_786	1	2.51	0.631	7.36	0.109	14.0	0.549	2.78	1.55	2.54	0.228	0.934	0.476	
10/13/2013 10:12	0913-111, A	13_10_13_1012_17_487	1	1.46	0.650	7.48	0.107	12.8	0.543	2.78	1.51	2.63	0.225	0.934	0.483	
10/13/2013 10:13	0913-111, A	13_10_13_1013_18_297	1	2.24	0.680	7.75	0.108	11.6	0.536	2.78	1.49	2.72	0.225	0.934	0.490	
10/13/2013 10:14	0913-111, A	13_10_13_1014_19_017	1	2.42	0.677	8.54	0.110	11.0	0.555	2.78	1.38	2.71	0.227	0.934	0.504	
10/13/2013 10:15	0913-111, A	13_10_13_1015_19_817	1	2.16	0.619	7.71	0.106	11.0	0.543	2.78	1.24	2.71	0.225	0.934	0.470	
10/13/2013 10:16	0913-111, A	13_10_13_1016_20_417	1	2.13	0.618	7.44	0.109	11.7	0.549	2.78	1.34	2.42	0.233	0.934	0.466	
10/13/2013 10:17	0913-111, A	13_10_13_1017_21_227	1	1.37	0.621	7.70	0.113	12.8	0.556	2.78	1.46	2.61	0.242	0.939	0.470	
10/13/2013 10:18	0913-111, A	13_10_13_1018_21_987	1	2.79	0.636	7.44	0.110	13.2	0.560	2.78	1.49	2.75	0.255	0.947	0.479	
10/13/2013 10:19	0913-111, A	13_10_13_1019_22_707	1	1.95	0.634	6.71	0.107	12.9	0.550	2.78	1.53	2.64	0.256	0.934	0.471	
10/13/2013 10:20	0913-111, A	13_10_13_1020_23_387	1	2.11	0.594	6.66	0.110	12.8	0.547	2.78	1.51	2.54	0.258	0.934	0.447	
10/13/2013 10:21	0913-111, A	13_10_13_1021_23_197	1	3.00	0.628	6.73	0.113	12.7	0.558	2.78	1.51	2.53	0.273	0.988	0.468	
Average Conc. (ppm):				1	1.90	0.631	6.40	0.108	18.8	0.539	2.78	1.29	2.37	0.222	0.967	0.472

Dryer 2 Run 2																
Date	Method	Filename	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/13/2013 11:04	0913-111, A	13_10_13_1104_56_401	1	2.45	0.615	6.06	0.106	10.4	0.532	2.78	1.31	1.47	0.260	3.09	0.457	
10/13/2013 11:05	0913-111, A	13_10_13_1105_57_461	1	2.20	0.620	6.50	0.108	10.0	0.535	2.78	1.31	1.39	0.260	3.57	0.457	
10/13/2013 11:06	0913-111, A	13_10_13_1106_57_901	1	2.54	0.621	7.03	0.102	10.5	0.542	2.78	1.31	1.52	0.260	3.34	0.458	
10/13/2013 11:07	0913-111, A	13_10_13_1107_58_651	1	1.00	0.692	7.38	0.103	10.1	0.564	2.78	1.30	1.04	0.252	4.46	0.510	
10/13/2013 11:08	0913-111, A	13_10_13_1108_59_481	1	2.72	0.633	7.22	0.109	10.2	0.560	2.78	1.29	1.71	0.257	3.00	0.473	
10/13/2013 11:10	0913-111, A	13_10_13_1110_00_091	1	2.32	0.634	6.92	0.103	10.3	0.553	2.78	1.28	1.40	0.254	3.20	0.466	
10/13/2013 11:11	0913-111, A	13_10_13_1111_01_001	1	2.71	0.646	6.81	0.112	10.7	0.582	2.78	1.28	1.67	0.262	3.57	0.485	
10/13/2013 11:12	0913-111, A	13_10_13_1112_01_811	1	2.29	0.627	7.86	0.112	10.1	0.568	2.78	1.28	1.57	0.260	3.79	0.463	
10/13/2013 11:13	0913-111, A	13_10_13_1113_02_502	1	3.29	0.629	6.97	0.107	10.7	0.541	2.78	2.74	1.35	0.248	3.29	0.465	
10/13/2013 11:14	0913-111, A	13_10_13_1114_03_312	1	2.51	0.629	6.60	0.106	10.5	0.530	2.78	2.55	1.30	0.241	2.61	0.465	
10/13/2013 11:15	0913-111, A	13_10_13_1115_04_382	1	2.24	0.610	6.53	0.102	10.4	0.538	2.78	2.10	1.56	0.248	2.57	0.448	
10/13/2013 11:16	0913-111, A	13_10_13_1116_04_943	1	2.72	0.588	6.10	0.101	10.3	0.543	2.78	1.79	1.33	0.238	3.08	0.448	
10/13/2013 11:17	0913-111, A	13_10_13_1117_05_582	1	0.56	0.592	6.24	0.0980	10.3	0.533	2.78	1.38	1.28	0.244	2.91	0.439	
10/13/2013 11:18	0913-111, A	13_10_13_1118_06_416	1	2.07	0.621	6.11	0.103	10.3	0.527	2.78	1.47	1.40	0.258	2.98	0.457	
10/13/2013 11:19	0913-111, A	13_10_13_1119_07_122	1	2.81	0.620	6.49	0.106	10.3	0.539	2.78	1.61	1.44	0.266	3.07	0.461	
10/13/2013 11:20	0913-111, A	13_10_13_1120_07_922	1	2.54	0.625	6.27	0.100	10.3	0.539	2.78	1.50	1.11	0.266	3.66	0.460	
10/13/2013 11:21	0913-111, A	13_10_13_1121_08_533	1	0.56	0.613	6.22	0.100	10.3	0.540	2.78	1.61	1.50	0.266	3.66	0.460	
10/13/2013 11:22	0913-111, A	13_10_13_1122_09_442	1	2.46	0.627	6.14	0.108	9.82	0.565	2.78	1.45	1.36	0.275	3.62	0.460	
10/13/2013 11:23	0913-111, A	13_10_13_1123_10_163	1	2.41	0.614	5.90	0.104	9.53	0.550	2.78	1.48	1.22	0.276	4.03	0.451	
10/13/2013 11:24	0913-111, A	13_10_13_1124_10_923	1	2.79	0.603	6.11	0.108	9.42	0.549	2.78	1.39	1.16	0.273	3.62	0.449	
10/13/2013 11:25	0913-111, A	13_10_13_1125_11_263	1	3.11	0.618	7.04	0.106	9.79	0.571	2.78	1.40	1.33	0.270	4.39	0.464	
10/13/2013 11:26	0913-111, A	13_10_13_1126_12_453	1	2.80	0.623	7.04	0.105	9.81	0.551	2.78	1.45	1.31	0.275	3.32	0.458	
10/13/2013 11:27	0913-111, A	13_10_13_1127_13_723	1	3.37	0.574	6.09	0.102	9.90	0.536	2.78	1.39	1.42	0.259	2.58	0.425	
10/13/2013 11:28	0913-111, A	13_10_13_1128_13_963	1	2.85	0.579	5.99	0.103	10.0	0.540	2.78	1.51	1.28	0.258	2.69	0.425	
10/13/2013 11:29	0913-111, A	13_10_13_1129_14_773	1	2.27	0.594	5.66	0.103	10.2	0.548	2.78	1.49	1.06	0.261	2.53	0.436	
10/13/2013 11:30	0913-111, A	13_10_13_1130_15_463	1	2.34	0.605	6.18	0.105	10.7	0.572	2.78	1.43	1.35	0.271	2.57	0.450	
Average Conc (ppm):				1	2.59	0.617	6.58	0.105	10.2	0.549	2.78	1.55	1.38	0.260	3.28	0.457

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	V0.62 13.10.18.12.58

Path Length - Path

Date	Method	FileName	ethylene (ppm)	SEC (ppm)
10/10/2013 8:12	0913-111_CTS	13_10_10_0812_04_850	8.79	0.137
10/10/2013 8:12	0913-111_CTS	13_10_10_0812_23_390	8.77	0.136
10/10/2013 8:12	0913-111_CTS	13_10_10_0812_42_040	8.78	0.137
10/10/2013 8:13	0913-111_CTS	13_10_10_0813_00_420	8.80	0.136
10/10/2013 8:13	0913-111_CTS	13_10_10_0813_18_930	8.82	0.137
10/10/2013 8:13	0913-111_CTS	13_10_10_0813_37_540	8.81	0.138
10/10/2013 8:13	0913-111_CTS	13_10_10_0813_56_040	8.82	0.137
10/10/2013 8:14	0913-111_CTS	13_10_10_0814_14_670	8.80	0.138

Average (m) 8.80 0.137

10/10/2013 19:33	0913-111_CTS	13_10_10_1933_09_783	8.67	0.137
10/10/2013 19:33	0913-111_CTS	13_10_10_1933_28_313	8.69	0.137
10/10/2013 19:33	0913-111_CTS	13_10_10_1933_46_843	8.69	0.138
10/10/2013 19:34	0913-111_CTS	13_10_10_1934_05_353	8.71	0.137
10/10/2013 19:34	0913-111_CTS	13_10_10_1934_23_963	8.70	0.137
10/10/2013 19:34	0913-111_CTS	13_10_10_1934_42_473	8.71	0.138
10/10/2013 19:35	0913-111_CTS	13_10_10_1935_01_103	8.66	0.137
10/10/2013 19:35	0913-111_CTS	13_10_10_1935_19_513	8.67	0.139

Average (m) 8.69 0.138

Average Pathlength (m) 8.74 0.137

Max (m) 8.80

Min (m) 8.69

Max % Deviation 0.62%

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	V0.62 13.10.18.12.58

Path Length - Path

Date	Method	FileName	ethylene (ppm)	SEC (ppm)
10/11/2013 9:38	0913-111_CTS	13_10_11_0938_33_970	8.13	0.130
10/11/2013 9:38	0913-111_CTS	13_10_11_0938_52_580	8.16	0.129
10/11/2013 9:39	0913-111_CTS	13_10_11_0939_11_060	8.17	0.129
10/11/2013 9:39	0913-111_CTS	13_10_11_0939_29_540	8.18	0.129
10/11/2013 9:39	0913-111_CTS	13_10_11_0939_48_180	8.19	0.130
10/11/2013 9:40	0913-111_CTS	13_10_11_0940_06_710	8.18	0.129
10/11/2013 9:40	0913-111_CTS	13_10_11_0940_25_190	8.20	0.129
10/11/2013 9:40	0913-111_CTS	13_10_11_0940_43_760	8.18	0.130

Average (m) 8.17 0.129

10/11/2013 11:22	0913-111_CTS	13_10_11_1122_55_958	8.63	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_14_479	8.66	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_32_989	8.68	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_51_519	8.71	0.133
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_10_019	8.70	0.134
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_28_559	8.73	0.134
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_47_159	8.74	0.134
10/11/2013 11:25	0913-111_CTS	13_10_11_1125_05_659	8.74	0.134

Average (m) 8.70 0.134

Average Pathlength (m) 8.44 0.131

Max (m) 8.70

Min (m) 8.17

Max % Deviation 3.10%

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	V0.62 13.10.18.12.58

Path Length - Path

Date	Method	FileName	ethylene (ppm)	SEC (ppm)
10/11/2013 11:22	0913-111_CTS	13_10_11_1122_55_958	8.63	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_14_479	8.66	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_32_989	8.68	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_51_519	8.71	0.133
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_10_019	8.70	0.134
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_28_559	8.73	0.134
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_47_159	8.74	0.134
10/11/2013 11:25	0913-111_CTS	13_10_11_1125_05_659	8.74	0.134
Average (m)			8.70	0.134
10/11/2013 13:02	0913-111_CTS	13_10_11_1302_32_762	8.73	0.133
10/11/2013 13:02	0913-111_CTS	13_10_11_1302_51_282	8.77	0.134
10/11/2013 13:03	0913-111_CTS	13_10_11_1303_09_882	8.73	0.133
10/11/2013 13:03	0913-111_CTS	13_10_11_1303_28_382	8.71	0.133
10/11/2013 13:03	0913-111_CTS	13_10_11_1303_46_792	8.74	0.133
10/11/2013 13:04	0913-111_CTS	13_10_11_1304_05_402	8.75	0.133
10/11/2013 13:04	0913-111_CTS	13_10_11_1304_23_922	8.74	0.133
10/11/2013 13:04	0913-111_CTS	13_10_11_1304_42_382	8.73	0.133
Average (m)			8.74	0.133
10/11/2013 17:56	0913-111_CTS	13_10_11_1756_33_272	8.44	0.129
10/11/2013 17:56	0913-111_CTS	13_10_11_1756_51_882	8.57	0.130
10/11/2013 17:57	0913-111_CTS	13_10_11_1757_10_412	8.67	0.132
10/11/2013 17:57	0913-111_CTS	13_10_11_1757_29_032	8.71	0.132
10/11/2013 17:57	0913-111_CTS	13_10_11_1757_47_542	8.75	0.132
10/11/2013 17:58	0913-111_CTS	13_10_11_1758_06_042	8.76	0.132
10/11/2013 17:58	0913-111_CTS	13_10_11_1758_24_642	8.79	0.133
10/11/2013 17:58	0913-111_CTS	13_10_11_1758_43_102	8.75	0.133
Average (m)			8.68	0.132
10/12/2013 7:59	0913-111_CTS	13_10_12_0759_05_353	8.70	0.139
10/12/2013 7:59	0913-111_CTS	13_10_12_0759_23_963	8.74	0.139
10/12/2013 7:59	0913-111_CTS	13_10_12_0759_42_473	8.71	0.137
10/12/2013 8:00	0913-111_CTS	13_10_12_0800_01_103	8.70	0.136
10/12/2013 8:00	0913-111_CTS	13_10_12_0800_19_593	8.69	0.137
10/12/2013 8:00	0913-111_CTS	13_10_12_0800_38_103	8.75	0.136
10/12/2013 8:00	0913-111_CTS	13_10_12_0800_56_713	8.68	0.136
10/12/2013 8:01	0913-111_CTS	13_10_12_0801_15_143	8.68	0.136

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	V0.62 13.10.18.12.58

Path Length - Path

Date	Method	FileName	ethylene (ppm)	SEC (ppm)
Average (m)			8.71	0.137
10/12/2013 8:15	0913-111_CTS	13_10_12_0815_33_684	8.60	0.134
10/12/2013 8:15	0913-111_CTS	13_10_12_0815_52_184	8.59	0.134
10/12/2013 8:16	0913-111_CTS	13_10_12_0816_10_704	8.58	0.134
10/12/2013 8:16	0913-111_CTS	13_10_12_0816_29_314	8.60	0.133
10/12/2013 8:16	0913-111_CTS	13_10_12_0816_47_804	8.60	0.133
10/12/2013 8:17	0913-111_CTS	13_10_12_0817_06_244	8.61	0.134
10/12/2013 8:17	0913-111_CTS	13_10_12_0817_24_834	8.62	0.133
10/12/2013 8:17	0913-111_CTS	13_10_12_0817_43_344	8.59	0.134
Average (m)			8.60	0.134
10/12/2013 13:02	0913-111_CTS	13_10_12_1302_33_472	8.74	0.137
10/12/2013 13:02	0913-111_CTS	13_10_12_1302_52_082	8.76	0.137
10/12/2013 13:03	0913-111_CTS	13_10_12_1303_10_582	8.79	0.137
10/12/2013 13:03	0913-111_CTS	13_10_12_1303_29_082	8.79	0.138
10/12/2013 13:03	0913-111_CTS	13_10_12_1303_47_602	8.78	0.137
10/12/2013 13:04	0913-111_CTS	13_10_12_1304_06_112	8.77	0.137
10/12/2013 13:04	0913-111_CTS	13_10_12_1304_24_752	8.78	0.137
10/12/2013 13:04	0913-111_CTS	13_10_12_1304_43_242	8.78	0.138
Average (m)			8.78	0.137
10/12/2013 19:42	0913-111_CTS	13_10_12_1942_21_772	8.68	0.133
10/12/2013 19:42	0913-111_CTS	13_10_12_1942_40_362	8.71	0.132
10/12/2013 19:42	0913-111_CTS	13_10_12_1942_58_862	8.77	0.134
10/12/2013 19:43	0913-111_CTS	13_10_12_1943_17_462	8.77	0.134
10/12/2013 19:43	0913-111_CTS	13_10_12_1943_35_992	8.80	0.134
10/12/2013 19:43	0913-111_CTS	13_10_12_1943_54_432	8.79	0.133
10/12/2013 19:44	0913-111_CTS	13_10_12_1944_13_082	8.82	0.135
10/12/2013 19:44	0913-111_CTS	13_10_12_1944_31_502	8.78	0.134
Average (m)			8.76	0.134
10/13/2013 7:58	0913-111_CTS	13_10_13_0758_40_845	8.55	0.130
10/13/2013 7:58	0913-111_CTS	13_10_13_0758_59_345	8.50	0.129
10/13/2013 7:59	0913-111_CTS	13_10_13_0759_17_835	8.49	0.129
10/13/2013 7:59	0913-111_CTS	13_10_13_0759_36_445	8.50	0.129
10/13/2013 7:59	0913-111_CTS	13_10_13_0759_54_925	8.49	0.129
10/13/2013 8:00	0913-111_CTS	13_10_13_0800_13_565	8.51	0.130
10/13/2013 8:00	0913-111_CTS	13_10_13_0800_31_995	8.47	0.130

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	V0.62 13.10.18.12.58

Path Length - Path

Date	Method	FileName	ethylene (ppm)	SEC (ppm)
10/13/2013 8:00	0913-111_CTS	13_10_13_0800_50_506	8.52	0.130
Average (m)			8.50	0.130
10/13/2013 8:16	0913-111_CTS	13_10_13_0816_09_687	8.73	0.133
10/13/2013 8:16	0913-111_CTS	13_10_13_0816_28_197	8.69	0.133
10/13/2013 8:16	0913-111_CTS	13_10_13_0816_46_707	8.71	0.134
10/13/2013 8:17	0913-111_CTS	13_10_13_0817_05_247	8.72	0.133
10/13/2013 8:17	0913-111_CTS	13_10_13_0817_23_757	8.73	0.134
10/13/2013 8:17	0913-111_CTS	13_10_13_0817_42_347	8.77	0.134
10/13/2013 8:18	0913-111_CTS	13_10_13_0818_00_857	8.70	0.133
10/13/2013 8:18	0913-111_CTS	13_10_13_0818_19_377	8.74	0.134
Average (m)			8.72	0.134
10/13/2013 14:34	0913-111_CTS	13_10_13_1434_10_233	8.70	0.135
10/13/2013 14:34	0913-111_CTS	13_10_13_1434_28_743	8.73	0.135
10/13/2013 14:34	0913-111_CTS	13_10_13_1434_47_263	8.76	0.136
10/13/2013 14:35	0913-111_CTS	13_10_13_1435_05_884	8.75	0.135
10/13/2013 14:35	0913-111_CTS	13_10_13_1435_24_394	8.72	0.133
10/13/2013 14:35	0913-111_CTS	13_10_13_1435_42_804	8.74	0.135
10/13/2013 14:36	0913-111_CTS	13_10_13_1436_01_424	8.74	0.134
10/13/2013 14:36	0913-111_CTS	13_10_13_1436_19_934	8.72	0.134
Average (m)			8.73	0.135
Average Pathlength (m)			8.69	0.134
Max (m)			8.78	
Min (m)			8.50	
Max % Deviation			2.17%	

APPENDIX D

Method 320 Log Sheet

FTIR Log - Enviva Wiggins

Date	Time	Filename	Method	Pressure	Notes	Run ID	
10-Oct	754	13.10.10.0753.42.969	CTS	14.7	Background		
	806	13.10.10.0806.08.036	CTS	14.7	CTS (pathlength = 8.78 m)		
	855	13.10.10.0855.00.744	0913-177A	14.6	Background		
	914	13.10.10.0914.12.674	0913-177A	13.5	Sampling GHM - Run 1 (0917-1017)	1	
	1036	13.10.10.0914.12.674	0913-177A	13.3	Sampling GHM - Run 2 (1036-1136)	2	
	1150	13.10.10.0914.12.674	0913-177A	13.5	Sampling GHM - Run 3 (1150-1250)	3	
	1738	13.10.10.1429.45.242	0913-177A	13.9	Sampling Dryer 1 - Run 1 (1738-1838)	4	
	1915	13.10.10.1915.03.541	0913-177A	14.6	Background		
	1923	13.10.10.1923.11.342	CTS	14.6	Background		
	1926	13.10.10.1926.54.274	CTS	14.7	CTS (pathlength = 8.78 m)		
	2005	13.10.10.2004.59.706	0913-177A	14.6	Water Spectra (Dryer 1 - Run 1)		
	2035	13.10.10.2034.59.394	0913-177A	14.6	Water Spectra (GHM)		
11-Oct	933	13.10.11.0932.48.189	CTS	14.8	Background		Background interference
	936	13.10.11.0936.57.524	CTS	14.8	CTS (pathlength = 8.18 m)		
	948	13.10.11.0948.41.630	0913-177A	14.8	Background		
	955	13.10.11.0954.19.486	0913-177A	14.4	Sampling Dryer 1 - Run 2 (1000-1100)	5	
	1117	13.10.11.1117.32.588	CTS	14.8	Background		
	1121	13.10.11.1121.00.310	CTS	14.8	CTS (pathlength = 8.73 m)		
	1127	13.10.11.1127.34.199	0913-177A	14.7	Background		
	1137	13.10.11.1134.41.951	0913-177A	14.2	Sampling Dryer 1 - Run 3 (1137-1237)	6	
	1257	13.10.11.1257.46.512	CTS	14.7	Background		
	1301	13.10.11.1301.14.338	CTS	14.7	CTS (pathlength = 8.73 m)		
	1308	13.10.11.1308.39.947	0913-177A	14.7	Background		
	1342	13.10.11.1342.51.774	0913-177A	14.2	Sampling Pellet Cooler 2 - Run 1 (1343-1443)	7	
	1508	13.10.11.1342.51.774	0913-177A	14.1	Sampling Pellet Cooler 2 - Run 2 (1508-1608)	8	
	1650	13.10.11.1342.51.774	0913-177A	14.1	Sampling Pellet Cooler 2 - Run 3 (1629-1729)	9	
	1752	13.10.11.1752.08.661	CTS	14.6	Background		
	1755	13.10.11.1755.37.781	CTS	14.6	CTS (pathlength = 8.7165 m)		
	1802	13.10.11.1802.37.522	0913-177A	14.6	Background		
	1342	13.10.11.1809.44.552	0913-177A	14.3	Sampling Hammermill 2 - Run 1 (1811-1911)	10	
	1935	13.10.11.1809.44.552	0913-177A	14.4	Sampling Hammermill 2 - Run 2 (1935-2035)	11	
	2048	13.10.11.1809.44.552	0913-177A	14.5	Sampling Hammermill 2 - Run 3 (2048-2148)	12	
	2200	13.10.11.2200.54.734	CTS	14.7	Background		
	2204	13.10.11.2204.32.940	CTS	14.8	CTS (pathlength = 8.75475 m)		
	2213	13.10.11.2213.44.875	0913-177A	14.8	Background		
	2224	13.10.11.2224.53.772	0913-177A	14.7	Water Spectra (Dryer 1 - Run 2, 3)		
	2240	13.10.11.2240.27.896	0913-177A	14.7	Water Spectra (Pellet Cooler 2, Hammermill 2)		
12-Oct	0805	13.10.12.0805.29.253	CTS	14.9	Background		
	0809	13.10.12.0809.22.964	CTS	14.9	CTS (pathlength = 8.59 m)		
	0822	13.10.12.08.22.17.097	0913-177A	14.8	Background		
	858	13.10.12.0857.28.740	0913-177A	14.4	Sampling Pellet Cooler 1- Run 1 (0858-0958)	13	
	1022	13.10.12.0857.28.740	0913-177A	14.3	Sampling Pellet Cooler 1- Run 2 (1022-1122)	14	
	1141	13.10.12.0857.28.740	0913-177A	14.2	Sampling Pellet Cooler 1- Run 1 (1141-1241)	15	
	1257	13.10.12.1257.12.281	CTS	14.6	Background		
	1301	13.10.12.1300.55.794	CTS	14.6	CTS (pathlength = 8.77 m)		
	1308	13.10.12.1309.21.752	0913-177A	14.6	Background		
	1509	13.10.12.1347.50.707	0913-177A	13.8	Sampling Aspirator- Run 1 (1509-1609)	16	
	1636	13.10.12.1347.50.707	0913-177A	13.8	Sampling Aspirator- Run 2 (1636-1736)	17	
	1800	13.10.12.1347.50.707	0913-177A	13.9	Sampling Aspirator- Run 3 (1800-1900)	18	
	1936	13.10.12.1936.27.563	CTS	14.91	Background		
	1940	13.10.12.1940.26.868	CTS	14.72	CTS (pathlength = 8.78 m)		
	1951	13.10.12.1951.39.443	0913-177A	14.75	Background		
	2003	13.10.12.2003.07.633	0913-177A	14.59	Water Spectra (Aspirator)		
	2023	13.10.12.2023.12.427	0913-177A	14.55	Water Spectra (Pellet Cooler 1)		
13-Oct	807	13.10.13.0807.16.306	0913-177A	14.77	Background		
	0810	13.10.13.0810.33.996	CTS	14.78	Background		
	0810	13.10.13.0813.37.211	CTS	14.85	CTS (pathlength = 8.71 m)		
	0921	13.10.13.0919.17.032	0913-177A	14.24	Sampling Dryer 2 - Run 1 (0921-1021)	19	
	1104	13.10.13.0919.17.032	0913-177A	14.17	Sampling Dryer 2 - Run 2 (1104-1204)	20	
	1231	13.10.13.0919.17.032	0913-177A	14.17	Sampling Dryer 2 - Run 3 (1231-1347); paused 1236-1252	21	
	1420	13.10.13.1419.54.342	CTS	14.91	Background		
	1430	13.10.13.1425.31.173	CTS	14.85	CTS (pathlength = 8.73 m)		
	1447	13.10.13.1447.35.695	0913-177A	14.8	Background		
	1506	13.10.13.1506.31.082	0913-177A	14.71	Water Spectra (Dryer 2)		1130-1200 water condensation in

APPENDIX E

Example Calculations

EXAMPLE CALCULATIONS

Run Number: Dryer 1 – Run 1

Stack Gas Temperature, °R

$$T_s = 460 + t_s$$

$$T_s = 460 + 146.3 = 606.3 \text{ °R}$$

Volume of Dry Gas Sampled at Standard Conditions, Dry Standard Cubic Feet

$$V_{\text{mstd}} = [17.64] \left[\gamma \right] \left[V_m \right] \left[\frac{\left(P_{\text{bar}} + \frac{\Delta H}{13.6} \right)}{T_m + 460} \right]$$

$$V_{\text{mstd}} = [17.64] [0.9728] [33.201] \left[\frac{\left(29.90 + \frac{1.00}{13.6} \right)}{541.3} \right]$$

$$V_{\text{mstd}} = 31.564 \text{ ft}^3$$

Volume of Water Sampled, SCF

$$V_{\text{wstd}} = 0.04715 [\text{Weight of Condensed Moisture}]$$

$$V_{\text{wstd}} = 0.04715 [129.5]$$

$$V_{\text{wstd}} = 6.106 \text{ ft}^3$$

Fraction of Water Vapor in Sample Gas Stream

$$\% \text{H}_2\text{O} = \left[\frac{V_{\text{wstd}}}{V_{\text{mstd}} + V_{\text{wstd}}} \right] \times 100$$

$$\% \text{H}_2\text{O} = \left[\frac{6.106}{31.564 + 6.106} \right] \times 100$$

$$\% \text{H}_2\text{O} = 16.21$$

Dry Mole Fraction of Flue Gas

$$M_{fd} = 1 - \%H_2O/100$$

$$M_{fd} = 1 - [16.21/100]$$

$$M_{fd} = 0.838$$

Molecular Weight of Sample Gas, Dry

$$M_d = 0.44[\%CO_2] + 0.32[\%O_2] + 0.28[100 - \%O_2 - \%CO_2]$$

$$M_d = 0.44[2.0] + 0.32[19.0] + 0.28[100 - 19.0 - 2.0]$$

$$M_d = 29.08 \text{ pounds/pound-mole}$$

Molecular Weight of Sample Gas, Actual Conditions

$$M_s = [M_d \times M_{fd}] + [0.18 \times \%H_2O]$$

$$M_s = [29.08 \times 0.838] + [0.18 \times 16.21]$$

$$M_s = 27.28 \text{ pounds/pound-mole}$$

Average Stack Gas Velocity, Feet/second

$$v_s = K_p C_p \left(\sqrt{(\Delta p)} \right)_{avg} \left[\sqrt{\frac{T_s + 460}{P_s M_s}} \right]$$

$$v_s = (85.49)(0.84) \left(\sqrt{(0.1.283)} \right) \left[\sqrt{\frac{606.3}{(29.84)(27.28)}} \right]$$

$$v_s = 70.18 \text{ feet/second}$$

Wet Volumetric Flue Gas Flow Rate at Stack Conditions, Cubic Feet per Minute

$$Q_{aw} = 60 \times v_s \times A$$

$$Q_{aw} = 60 \times 70.18 \times 10.56$$

$$Q_{aw} = 44,461 \text{ Actual Cubic Feet per Minute}$$

Dry Volumetric Flue Gas Flow Rate at Standard Conditions, Cubic Feet per Minute

$$Q_{sd} = 60 \times Mfd \times v_s \times A \times \left[\frac{528}{ts + 460} \right] \left[\frac{Ps}{29.92} \right]$$

$$Q_{sd} = 60 \times 0.838 \times 70.18 \times 10.56 \left[\frac{528}{606.3} \right] \left[\frac{29.84}{29.92} \right]$$

$$Q_{sd} = 32,360 \text{ Dry Standard Cubic Feet per Minute}$$

Average THC Dry Basis Concentration as Propane

$$C_{THCD} = (C_{THCW}) / (M_{fd})$$

Where: C_{THCd} = dry basis concentration of THC in ppm
 M_{fd} = dry mole fraction from Method 4 concurrent run

$$C_{THCD} = 66.7 / 0.838 = 79.6 \text{ ppm THC as propane}$$

Average THC Dry Basis Concentration as Carbon

$$C_{THCD} = (C_{THCW}) \times (3) / (M_{fd})$$

Where: C_{THCd} = dry basis concentration of THC in ppm
 M_{fd} = dry mole fraction from Method 4 concurrent run

$$C_{THCD} = (66.7) \times (3) / 0.838 = 238.8 \text{ ppm THC as Carbon}$$

VOC Emission Rate in Pounds Per Hour

$$E_{VOC} = (C_{VOC}) (Q_{SD}) (60 \text{ min/hr}) (C_F)$$

Where: Q_{SD} = measured flow rate in stack in dscfm
 C_F = Conversion factor in lb/scf – ppm
 $C_F = 3.117 \times 10^{-8}$ for Carbon

$$E_{VOC} = (238.8) (32,360) (60 \text{ min/hr}) (3.117 \times 10^{-8}) = 14.5 \text{ lb/hr as Carbon}$$

APPENDIX F

Gas Cylinder Certification Sheets

CERTIFICATE OF ANALYSIS

Grade of Product: EPA Protocol

Airgas Specialty Gases

630 United Drive
Durham, NC 27713
919-544-3773 Fax: 919-544-3774
www.airgas.com

Part Number: E02A199E15A00A6
Cylinder Number: CC410934
Laboratory: ASG - Durham - NC
PGVP Number: B22012
Gas Code: APPVD

Reference Number: 122-124323950-1
Cylinder Volume: 146 Cu.Ft.
Cylinder Pressure: 2015 PSIG
Valve Outlet: 590
Analysis Date: Jul 02, 2012

Expiration Date: Jul 02, 2015

Certification performed in accordance with "EPA Traceability Protocol (Sept. 1997)" using the assay procedures listed. Analytical Methodology does not require correction for analytical interferences. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.
Do Not Use This Cylinder below 150 psig i.e. 1 Mega Pascal

ANALYTICAL RESULTS				
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty
PROPANE	28.00 PPM	27.99 PPM	G1	+/- 1% NIST Traceable
Air	Balance			

CALIBRATION STANDARDS				
Type	Lot ID	Cylinder No	Concentration	Expiration Date
NTRM	080610	CC263046	49.62PPM PROPANE/AIR	May 14, 2018

ANALYTICAL EQUIPMENT		
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Nicolet 6700 AHR0801333 C3H8	FTIR	Jun 19, 2012

Triad Data Available Upon Request

Notes: ANW PN: 781077

Approved for Release



Praxair Distribution Mid-Atlantic
145 Shimmersville Rd.
Bethlehem, PA 18015
Tel: (610) 317-1608 Fax: (610) 758 8382
PGVP ID:

DocNumber: 000003740

CERTIFICATE OF ANALYSIS / EPA PROTOCOL GAS

Customer & Order Information:

CHEROKEE INSTRUMENTS INC *
901 BRIDGE ST
FUQUAY VARINA NC 275260

Praxair Order Number: 13003732
Customer P. O. Number: 10429
Customer Reference Number:

Fill Date: 4/7/2010
Part Number: EV AIPR50ME-AS
Lot Number: 917009747
Cylinder Style & Outlet: AS CGA 590
Cylinder Pressure & Volume: 2000 psig 140 cu. ft.

Certified Concentration:

Expiration Date:	4/12/2018	NIST Traceable
Cylinder Number:	CC283143	Analytical Uncertainty:
50.0 ppm PROPANE	± 1 %	
Balance AIR		

Certification Information: Certification Date: 4/12/2010 Term: 96 Months Expiration Date: 4/12/2018

This cylinder was certified according to the 1997 EPA Traceability Protocol, Document #EPA-600/R-97/121, using Procedure G1. Do Not Use this Standard if Pressure is less than 150 PSIG.

Analytical Data:

(R=Reference Standard, Z=Zero Gas, C=Gas Candidate)

1. Component: PROPANE

Requested Concentration: 50 ppm
Certified Concentration: 50.0 ppm
Instrument Used: VARIAN 3300 INST 023 (PROPANE)
Analytical Method: FID
Last Multipoint Calibration: 3/16/2010

First Analysis Data:		Date:		4/12/2010
Z: 0	R: 50.39	C: 49.84	Conc: 49.777	
R: 50.36	Z: 0	C: 50.21	Conc: 50.147	
Z: 0	C: 50.2	R: 50.34	Conc: 50.137	
UOM: PPM	Mean Test Assay:		50.02 PPM	

Reference Standard Type: GMIS
Ref. Std. Cylinder #: CC162336
Ref. Std. Conc: 50.3 PPM
Ref. Std. Traceable to SRM #: 1668b
SRM Sample #: 82-J-49
SRM Cylinder #: XF003734B

Second Analysis Data:		Date:		
Z: 0	R: 0	C: 0	Conc: 0	
R: 0	Z: 0	C: 0	Conc: 0	
Z: 0	C: 0	R: 0	Conc: 0	
UOM: PPM	Mean Test Assay:		0 PPM	

Analyzed by:

Megha Patel for
John Pribish

Certified by:

Robin Morgan
Robin Morgan

CERTIFICATE OF ANALYSIS

Grade of Product: EPA Protocol

Part Number:	E02AI99E15A3227	Reference Number:	122-124370084-1
Cylinder Number:	SG9164792BAL	Cylinder Volume:	146.2 CF
Laboratory:	ASG - Durham - NC	Cylinder Pressure:	2015 PSIG
PGVP Number:	B22013	Valve Outlet:	590
Gas Code:	PPN	Certification Date:	Apr 17, 2013

Expiration Date: Apr 17, 2021

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS					
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
PROPANE	86.00 PPM	86.13 PPM	G1	+/- 1% NIST Traceable	04/17/2013
AIR	Balance				

CALIBRATION STANDARDS					
Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
NTRM	09061735	CC304058	97.82 PPM PROPANE/AIR	+/- 0.5%	Oct 02, 2013

ANALYTICAL EQUIPMENT		
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Nicolet 6700 AHR0801333 C3H8	FTIR	Mar 20, 2013

Triad Data Available Upon Request

Notes:

[Signature]

Approved for Release



Praxair Distribution Mid-Atlantic
145 Shimersville Rd.
Bethlehem, PA 18015
Telephone: (610) 317-1608
Facsimile: (610) 758-8382

DocNumber: 000007981

CERTIFICATE OF ANALYSIS / EPA PROTOCOL GAS

Customer & Order Information:

CHEROKEE INSTRUMENTS INC *
901 BRIDGE ST
FUQUAY VARINA NC 275260

Praxair Order Number: 15303079
Customer P. O. Number: 11036
Customer Reference Number:

FBI Date: 12/8/2010
Part Number: AI PR260ZE-AS
Lot Number: 917034266
Cylinder Style & Outlet: AS CGA 590
Cylinder Pressure & Volume: 2000 psig 140 cu. ft.

Certified Concentration:

Expiration Date:	12/13/2013	NIST Traceable
Cylinder Number:	CC109519	Analytical Uncertainty:
258.1 ppm PROPANE	± 1 %	
Balance AIR		

Certification Information: Certification Date: 12/13/2010 Term: 36 Months Expiration Date: 12/13/2013

This cylinder was certified according to the 1997 EPA Traceability Protocol, Document #EPA-600/R-97/121, using Procedure G1
Do Not Use this Standard if Pressure is less than 150 PSIG

Analytical Data:

(R=Reference Standard, Z=Zero Gas, C=Gas Candidate)

1. Component: PROPANE

Requested Concentration: 260 ppm
Certified Concentration: 258.1 ppm
Instrument Used: VARIAN 3300 INST 023 (PROPANE)
Analytical Method: FID
Last Multipoint Calibration: 11/19/2010

Reference Standard Type: GMIS
Ref. Std. Cylinder #: CC138736
Ref. Std. Conc: 499.9 PPM
Ref. Std. Traceable to SRM #: 1669b
SRM Sample #: 81-H-14
SRM Cylinder #: XF004157b

First Analysis Data:		Date:	12/13/2010
Z: 0	R: 501.2	C: 258.6	Conc: 258.07
R: 501.4	Z: 0	C: 258.5	Conc: 257.97
Z: 0	C: 258.7	R: 500.2	Conc: 258.17
UOM: PPM	Mean Test Assay: 258.07 PPM		

Second Analysis Data:		Date:	
Z: 0	R: 0	C: 0	Conc: 0
R: 0	Z: 0	C: 0	Conc: 0
Z: 0	C: 0	R: 0	Conc: 0
UOM: PPM	Mean Test Assay: 0 PPM		

Analyzed by:

John Pribish 12/28/10

Certified by:

Ashley Davila



Praxair Distribution Mid-Atlantic
145 Shimersville Rd.
Bethlehem, PA 18015
Telephone: (610) 317-1608
Facsimile: (610) 758-8382

DocNumber: 000009995

CERTIFICATE OF ANALYSIS / EPA PROTOCOL GAS

Customer & Order Information:

CHEROKEE INSTRUMENTS INC *
901 BRIDGE ST
FUQUAY VARINA NC 275260

Praxair Order Number: 16230993
Customer P. O. Number: 11207
Customer Reference Number:

Fill Date: 3/17/2011
Part Number: EV AIPR500ME-AS
Lot Number: 917117666
Cylinder Style & Outlet: AS CGA 590
Cylinder Pressure & Volume: 2000 psig 140 cu. ft.

Certified Concentration:

Expiration Date:	3/21/2014	NIST Traceable
Cylinder Number:	SA20675	Analytical Uncertainty:
507.1 ppm	PROPANE	± 1 %
Balance	AIR	

Certification Information: Certification Date: 3/21/2011 Term: 36 Months Expiration Date: 3/21/2014

This cylinder was certified according to the 1997 EPA Traceability Protocol, Document #EPA-600/R-97/121, using Procedure G1

Do Not Use this Standard if Pressure is less than 150 PSIG

Analytical Data:

(R=Reference Standard, Z=Zero Gas, C=Gas Candidate)

1. Component: PROPANE

Requested Concentration: 500 ppm
Certified Concentration: 507.1 ppm
Instrument Used: VARIAN 3300 INST 023 (PROPANE)
Analytical Method: FID
Last Multipoint Calibration: 3/16/2011

First Analysis Data:		Date:	3/21/2011
Z:	0	R:	749.9
C:	508.2	Conc:	507.86
R:	749.1	Z:	0
C:	507.2	Conc:	506.86
Z:	0	C:	506.8
R:	750.4	Conc:	506.46
UOM:	PPM	Mean Test Assay:	507.06 PPM

Analyzed by:

John Pribish

Reference Standard Type: GMIS
Ref. Std. Cylinder #: CC103865
Ref. Std. Conc: 749.3 PPM
Ref. Std. Traceable to SRM #: 2646a
SRM Sample #: 103-C-23
SRM Cylinder #: XF000820B

Second Analysis Data:		Date:	
Z:	0	R:	0
C:	0	Conc:	0
R:	0	Z:	0
C:	0	Conc:	0
Z:	0	C:	0
R:	0	Conc:	0
UOM:	PPM	Mean Test Assay:	0 PPM

Certified by:

Michelle Kostik

CERTIFICATE OF ANALYSIS

Grade of Product: EPA Protocol

Airgas Specialty Gases
630 United Drive
Durham, NC 27713
919-544-3773 Fax: 919-544-3774
www.airgas.com

Part Number: E02AI99E15A0333
Cylinder Number: CC148274
Laboratory: ASG - Durham - NC
PGVP Number: B22012
Gas Code: APPVD

Reference Number: 122-124344171-1
Cylinder Volume: 146 Cu.Ft.
Cylinder Pressure: 2015 PSIG
Valve Outlet: 590
Analysis Date: Nov 05, 2012

Expiration Date: Nov 05, 2020

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS				
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty
PROPANE	850.0 PPM	836.9 PPM	G1	+/- 1% NIST Traceable
Air	Balance			

CALIBRATION STANDARDS				
Type	Lot ID	Cylinder No	Concentration	Expiration Date
NTRM	110609	CC343416	1000.3PPM PROPANE/NITROGEN	Mar 04, 2017

ANALYTICAL EQUIPMENT		
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Nicolet 6700 AHR0801333 C3H8	FTIR	Oct 11, 2012

Triad Data Available Upon Request

Notes:ANW PN: 781018

Approved for Release

6141 EASTON ROAD, BLDG 1, PLUMSTEADVILLE, PA 18949-0310

Phone: 800-331-4953 Fax: 215-766-7226

CERTIFICATE OF ACCURACY: Certified Working Class Calibration Standard

Product Information

Document #: 46628943-001
Item No.: MM301080-T-30AL
P.O. No.: 06081203

Cylinder Number: ALM018055
Cylinder Size: 30AL
Certification Date: 21Jun2012
Expiration Date: 21Jun2014
Lot Number: PLU0109851

Customer

ENTHALPY ANALYTICAL, INC.
06081203
800-1 CAPITOLA DRIVE
DURHAM, NC 27703
US

CERTIFIED CONCENTRATION

<u>Component Name</u>	<u>Concentration (Moles)</u>	<u>Accuracy (+/-%)</u>
METHANOL	105. PPM	5
SULFUR HEXAFLUORIDE	3.0 PPM	5
NITROGEN	BALANCE	

TRACEABILITY

Traceable To

Scott Reference Standard

APPROVED BY:


DAVID ASHNOFF

DATE:

6-21-2012

CERTIFICATE OF ANALYSIS

Grade of Product: CERTIFIED STANDARD-SPEC

Part Number: X03NI99C15A1FX5
Cylinder Number: CC90659
Laboratory: ASG - Port Allen - LA
Analysis Date: Sep 30, 2013
Lot Number: 83-124390037-1A

Reference Number: 83-124390037-1A
Cylinder Volume: 144.4 CF
Cylinder Pressure: 2015 PSIG
Valve Outlet: 350S

Product composition verified by direct comparison to calibration standards traceable to N.I.S.T. weights and/or N.I.S.T. Gas Mixture reference materials.

ANALYTICAL RESULTS

Component	Requested Concentration	Actual Concentration (Mole %)	Analytical Uncertainty
SULFUR HEXAFLUORIDE	3.000 PPM	3.127 PPM	+/- 5%
METHANOL	100.0 PPM	91.71 PPM	+/- 2%
NITROGEN	Balance		

Notes:


Approved for Release

CERTIFICATE OF ANALYSIS

Grade of Product: CERTIFIED STANDARD-SPEC

Part Number: X02NI99C15A1268

Cylinder Number: CC432538

Laboratory: ASG - Durham - NC

Analysis Date: May 08, 2013

Lot Number: 122-124373993-1

Reference Number: 122-124373993-1

Cylinder Volume: 144.4 CF

Cylinder Pressure: 2015 PSIG

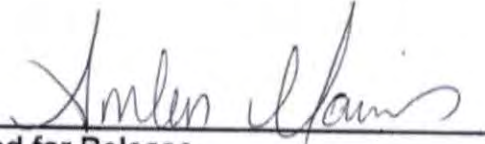
Valve Outlet: 350

Product composition verified by direct comparison to calibration standards traceable to N.I.S.T. weights and/or N.I.S.T. Gas Mixture reference materials.

ANALYTICAL RESULTS

Component	Requested Concentration	Actual Concentration (Mole %)	Analytical Uncertainty
ETHYLENE	100.0 PPM	99.88 PPM	+/- 2%
NITROGEN	Balance		

Notes:


Approved for Release

APPENDIX F

Equipment Calibration Sheets

APEX INSTRUMENTS METHOD 5 POST-TEST CONSOLE CALIBRATION
USING CALIBRATED CRITICAL ORIFICES
3-POINT ENGLISH UNITS

Meter Console Information	
Console Model Number	522
Console Serial Number	909033
DGM Model Number	RW 110
DGM Serial Number	961167

Calibration Conditions			
Date	Time	10/23/13	1030
Barometric Pressure		29.46	in Hg
Theoretical Critical Vacuum ¹		13.91	in Hg
Calibration Technician		TTB	

Factors/Conversions		
Std Temp	528	°R
Std Press	29.92	in Hg
K ₁	17.647	oR/in Hg

¹For valid test results, the Actual Vacuum should be 1 to 2 in. Hg greater than the Theoretical Critical Vacuum shown above.

²The Critical Orifice Coefficient, K', must be entered in English units, (ft³*°R^{1/2})/(in.Hg*min).

Calibration Data										
Run Time		Metering Console				Critical Orifice				
Elapsed	DGM Orifice ΔH	Volume Initial	Volume Final	Outlet Temp Initial	Outlet Temp Final	Serial Number	Coefficient	Amb Temp Initial	Amb Temp Final	Actual Vacuum
(θ)	(P _m)	(V _{mi})	(V _{mf})	(t _{mi})	(t _{mf})	FO55	K'	(t _{amb})	(t _{amb})	
min	in H ₂ O	cubic feet	cubic feet	°F	°F	FO55	see above ²	°F	°F	in Hg
16.0	1.20	637.000	646.659	62	63	FO55	0.4594	63	65	19.00
13.0	1.20	647.000	654.859	64	64	FO55	0.4594	65	65	19.00
13.0	1.20	655.100	662.965	64	65	FO55	0.4594	65	66	19.00

Results								
Standardized Data				Dry Gas Meter				
Dry Gas Meter		Critical Orifice		Calibration Factor		Flowrate	ΔH @	
(V _{m(std)})	(Q _{m(std)})	(V _{cr(std)})	(Q _{cr(std)})	Value	Variation	Std & Corr	0.75 SCFM	Variation
(V _{m(std)})	(Q _{m(std)})	(V _{cr(std)})	(Q _{cr(std)})	(Y)	(ΔY)	(Q _{m(std)(corr)})	(ΔH@)	(ΔΔH@)
cubic feet	cfm	cubic feet	cfm			cfm	in H ₂ O	
9.639	0.602	9.460	0.591	0.981	0.000	0.591	1.934	0.001
7.821	0.602	7.679	0.591	0.982	0.000	0.591	1.933	-0.001
7.819	0.601	7.675	0.590	0.982	0.000	0.590	1.933	-0.001
Pretest Gamma	0.9828	% Deviation	0.1	0.982	Y Average		1.933	ΔH@ Average

Note: For Calibration Factor Y, the ratio of the reading of the calibration meter to the dry gas meter, acceptable tolerance of individual values from the average is +0.02.

I certify that the above Dry Gas Meter was calibrated in accordance with USEPA Methods, CFR Title 40, Part 60, Appendix A-3, Method 5, 16.2.3

Signature _____ Todd Brozell

Date _____ 10/23/2013

Type S Pitot Tube Inspection and
Stack Thermocouple Calibration

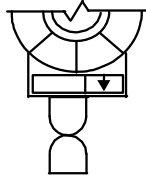
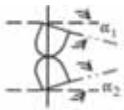
GENERAL INFORMATION

Probe ID
Date

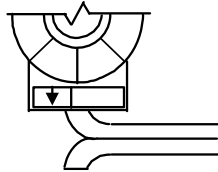
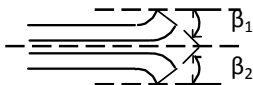
Personnel
Coefficient Value

PITOT TUBE INSPECTION

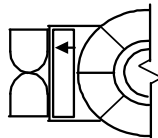
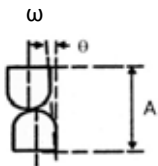
Pitot Tube assembly level? (yes/no)
Pitot Tube obstruction? (yes/no)
Pitot Tube openings damaged? (yes/no)



α_1 $\leq \pm 10^\circ$
 α_2 $\leq \pm 10^\circ$

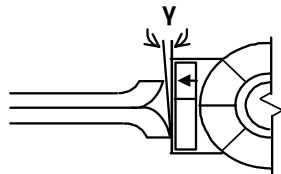
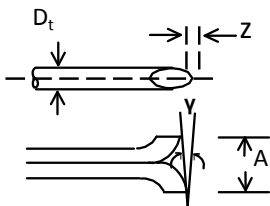


β_1 $\leq \pm 5^\circ$
 β_2 $\leq \pm 5^\circ$



γ
 θ
 $z = A \tan (\gamma)$ $\leq \pm \frac{1}{8}"$
 $\omega = A \tan (\theta)$ $\leq \pm \frac{1}{32}"$

D_t
($\frac{3}{16}" < D_t < \frac{3}{8}"$ Recommended)



A

P_A
 P_B
($1.05 < P/D_t < 1.50$ Recommended)

STACK THERMOCOUPLE CALIBRATION

Ref. Type

Ref. ID

Source	Ref., °F	Stack TC, °F	Abs. Diff., °F
Ice bath	43	45	2
Ambient	75	75	0
Hot water	193	194	1
Maximum Temp. Difference, °F			2

Type S Pitot Tube Inspection and
Stack Thermocouple Calibration

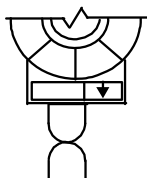
GENERAL INFORMATION

Probe ID
Date

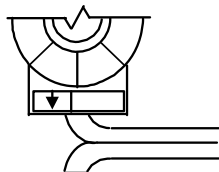
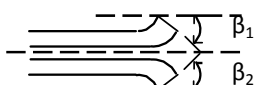
Personnel
Coefficient Value

PITOT TUBE INSPECTION

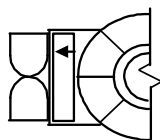
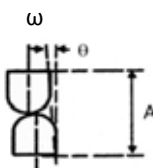
Pitot Tube assembly level? (yes/no)
Pitot Tube obstruction? (yes/no)
Pitot Tube openings damaged? (yes/no)



α_1 $\leq \pm 10^\circ$
 α_2 $\leq \pm 10^\circ$



β_1 $\leq \pm 5^\circ$
 β_2 $\leq \pm 5^\circ$



γ
 θ

$z = A \tan(\gamma)$ $\leq \pm \frac{1}{8}"$
 $\omega = A \tan(\theta)$ $\leq \pm \frac{1}{32}"$

D_t
($\frac{3}{16}" < D_t < \frac{3}{8}"$ Recommended)

A

P_A
 P_B
($1.05 < P/D_t < 1.50$ Recommended)

STACK THERMOCOUPLE CALIBRATION

Ref. Type

Ref. ID

Source	Ref., °F	Stack TC, °F	Abs. Diff., °F
Ice bath	43	45	2
Ambient	75	75	0
Hot water	193	192	1
Maximum Temp. Difference, °F			2